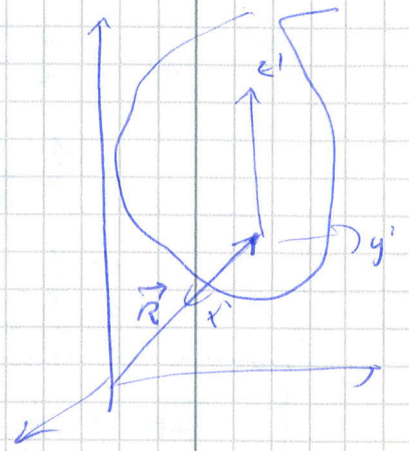


Now consider the kinetic energy (free rigid body)

$$\begin{aligned}
 T &= \frac{1}{2} \sum_i \Delta m_i \dot{\vec{r}}_i^2 \\
 &= \frac{1}{2} \sum_i \Delta m_i (\dot{\vec{R}} + \dot{\vec{r}}_i')^2 \\
 &= \frac{1}{2} \sum_i \Delta m_i (\dot{\vec{R}} + \vec{\omega} \times \vec{r}_i')^2 \\
 &= \frac{1}{2} \sum_i \Delta m_i \left\{ \dot{\vec{R}}^2 + 2 \vec{R} \cdot \Delta m_i (\vec{\omega} \times \vec{r}_i') \right. \\
 &\quad \left. + \frac{1}{2} \sum_i \Delta m_i (\vec{\omega} \times \vec{r}_i') (\vec{\omega} \times \vec{r}_i') \right\}
 \end{aligned}$$



$$= T_1 + T_2 + T_3$$

$$\begin{aligned}
 \vec{R} = \vec{R}_{cm} \\
 T_1 &= \frac{1}{2} \sum_i \Delta m_i R_{cm}^2 = \frac{1}{2} M R_{cm}^2 \quad \text{CoM translation}
 \end{aligned}$$

$$T_2 = \sum_i \vec{R} \cdot (\vec{\omega} \times \Delta m_i \vec{r}_i') = \vec{R} \cdot (\vec{\omega} \times M \vec{R})$$

= 0 in CoM frame
rot.
(cf. symmetry discussion)

$$\Rightarrow T = T_3 = \frac{1}{2} \sum_i \Delta m_i (\vec{\omega} \times \vec{r}_i') (\vec{\omega} \times \vec{r}_i') \quad \text{rot. around CoM}$$

$$\text{if } \vec{R} \neq \text{fixed} \quad T_1 = T_2 = 0 \quad (\vec{R} \text{ would be on rotational axis})$$

$$T = T_{rot}$$

$$\begin{aligned}
 \underbrace{(\vec{\omega} \times \vec{r}_i')}_a \underbrace{(\vec{\omega} \times \vec{r}_i')}_b \cdot \vec{c} &= -\vec{r}_i' \cdot (\vec{\omega} \times \vec{r}_i') \cdot \vec{\omega} = -\vec{r}_i' \cdot \vec{\omega} \cdot \vec{\omega} \\
 &= \vec{r}_i' \cdot ((\vec{\omega} \times \vec{r}_i') \times \vec{\omega}) = -\vec{r}_i' \cdot (\vec{\omega} \times (\vec{\omega} \times \vec{r}_i')) \\
 &= -\vec{r}_i' \cdot (\vec{\omega} (\vec{\omega} \cdot \vec{r}_i') - \omega^2 \vec{r}_i') \\
 &= -(\vec{\omega} \cdot \vec{r}_i')^2 + \omega^2 r_i'^2
 \end{aligned}$$

$$\Rightarrow T_{rot} = \frac{1}{2} \sum_i \Delta m_i (\omega^2 r_i'^2 - (\vec{\omega} \cdot \vec{r}_i')^2) \quad \omega^2 = \vec{\omega} \cdot \vec{\omega} = \sum_a \omega_a^2$$

$$= \frac{1}{2} \sum_i \Delta m_i (\omega_a^2 r_{ia}^2 - \sum_{ab} \omega_a \omega_b r_{ia} r_{ib})$$

$$\omega^2 = \sum_a \omega_a^2 = \sum_{ab} \omega_a^2 \delta_{ab} = \sum_{ab} \omega_a \omega_b$$

$$\Rightarrow T_{rot} = \frac{1}{2} \sum_i \Delta m_i \sum_{ab} \left(r_i^2 \delta_{ab} \omega_a \omega_b - r_{ia} r_{ib} \omega_a \omega_b \right)$$

$$= \frac{1}{2} \sum_{ab} \omega_a \left(\sum_i \Delta m_i (r_i^2 \delta_{ab} - r_{ia} r_{ib}) \right) \omega_b$$

$$\equiv \frac{1}{2} \sum_{ab} \omega_a \hat{I}_{ab} \omega_b$$

$$T_{rot} = \frac{1}{2} \vec{\omega}^T \hat{I} \vec{\omega}$$

$$\hat{I} = \sum_i \Delta m_i (r_i^2 \delta_{ab} - r_{ia} r_{ib})$$

use x_i for consistency?
 I_{aa} : mom. of inertia around axis
 I_{ab} : deviator of moment
moment of inertia tensor

Make it continuous:

$$I = \int_{M_{solid}} dm (r^2 \delta_{ab} - r_a r_b)$$

$$= \int_{V_{solid}} d^3 r \rho(\vec{r}) (r^2 \delta_{ab} - r_a r_b)$$

$$dm = \rho dV = \sigma dA = \lambda dl$$

↑
volume density

↑
surface/area density
(thin plate, hollow cylinder)

↑
linear mass density
(thin rod, wire)

Do this first

\hat{I} transforms ~~like a vector~~ under rotations ~~analog~~ in a specific way, since it's made of position vectors!

$$\hat{I}'_{ab} = \sum_i R_{ai} R_{bj} \hat{I}_{ij} = (R \hat{I} R^T)_{ab}$$

What happens to T_{rot} ? $\vec{\omega} \rightarrow R \vec{\omega}$ so

$$T_{rot} = \frac{1}{2} \vec{\omega}'^T \hat{I}' \vec{\omega}' = \frac{1}{2} \vec{\omega}^T R^T R \hat{I} R^T R \vec{\omega} = \frac{1}{2} \vec{\omega}^T \hat{I} \vec{\omega}$$

More general: shift in coordinates / axes.

$$I_{ab} = \int dm r^2 s_{ab} - r_a r_b$$

$$s_a = D_a + r_a$$

$$\vec{s} = \vec{D} + \vec{r}$$

$$= \int dm (s^2 + D^2 + 2\vec{s} \cdot \vec{D}) s_{ab} - s_a s_b - D_a D_b + s_a D_b + s_b D_a$$

In general, we can always diagonalize \hat{I} . This defines a special coordinate system whose axes are the principal axes of the solid:

$$\hat{I} = \begin{pmatrix} A & & \\ & B & \\ & & C \end{pmatrix} \text{ etc.}$$

To find the moment of inertia w.r.t. a fixed axis,

first we

$$T_{rot} = \frac{1}{2} I \omega^2 = \frac{1}{2} \sum_{ab} \left(\int dm r_a r_b \right) \omega_a \omega_b$$

$$\vec{n} = \frac{\vec{\omega}}{|\vec{\omega}|}$$

$$\Rightarrow \vec{\omega} = \omega \vec{n}$$

$$\vec{\omega} = \omega \cdot \vec{n}$$

\Rightarrow

$$T_{rot} = \frac{1}{2} \omega^2 \vec{n}^T \cdot \hat{I} \vec{n}$$

$$= \frac{1}{2} \omega^2 \left(\sum_{ab} n_a \hat{I}_{ab} n_b \right)$$

$$\equiv I$$

moment of inertia around $\vec{\omega}$

→ rotational kinetic energy is invariant under rotations

→ scalar!

→ \hat{I} is a rank 2 tensor! $\vec{\omega}$ is a vector
(~~vector~~)

• \hat{I} depends on choice of tagged point.
(will lead to Steiner's theorem)

$$\hat{I}_{ab} = \int \lambda (r_i^2 \delta_{ab} - r'_a r'_b) dl$$

$$\lambda = \frac{M}{2\pi R}$$

$$x' = R \cos \phi'$$

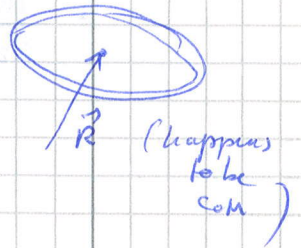
$$y' = R \sin \phi'$$

$$z' = 0$$

$$\Rightarrow I_{xx'} = \frac{M}{2\pi R} \int_0^{2\pi} (R^2 - R^2 \cos^2 \phi) R d\phi =$$

$$= \frac{M}{2\pi R} R^2 \int_0^{2\pi} \sin^2 \phi d\phi = \frac{MR^2}{2\pi} \cdot \frac{1}{2\pi} \int_0^{2\pi} \sin^2 \phi d\phi = \frac{1}{2} MR^2$$

$$= \frac{1}{2} \int_0^{2\pi} \sin^2 \phi d\phi$$



analogous for $I_{yy'}$;

$$I_{yy'} = \frac{M}{2\pi} R^2 \int_0^{2\pi} \cos^2 \phi' d\phi' = MR^2$$

(→ analogous for hollow cylinders)

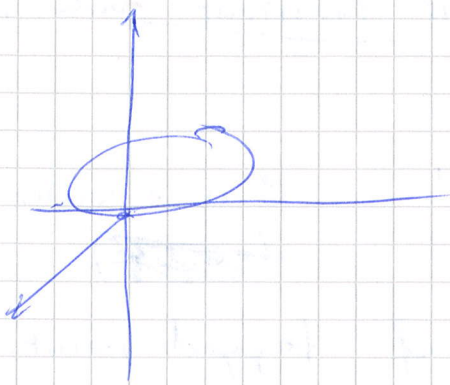
$$I_{xy'} = \frac{M}{2\pi R} R \int_0^{2\pi} (-R^2 \sin \phi \cos \phi) d\phi = 0$$

$= \frac{1}{2} \sin 2\phi$

$I_{xz'}$, $I_{yz'}$ trivially zero

$$\hat{I} = \begin{pmatrix} \frac{1}{2} MR^2 & 0 & 0 \\ 0 & \frac{1}{2} MR^2 & 0 \\ 0 & 0 & MR^2 \end{pmatrix}$$

→ diag because of symmetry & com system.



rotak around point on z
axis.

$$\begin{aligned}x' &= R \cos \phi' \\y' &= R \sin \phi' + R \\z' &= 0\end{aligned}$$

$$\Rightarrow r'^2 = 2R^2(1 + \sin^2 \phi')$$

$$\hat{I}_{xx} = \frac{m}{2\pi R} R \int_0^{2\pi} d\phi' \left[2R^2(1 + \sin^2 \phi') - R^2 \cos^2 \phi' \right]$$

$$= \frac{m}{2\pi} \left(\int_0^{2\pi} d\phi' R^2(1 - \cos^2 \phi') \right)$$

$$\begin{aligned}R^2 \cos^2 \phi' \\+ R^2 \sin^2 \phi' \\+ 2R^2 \sin \phi' \\+ R^2\end{aligned}$$

$$+ \int_0^{2\pi} d\phi' R^2(1 + \sin^2 \phi')$$

$$= \frac{m}{2\pi} \left(\pi R^2 + 2\pi R^2 + R^2 \underbrace{\int_0^{2\pi} d\phi' \sin^2 \phi'}_{=0} \right) = \frac{3}{2} m R^2$$

$$I_{yy} = \frac{1}{2} m R^2 \int_0^{2\pi} d\phi' 2R^2(1 + \sin^2 \phi') - (R^2 \sin^2 \phi' + 2R^2 \sin \phi' + R^2)$$

$$= \frac{m}{2\pi R} \int_0^{2\pi} d\phi' R^2(1 - \sin^2 \phi') = \frac{1}{2} m R^2 \quad \text{as before}$$

$$I_{zz} = 2mR^2$$

$$I_{xy} = I_{yz} = I_{xz} = 0$$

$$\Rightarrow \hat{I} = \begin{pmatrix} \frac{3}{2} m R^2 & & \\ & \frac{1}{2} m R^2 & \\ & & 2mR^2 \end{pmatrix} = \hat{I}_{cm} + \begin{pmatrix} mR^2 & & \\ & 0 & \\ & & mR^2 \end{pmatrix}$$

with \leftarrow get back to that