

^{29}Si $Z = 14$ $N = 15$ [link to full NNDC output](#)

Based on ENSDF from Dec 2018, and mass evaluation from 2016

BE = 245.010 (0.000) MeV

	Energy T	J+	J-	J-other	T1/2
29SI 1	0.000	1/2+			1 STABLE
29SI 2	1.273	3/2+			2 291 FS 10
29SI 3	2.028	5/2+			3 306 FS 10
29SI 4	2.426	3/2+			4 18.1 FS 7
29SI 5	3.067	5/2+			5 33 FS 1
29SI 6			3.623	7/2-	6 2.63 PS 9
29SI 7	4.080	7/2+			7 44 FS 12
29SI 8				4.741 (9/2+)	8 36 FS 7
29SI 9	4.840	1/2+			9 3.5 FS LT
29SI 10	4.895	5/2+			10 12 FS 5
29SI 11			4.934	3/2-	11 0.84 FS 12
29SI 12				5.254 (9/2-)	12 82 FS 4
29SI 13	5.285	7/2+			13 6 FS 3
29SI 14	5.652	9/2+			14 51 FS 3
29SI 15	5.812	7/2+			15 32 FS 12
29SI 16	5.947	3/2+			16 10 FS LT
29SI 17				6.107 5/2	17 21 FS 3
29SI 18			6.193	7/2-	18 17 FS 3
29SI 19			6.381	1/2-	19 0.36 FS 11
29SI 20				6.423 (7/2+)	20 14 FS LT
29SI 21	6.496	1/2+ 5/2+			21 24 FS LT
29SI 22	6.522	5/2+			22 10 FS LT
29SI 23				6.615 (9/2+)	23 14 FS LT
29SI 24	6.696	1/2+			24
29SI 25				6.710 (5/2+)	25 62 FS LT
29SI 26				6.713 (3/2)	26
29SI 27				6.781 (11/2-)	27 15 FS 2
29SI 28				6.909 (1/2+, 3/2)	28
29SI 29				6.921 (7/2+)	29 14 FS LT
29SI 30				7.014 (5/2-, 7/2-)	30 32 FS 10
29SI 31	7.058	1/2+			31 15 FS LT
29SI 32				7.072 (3/2+, 5/2+)	32 10.4 FS LT
29SI 33				7.139 (11/2+)	33 29 FS 10
29SI 34				7.182 (3/2)	34
29SI 35				7.197 (3/2, 5/2)	35
29SI 36				7.523 (1/2, 3/2)	36 14 FS LT
29SI 37				7.622 (5/2-, 7/2-)	37 10.4 FS LT
29SI 38				7.692 (1/2+, 3/2+)	38

29SI 39				7.767	(3/2,5/2)	39	14 FS	LT
29SI 40				7.787	(7/2+)	40	15 FS	8

29SI 41				7.892		41		
29SI 42				7.987	(9/2)	42	14 FS	LT
29SI 43				7.997	(3/2-)	43		
29SI 44				8.138		44		
29SI 45				8.161		45	14 FS	LT
29SI 46				8.173	(11/2+)	46	14 FS	LT
29SI 47				8.209	(3/2+)	47	14 FS	LT
29SI 48				8.270	(5/2-,7/2-)	48		
29SI 49		8.290 3/2 5/2+				49		
29SI 50				8.331		50	10.4 FS	LT

29SI 51				8.349		51		
29SI 52				8.371		52		
29SI 53				8.418	(3/2)	53		
S-n =	8.474	(0.000)	-----					
29SI 54				8.476		54	10.4 FS	LT
29SI 55				8.507	(3/2+,5/2+)	55		
29SI 56				8.529		56		
29SI 57				8.541		57		
29SI 58				8.558		58		
29SI 59				8.603		59		
29SI 60				8.609		60	15 FS	LT

29SI 61				8.610		61	15 FS	LT
29SI 62				8.622		62	15 FS	LT
29SI 63				8.641		63	14 FS	LT
29SI 64				8.655		64	60 KEV	7
29SI 65				8.670		65	15 FS	LT
29SI 66				8.762		66	19 FS	4
29SI 67				8.854		67		
29SI 68				8.865		68	29 FS	10
29SI 69				8.909		69		
29SI 70				8.959		70		

29SI 71				9.019		71		
29SI 72				9.151		72		
29SI 73				9.157		73		
29SI 74				9.219		74		
29SI 75				9.252		75		
29SI 76				9.298		76		
29SI 77				9.326		77	14 FS	LT
29SI 78				9.392		78		
29SI 79				9.413		79		
29SI 80				9.518		80		

29SI 81		9.630 3/2 1/2+				81		
29SI 82				9.667		82		

29SI 83				9.683	83
29SI 84				9.765	84
29SI 85				9.779	85
29SI 86				9.850	86
29SI 87				9.943	87
29SI 88				9.952	88
29SI 89				9.987	89
29SI 90				10.006	90

29SI 91				10.083	91
29SI 92				10.131	92
29SI 93				10.170	93
29SI 94				10.213	94
29SI 95				10.236	95
29SI 96				10.252	96
29SI 97				11.087 3/2 (3/2+,5/2+)	97
S-alpha=	11.127	(0.000)	-----		
29SI 98				11.305 3/2 (3/2+,5/2+)	98
29SI 99		11.665 3/2 1/2+			99

S-p = 12.333 (0.000)-----
S-n = 8.474 (0.000)-----
S-2p = 21.886 (0.000)-----
S-2n = 25.653 (0.000)-----
S-alpha= 11.127 (0.000)-----

S+p = -5.595 (0.000)
S+n = -10.609 (0.000)
S+2p = -11.725 (0.000)
S+2n = -17.197 (0.000)
S+alpha = -7.116 (0.000)

gap p = 6.739 (0.000)
gap n = -2.136 (0.000)
gap 2p = 10.161 (0.000)
gap 2n = 8.457 (0.000)
gap alpha = 4.011 (0.000)