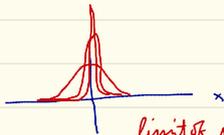


## \* Recap from last time

Dirac delta function:

$$\delta(x) = \begin{cases} 0 & x \neq 0 \\ \infty & x = 0 \end{cases}$$



limit of infinitely narrow spike @  $x=0$  but w/ unit area

where

$$\int_a^b \delta(x) dx = 1$$

where  $a < 0 < b$

$$\int_a^b \delta(x) f(x) dx = f(0)$$

↑  
arbitrary function

shifted  $\delta$ -fun:  $\delta(x-x') = \begin{cases} 0 & x \neq x' \\ \infty & x = x' \end{cases} \Rightarrow \int_a^b \delta(x-x') dx = 1$  if  $a < x' < b$

$$\int_a^b \delta(x-x') f(x) dx = f(x')$$

3d  $\delta$ -fun:  $\delta^3(\vec{r}) \equiv \delta(x)\delta(y)\delta(z)$

$$\int_{\text{Vol}} \delta^3(\vec{r}) F(\vec{r}) d^3r = F(0) \text{ if Vol encloses } \vec{r}=0 \\ = 0 \text{ else}$$

Useful identities we derived

$$\vec{\nabla} \cdot \left( \frac{\hat{r}}{r^2} \right) = 4\pi \delta^3(\vec{r})$$

$$\vec{\nabla} \cdot \left( \frac{\vec{r}-\vec{r}'}{|\vec{r}-\vec{r}'|^3} \right) = 4\pi \delta^3(\vec{r}-\vec{r}')$$

Used these to derive  
Gauss's Law

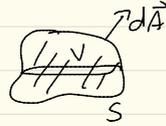
# Gauss's Law (Differential + Integral)

$$\vec{\nabla} \cdot \vec{g}(\vec{r}) = -4\pi G \rho(\vec{r})$$

⊛

$$\oint_S \vec{g} \cdot d\vec{A} = -4\pi G M_{\text{enclosed}}$$

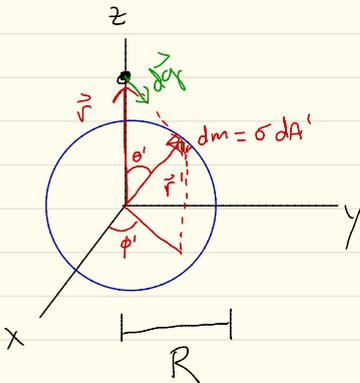
$$M_{\text{enclosed}} = \int_V \rho(\vec{r}) d^3r$$



Eqn ⊛ is true in general. However, in specific cases where  $\rho(\vec{r})$  is highly symmetric, then ⊛ gives us a way to trivially calculate  $\vec{g}(\vec{r})$ .

To appreciate the labor saved by ⊛, let's first sketch the soln for a problem in the "brute force" approach.

e.g.: Hollow spherical shell w/ uniform surface  $\sigma = \frac{M}{4\pi R^2}$



$$d\vec{g}(\vec{r} = z\hat{k}) = -G dm \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3}$$

Symmetry:  $\int d\vec{g}(0,0,z) = g(0,0,z) \hat{k}$

$$\therefore g = \int d\vec{g} \cdot \hat{k}$$

Identifying the relevant variable

$$\vec{r} = z \hat{k}$$

$$\vec{r}' = R \sin \theta' \cos \phi' \hat{i} + R \sin \theta' \sin \phi' \hat{j} + R \cos \theta' \hat{k}$$

↓

$$|\vec{r} - \vec{r}'|^3 = [R^2 + z^2 - 2Rz \cos \theta']^{3/2}$$

$$\therefore d\vec{g} = \frac{-G dm (R \sin \theta' \cos \phi' \hat{i} + R \sin \theta' \sin \phi' \hat{j} + (z - R \cos \theta') \hat{k})}{[R^2 + z^2 - 2Rz \cos \theta']^{3/2}}$$

$$\boxed{d\vec{g} \cdot \hat{k} = \frac{-G dm (z - R \cos \theta')}{[R^2 + z^2 - 2Rz \cos \theta']^{3/2}}}$$

\* recall,  $dA' = R^2 \sin \theta' d\theta' d\phi'$  for spherical surface.

and

$$dm = \sigma dA' = \frac{M}{4\pi R^2} R^2 \sin \theta' d\theta' d\phi'$$

$$\therefore g(\theta, z) = \frac{-MG}{4\pi} \int_0^{2\pi} \int_0^{\pi} \frac{(z - R \cos \theta')}{[R^2 + z^2 - 2Rz \cos \theta']^{3/2}} \sin \theta' d\theta' d\phi'$$

$$= \frac{-MG}{2} \int_0^{\pi} \frac{z - R \cos \theta'}{[R^2 + z^2 - 2Rz \cos \theta']^{3/2}} \sin \theta' d\theta'$$

$$\left. \begin{array}{l} * \text{ let } u = \cos \theta' \\ du = -\sin \theta' d\theta' \end{array} \right\} \Rightarrow g = \frac{-MG}{2} \int_{-1}^{+1} \frac{(z - Ru) du}{[R^2 + z^2 - 2Rz u]^{3/2}}$$

$$g = \frac{-MG}{2} \int_{-1}^{+1} \frac{(z - Ru) du}{[R^2 + z^2 - 2Rzu]^{3/2}} = (\text{Thanks to Mathematica})$$

$$\text{integral} = \begin{cases} 0 & \text{if } z < R \\ \frac{2}{z^2} & \text{if } z \geq R \end{cases}$$

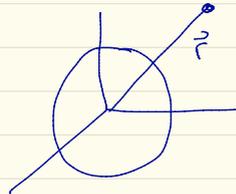
=> At the end of a long & tedious calculation, we thus find

$$\vec{g}(0,0,z) = \begin{cases} 0 & \text{if } z < R \\ -\frac{MG}{z^2} \hat{k} & \text{if } z \geq R \end{cases}$$

NOTE: for  $z \geq R$ , this is the same you would get for a point mass  $M$  placed at the origin.

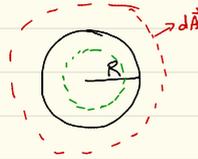
\* Also note that the spherical symmetry implies

$$\vec{g}(\vec{r}) = \begin{cases} 0 & \text{if } |\vec{r}| < R \\ -\frac{MG}{r^2} \hat{r} & \text{if } |\vec{r}| \geq R \end{cases}$$



\* OK, having convinced you that the hollow sphere problem is somewhat tedious (yet such a simple final form), we now show how to solve it trivially using Gauss's Law.

$$\oint_S \vec{g} \cdot d\vec{A} = -4\pi G M_{\text{enc}}$$



\* The surface  $S$  is arbitrary. Let us consider  $S =$  sphere of radius  $r$  & consider the 2 cases  $r > R$  &  $r < R$ .

Step 1: spherical symmetry (mathematically, this means  $\rho(r, \theta, \phi) = \rho(r)$ . No directional dep!) implies

$$\vec{g}(r, \theta, \phi) = g(r) \hat{r}$$

(This is the crucial step in all Gauss's Law problems!)

Step 2:  $d\vec{A} = r^2 \sin\theta d\theta d\phi \hat{r} \equiv r^2 d\Omega \hat{r}$

$$\therefore \oint_S \vec{g} \cdot d\vec{A} = \int_{\text{Sphere}} g(r) r^2 d\Omega = g(r) 4\pi r^2$$

Sphere  
radius  $r$

Case 1:  $r < R \Rightarrow M_{\text{enclosed}} = 0$

$$\therefore g(r) 4\pi r^2 = 0 \Rightarrow g(r < R) = 0$$

Case 2:  $r \geq R \Rightarrow M_{\text{enclosed}} = M \Rightarrow g(r > R) = \frac{-4\pi G M}{4\pi r^2} = -\frac{GM}{r^2}$

Which agrees w/ our earlier result!

General Idea: for very symmetric  $S$ , use symmetry to "guess" the form of  $\vec{g}$   
that lets you pull  $\vec{g}$  out of the integral

$$\oint_S \vec{g} \cdot d\vec{A}$$

for suitably chosen  $S$ . ("Gaussian Surface")

\* Can do this for 2 other "classes" of  $S$   $\left\{ \begin{array}{l} \text{cylindrical symmetry} \\ \text{planar symmetry} \end{array} \right.$

### Cylindrical (aka axial) symmetry

Mathematical criteria  $\rho(r, \phi, z) = \rho(r)$

NOTE: Here  $r, \phi, z$  are cylindrical coords!

$$\Rightarrow \vec{g}(r, \phi, z) = g(r) \hat{r}$$

Example:



\* brute force calc. for finite wire (length  $2l$ ) done in class last week

- in midplane, argued that vertical components of  $\vec{g}$  cancel. I.e.,

$$\vec{g}_{2l}(r) = -G\lambda r \cdot \frac{2l}{r^2 \sqrt{l^2 + r^2}} \hat{r} \quad \text{in } z=0 \text{ plane}$$

\* for  $\infty$ -wire, every point is the "midplane" (not just  $z=0$ )

$$\Rightarrow \vec{g}(r, \phi, z) = g(r) \hat{r}$$



$$\oint \vec{g} \cdot d\vec{A} = \int_{\text{Lids of cylinder}} \vec{g} \cdot d\vec{A} + \int_{\text{Sides of cylinder}} \vec{g} \cdot d\vec{A}$$

0 since  $d\vec{A} \perp \vec{g}$

for sides of cylinder,  $d\vec{A} = \hat{r} 2\pi r dz$

$$\Rightarrow \oint \vec{g} \cdot d\vec{A} = g(r) 2\pi r \int_{-\frac{h}{2}}^{\frac{h}{2}} dz = g(r) 2\pi r h$$

$$M_{\text{enclosed}} = h\lambda$$

$$\therefore \oint \vec{g} \cdot d\vec{A} = -4\pi\epsilon_0 M_{\text{enc}} \Rightarrow g(r) 2\pi r \cancel{h} = -4\pi\epsilon_0 \cancel{h} \lambda$$

$\Downarrow$

$$g(r) = \frac{-2\epsilon_0 \lambda}{r}$$

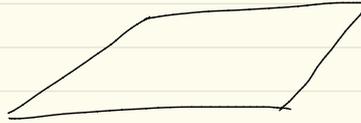
\* Check it by comparing to  $l \rightarrow \infty$  result derived for finite wire

$$\vec{g}_{0z}(r) = -G\lambda r \cdot \frac{z l}{r^2 \sqrt{l^2 + r^2}} \hat{r} \quad \text{in } z=0 \text{ plane}$$

$$= \frac{-G\lambda z l}{r l \sqrt{1 + (r/z)^2}} \xrightarrow{l \rightarrow \infty} \frac{-2G\lambda}{r} \checkmark$$

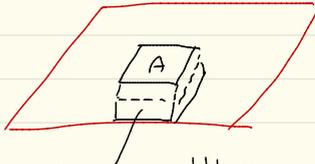
NOTE: For cylindrical symmetric masses, strictly speaking they must be infinite in the  $z$ -direction for  $\rho(r, \phi, z) = \rho(r)$  to be obeyed. HOWEVER, we often cheat & assume  $\vec{g} = g(r) \hat{r}$  if the mass is "very long" but finite. In this case, the Gauss's Law result will be the most accurate close to the midplane  $z=0$ .

Planar Symmetry example



$\infty$ -plane w/ uniform  $\sigma$   
at  $z=0$

Symmetry:  $\vec{g} = \begin{cases} -|g| \hat{k} & z > 0 \\ +|g| \hat{k} & z < 0 \end{cases}$



Gaussian matchbox  
equal distant above/below

$$\oint_{\text{Multi-body}} \vec{g} \cdot d\vec{A} = \int_{\text{Top}} \vec{g} \cdot d\vec{A} + \int_{\text{bottom}} \vec{g} \cdot d\vec{A} + \int_{\text{Sides}} \vec{g} \cdot d\vec{A}$$

$$d\vec{A}_{\text{top}} = dx dy \hat{k}$$

$$d\vec{A}_{\text{bot}} = -dx dy \hat{k}$$

$$\therefore \oint \vec{g} \cdot d\vec{A} = -2|g|A = -4\pi G M_{\text{enc}}$$

$$M_{\text{enc}} = A\sigma$$

$$\Rightarrow -2|g|A = -4\pi G A \sigma$$

$$\Rightarrow |g| = 2\pi\sigma G$$