

^{115}Sn $Z = 50$ $N = 65$ adopted link ENSDF link

Based on ENSDF from Oct 2022, and mass evaluation from 2020

BE = 979.118 (0.000) MeV

	Energy T	J+	J-	J-other	T1/2
115SN 1	0.000	1/2+			1 STABLE
115SN 2	0.497	3/2+			2 11 PS 2
115SN 3	0.613	7/2+			3 3.26 US 8
115SN 4			0.714	11/2-	4 159 US 1
115SN 5	0.987	5/2+			5 1.97 PS 10
115SN 6	1.280	3/2+			6 0.44 PS 9
115SN 7	1.417	5/2+			7 0.35 PS 4
115SN 8				1.634 3/2(+)	8 0.97 PS +35-14
115SN 9				1.644 (7/2-,9/2+)	9
115SN 10				1.644 (7/2-)	10
115SN 11	1.734	5/2+			11
115SN 12				1.786 (9/2 TO 13/2)-	12 0.69 PS +21-14
115SN 13				1.805 (11/2+,13/2+)	13
115SN 14				1.825 (3/2+,5/2+)	14
115SN 15	1.857	7/2+			15 0.35 PS 7
115SN 16				1.946 11/2-,13/2-	16 1.3 PS +4-3
115SN 17	1.974	1/2+			17
115SN 18				1.994 3/2+,5/2+	18
115SN 19				1.997 (11/2+)	19 1.04 PS +21-14
115SN 20				2.025 (15/2-)	20 1.0 PS +4-3
115SN 21	2.060	5/2+			21
115SN 22				2.077 (1/2+)	22
115SN 23				2.084 (9/2+)	23 0.90 PS +28-14
115SN 24				2.156 (7/2+)	24
115SN 25				2.165 (3/2+,5/2+)	25
115SN 26				2.193 (3/2+,5/2+)	26
115SN 27				2.197	27
115SN 28	2.207	5/2+			28 1.0 PS 4
115SN 29				2.230 (3/2,5/2+)	29
115SN 30				2.265 1/2-,3/2-	30
115SN 31				2.302 (5/2-,7/2-)	31
115SN 32				2.314 3/2+,5/2+	32
115SN 33				2.347 (11/2-)	33
115SN 34				2.352 (1/2+,3/2,5/2+)	34
115SN 35				2.365 (3/2+,5/2+)	35
115SN 36				2.371 7/2+,9/2+	36
115SN 37				2.440 (7/2+)	37
115SN 38				2.448 (1/2-,3/2-)	38

115SN 39						2.487	7/2+,9/2+	39		
115SN 40		2.510	5/2+					40		

115SN 41						2.554	(3/2+,5/2+)	41		
115SN 42						2.560	(1/2-,3/2-)	42		
115SN 43						2.592	(15/2-)	43	2.4 PS	GT
115SN 44				2.593	1/2-			44		
115SN 45				2.644	15/2-			45		
115SN 46				2.654	13/2-			46		
115SN 47						2.654	(11/2+)	47	1.2 PS	+14-5
115SN 48						2.686	(17/2-)	48	1.2 PS	+5-3
115SN 49						2.745	(11/2+,13/2+)	49		
115SN 50						2.760		50		

115SN 51						2.770	(1/2-,3/2-)	51		
115SN 52		2.807	5/2+					52	0.6 PS	+4-3
115SN 53						2.808	(15/2,17/2)	53		
115SN 54				2.843	15/2-			54	0.62 PS	+21-14
115SN 55						2.855	3/2+,5/2+	55		
115SN 56						2.860	(11/2+,13/2+)	56		
115SN 57						2.890	9/2-,11/2-	57		
115SN 58						2.913	(13/2+)	58		
115SN 59						2.930	(9/2-,11/2-)	59		
115SN 60						2.938	(17/2-)	60	1.7 PS	GT

115SN 61		2.950	5/2+					61		
115SN 62						2.975	3/2+,5/2+	62		
115SN 63						3.000	(3/2+,5/2+)	63		
115SN 64				3.004	19/2-			64	0.62 PS	+35-21
115SN 65						3.025	(3/2+,5/2+)	65		
115SN 66						3.043	(15/2+)	66		
115SN 67						3.060	7/2+,9/2+	67		
115SN 68						3.085		68		
115SN 69						3.130	3/2+,5/2+	69		
115SN 70						3.190	3/2+,5/2+	70		

115SN 71						3.191	9/2-,11/2-	71		
115SN 72				3.204	17/2-			72	1.0 PS	GT
115SN 73						3.205	(15/2+)	73		
115SN 74						3.206	(3/2+,5/2+)	74		

S-alpha=		3.207 (0.000)								
115SN 75		3.220	17/2+					75	1.2 PS	+4-3
115SN 76				3.259	19/2-			76		
115SN 77						3.265	(3/2+,5/2+)	77		
115SN 78						3.300	(5/2-,7/2-)	78		
115SN 79				3.319	19/2-			79	1.3 PS	+5-4
115SN 80						3.345	3/2+,5/2+	80		

115SN 81						3.380		81		
115SN 82						3.386	(19/2+)	82	0.42 PS	+21-14

115SN 83						3.405	9/2-, 11/2-	83
115SN 84						3.420	3/2+, 5/2+	84
115SN 85						3.470	3/2+, 5/2+	85
115SN 86				3.472	19/2-			86
115SN 87						3.500	7/2+, 9/2+	87
115SN 88		3.510	21/2+					88
115SN 89						3.526	(17/2+)	89
115SN 90						3.533	(19/2+)	90

115SN 91						3.550	3/2+, 5/2+	91
115SN 92						3.590		92
115SN 93						3.645	3/2+, 5/2+	93
115SN 94		3.667	9/2+					94
115SN 95		3.667	23/2+					95
115SN 96						3.690		96
115SN 97						3.710	(7/2+, 9/2+)	97
115SN 98						3.745	(21/2-)	98
115SN 99						3.839	(25/2+)	99
115SN 100						3.842		100

115SN 101						3.859	(19/2+)	101
115SN 102				3.879	21/2-			102 0.8 PS +4-2
115SN 103						3.890		103
115SN 104						3.960	(23/2+)	104
115SN 105						4.030		105
115SN 106				4.047	23/2-			106
115SN 107						4.060	(23/2-)	107 1.0 PS GT
115SN 108						4.132		108
115SN 109						4.163		109
115SN 110						4.243	(21/2+)	110

115SN 111						4.272	(27/2+)	111
115SN 112						4.611	(23/2+)	112
115SN 113						4.636		113
115SN 114				4.688	25/2-			114
115SN 115				4.866	27/2-			115
115SN 116						4.889	(27/2-)	116
115SN 117						5.031		117
115SN 118						5.061	(25/2+)	118
115SN 119						5.093		119
115SN 120						5.226		120

115SN 121		5.331	29/2+					121
115SN 122						5.418	(27/2+)	122
115SN 123		5.434	29/2+					123
115SN 124						5.458	(27/2+)	124
115SN 125						5.600	(29/2)	125
115SN 126				5.630	29/2-			126
115SN 127						5.660		127
115SN 128						5.749	(31/2+)	128

115SN 129		5.810	31/2-		129
115SN 130				5.813 (31/2-)	130

115SN 131				5.911 (31/2+)	131
115SN 132				5.966 (29/2+)	132
115SN 133				6.074	133
115SN 134				6.269 (31/2+)	134
115SN 135				6.287 (33/2)	135
115SN 136				6.357 (31/2-)	136
115SN 137				6.461	137
115SN 138				6.576 (33/2-)	138
115SN 139		6.685	33/2-		139
115SN 140		6.719	35/2-		140

115SN 141				6.831 (35/2-)	141
115SN 142				6.950 (35/2-)	142
115SN 143				7.157 (35/2+)	143
115SN 144				7.249 (37/2-)	144
S-n	=	7.545	(0.000)	-----	
115SN 145				7.684 (39/2-)	145
115SN 146				7.826 (37/2-)	146
115SN 147				7.923 (39/2-)	147
115SN 148				8.163 (39/2+)	148
S-p	=	8.753	(0.000)	-----	
115SN 149				9.070 (43/2-)	149

S-p	=	8.753	(0.000)	-----	
S-n	=	7.545	(0.000)	-----	
S-2p	=	15.568	(0.000)	-----	
S-2n	=	17.848	(0.002)	-----	
S-alpha	=	3.207	(0.000)	-----	

S+p	=	-4.077	(0.005)		
S+n	=	-9.563	(0.000)		
S+2p	=	-9.640	(0.013)		
S+2n	=	-16.507	(0.000)		
S+alpha	=	0.426	(0.007)		

gap p	=	4.676	(0.005)		
gap n	=	-2.018	(0.000)		
gap 2p	=	5.929	(0.013)		
gap 2n	=	1.342	(0.002)		
gap alpha	=	3.633	(0.007)		