

^{75}Se $Z = 34$ $N = 41$ [link to full NNDC output](#)

Based on ENSDF from Dec 2018, and mass evaluation from 2016

BE = 650.919 (0.000) MeV

Qbeta+ = 0.865 (0.001) MeV

	Energy T	J+	J-	J-other	T1/2
75SE 1	0.000	5/2+			1 119.78 D 5
75SE 2	0.112	7/2+			2 0.69 NS 12
75SE 3	0.133	9/2+			3 5.3 NS 6
75SE 4			0.287 3/2-		4 1.29 NS 15
75SE 5			0.293 1/2-		5 30.0 NS 4
75SE 6			0.428 5/2-		6
75SE 7			0.586 3/2-		7
75SE 8	0.611	1/2+			8
75SE 9	0.628	5/2+			9
75SE 10			0.664 5/2-		10
75SE 11			0.748 7/2-		11
75SE 12				0.761	12
75SE 13			0.777 5/2-		13
75SE 14				0.790 7/2(+)	14
75SE 15	0.814	11/2+			15
75SE 16	0.840	3/2+			16
75SE 17			0.860 3/2-		17
75SE 18				0.895 1/2-,3/2-	18
75SE 19	0.934	13/2+			19
75SE 20				0.953 5/2+,7/2	20
75SE 21			0.963 3/2-		21
75SE 22	1.004	5/2+			22 0.054 PS +29-18
75SE 23				1.020 1/2-,3/2-	23
75SE 24				1.047 5/2-,7/2-	24 0.11 PS +10-3
75SE 25				1.066	25
75SE 26			1.074 5/2-		26 0.073 PS +45-24
75SE 27			1.079 9/2-		27
75SE 28				1.087	28
75SE 29				1.088 (7/2)	29 0.2 PS +10-1
75SE 30				1.144 3/2+,5/2+	30 0.09 PS +6-3
75SE 31				1.162 (7/2+,9/2+)	31
75SE 32				1.182 5/2-,7/2-	32
75SE 33				1.184 1/2,3/2,5/2	33
75SE 34				1.189	34
75SE 35	1.199	5/2+			35 0.13 PS +17-6
75SE 36			1.245 3/2-		36 0.25 PS +69-10
75SE 37				1.260	37 0.044 PS +18-12

75SE 38						1.302	5/2,7/2	38	0.14 PS	+10-5
75SE 39						1.369	(7/2+,9/2+)	39		
75SE 40						1.375	1/2,3/2,5/2	40		

75SE 41						1.380		41		
75SE 42						1.407	(5/2-,7/2-)	42		
75SE 43						1.432		43		
75SE 44		1.433	1/2+					44		
75SE 45						1.439	(7/2+)	45	0.037 PS	+13-8
75SE 46						1.455		46		
75SE 47						1.457	(5/2-)	47	0.19 PS	+18-7
75SE 48						1.484	5/2-,7/2-	48		
75SE 49						1.488	(11/2-)	49		
75SE 50						1.491	(7/2-)	50	0.10 PS	+6-3

75SE 51						1.550	(7/2+,9/2+)	51	0.064 PS	+21-17
75SE 52						1.551	3/2+,5/2+	52		
75SE 53						1.561	(5/2,7/2-)	53	0.083 PS	+31-21
75SE 54		1.590	5/2+					54	0.050 PS	+15-8
75SE 55						1.603	(3/2+,5/2+)	55		
75SE 56						1.628	(13/2+)	56		
75SE 57		1.653	5/2+					57	0.026 PS	+14-7
75SE 58						1.668	(5/2-)	58	0.037 PS	+18-12
75SE 59						1.673	(1/2-,3/2-)	59		
75SE 60						1.741	(15/2+)	60	0.25 PS	5

75SE 61						1.764	(5/2-,7/2-)	61		
75SE 62		1.784	1/2+					62		
75SE 63						1.802	3/2+,5/2+	63		
75SE 64						1.811	1/2-,3/2-	64		
75SE 65						1.895		65		
75SE 66						1.905	(13/2-)	66		
75SE 67						1.911	(17/2+)	67	0.30 PS	6
75SE 68						1.912		68		
75SE 69						1.913	(1/2-,3/2-)	69		
75SE 70						1.943		70		

75SE 71						1.958		71		
75SE 72						1.986	1/2,3/2,5/2+	72		
75SE 73						2.030	3/2+,5/2+	73		
75SE 74						2.072		74		
75SE 75						2.093		75		
75SE 76						2.119		76		
75SE 77						2.159		77		
75SE 78						2.167	1/2,3/2,5/2+	78		
75SE 79						2.235		79		
75SE 80						2.242		80		

75SE 81						2.271		81		
75SE 82						2.297	(-)	82		

75SE 83				2.349	(3/2+,5/2+)	83		
75SE 84				2.391	(15/2-)	84		
75SE 85				2.437	3/2+,5/2+	85		
75SE 86				2.456	3/2+,5/2+	86		
75SE 87				2.519		87		
75SE 88		2.565	1/2+			88		
75SE 89				2.573	1/2-,3/2-	89		
75SE 90				2.596	(17/2+)	90		

75SE 91				2.598	1/2,3/2,5/2+	91		
75SE 92		2.632	1/2+			92		
75SE 93				2.670		93		
75SE 94				2.713	3/2+,5/2+	94		
75SE 95				2.737	1/2,3/2,5/2+	95		
75SE 96				2.766	(19/2+)	96	0.18 PS	3
75SE 97				2.782		97		
75SE 98		2.824	1/2+			98		
75SE 99				2.840	(17/2-)	99	0.43 PS	20
75SE 100				2.872	(17/2-)	100	0.48 PS	21

75SE 101				2.887		101		
75SE 102				2.932		102		
75SE 103				2.941	3/2+,5/2+	103		
75SE 104				3.019	(21/2+)	104	0.23 PS	6
75SE 105				3.020	(3/2+,5/2+)	105		
75SE 106				3.101	3/2+,5/2+	106		
75SE 107				3.153	3/2+,5/2+	107		
75SE 108				3.170	3/2+,5/2+	108		
75SE 109				3.182		109		
75SE 110				3.210		110		

75SE 111				3.289	(19/2-)	111	0.62 PS	19
75SE 112		3.290	1/2+			112		
75SE 113				3.306	(19/2-)	113		
75SE 114				3.333	3/2+,5/2+	114		
75SE 115				3.340		115		
75SE 116				3.432	(19/2-)	116		
75SE 117				3.457		117		
75SE 118				3.483		118		
75SE 119		3.619	1/2+			119		
75SE 120				3.646	(21/2-)	120		

75SE 121				3.746	(23/2+)	121	0.17 PS	3
75SE 122				3.767		122		
75SE 123				3.885	(21/2-)	123		
75SE 124				3.895		124		
75SE 125				3.917	3/2+,5/2+	125		
75SE 126				4.079		126		
75SE 127				4.130		127		
75SE 128				4.199	(25/2+)	128	0.10 PS	2

75SE 129				4.255		129
75SE 130				4.268	(23/2-)	130

75SE 131				4.296		131
75SE 132				4.472	(23/2-)	132
75SE 133				4.601		133
S-alpha=	4.688	(0.001)	-----			
75SE 134				4.707	(25/2-)	134
75SE 135				4.726	3/2+,5/2+	135
75SE 136				4.831	(27/2+)	136 0.32 PS 6
75SE 137				5.037	(25/2-)	137
75SE 138				5.476	(29/2+)	138 0.11 PS 2
75SE 139				5.586	(27/2-)	139
75SE 140				6.059	(29/2-)	140

75SE 141				6.173	(31/2+)	141
75SE 142				6.871	(33/2+)	142
75SE 143				7.650	(33/2-)	143
75SE 144				7.756	(35/2+)	144
75SE 145		8.028	1/2+			145
75SE 146		8.028	1/2+			146
75SE 147		8.028	1/2+			147
S-n	=	8.028	(0.000)	-----		
75SE 148		8.029	1/2+			148
75SE 149		8.029	1/2+			149
75SE 150		8.029	1/2+			150

75SE 151		8.029	1/2+			151
75SE 152		8.030	1/2+			152
75SE 153		8.035	1/2+			153
75SE 154				8.448	(37/2+)	154
S-p	=	8.598	(0.002)	-----		
75SE 155				10.243	(41/2+)	155

S-p	=	8.598	(0.002)	-----		
S-n	=	8.028	(0.000)	-----		
S-2p	=	15.450	(0.000)	-----		
S-2n	=	20.085	(0.007)	-----		
S-alpha=	4.688	(0.001)	-----			
S+p	=	-5.409	(0.009)			
S+n	=	-11.154	(0.000)			
S+2p	=	-12.578	(0.002)			
S+2n	=	-18.573	(0.000)			
S+alpha	=	-4.698	(0.003)			
gap p	=	3.190	(0.010)			
gap n	=	-3.126	(0.000)			
gap 2p	=	2.872	(0.002)			

gap 2n = 1.512 (0.007)
gap alpha = -0.010 (0.004)