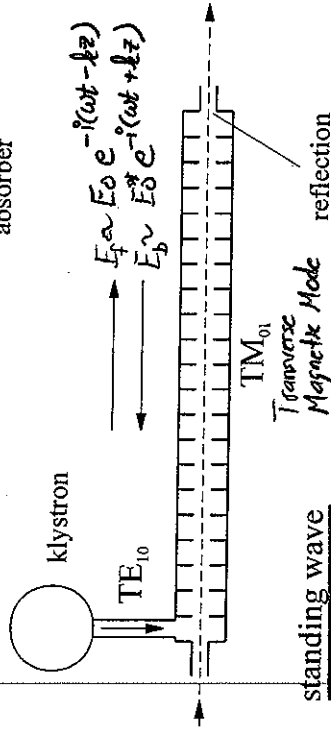
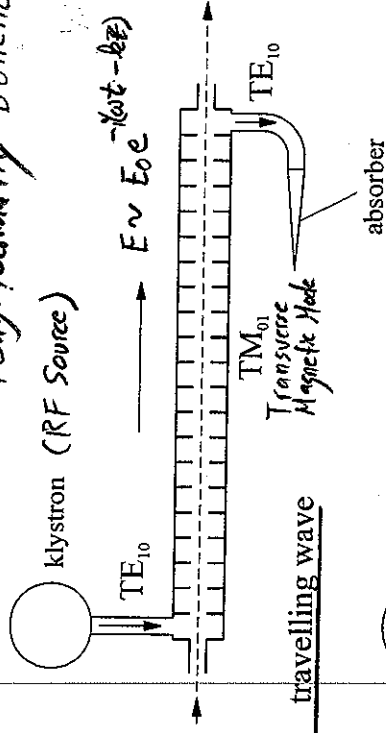


Longitudinal Physics: Beam Acceleration

Different technologies can be employed for beam acceleration

RF: Radio Frequency EM Waves  
 Tuned to resonate with beam.  
 that is longitudinally bunched.



standing wave

The two modes of operation of the linac structure. The upper diagram shows the more commonly used travelling wave mode in which an absorber is installed at the end of the structure to prevent reflections. In the second case the wave is reflected virtually without losses, resulting in a standing wave.

- Two basic schemes!
- 1) Travelling Wave:  $e^-$  machines common
  - 2) Standing Wave: most common  
 Cavities coupled or individually controlled.

Travelling Wave

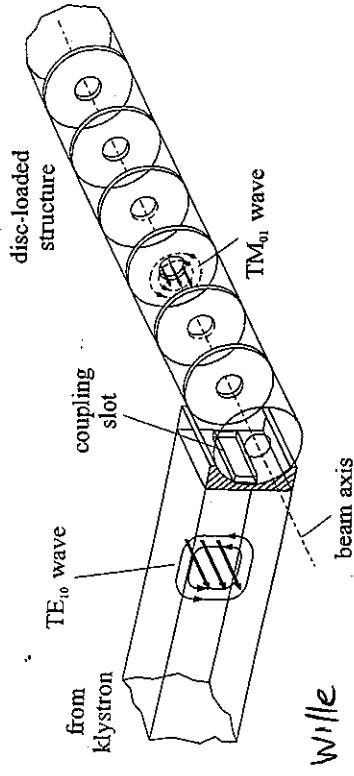


Fig. 5.8 Coupling of the TE<sub>10</sub> waveguide to the linac structure. The transfer of the wave is achieved without reflections via an appropriately sized coupling slot.

Standing Wave

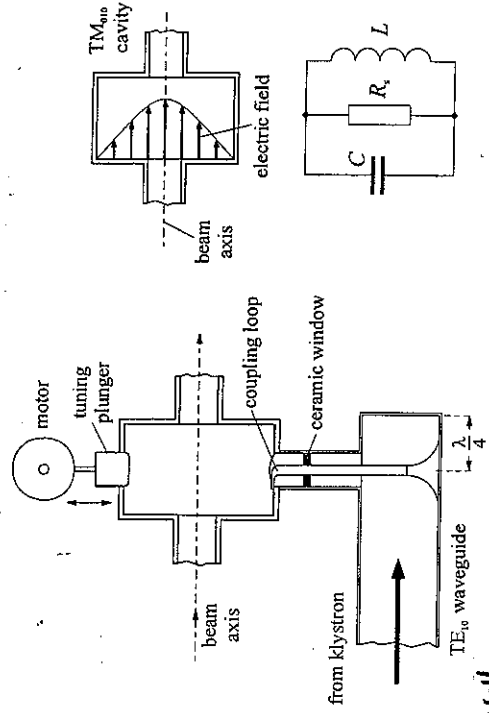


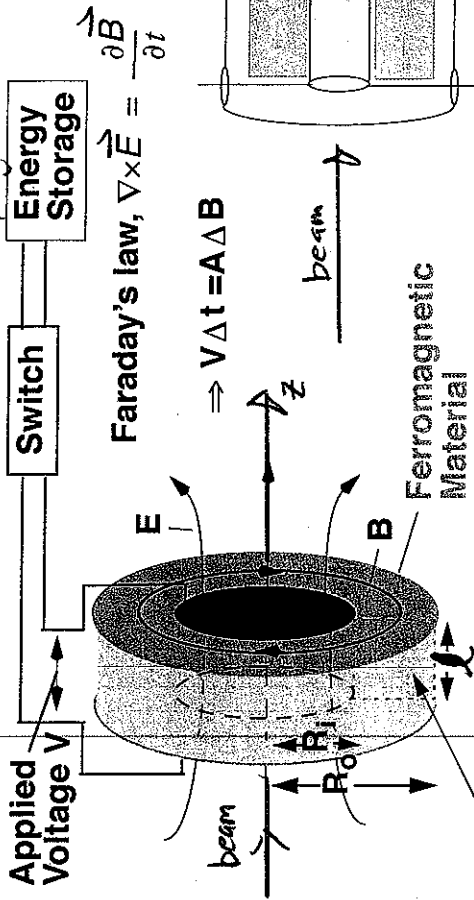
Fig. 5.4 Design of a single-cell accelerating structure using the TM<sub>010</sub> mode. The exact resonant frequency is adjusted using a tuning plunger. The resonator is excited by an inductive coupling loop.

Wille

Induction Acceleration

Beam coupled inductively to a pulsed power source. Operates like a 1:1 transformer. Ferromagnetic core must have sufficient "capacity" (Volt-seconds) to keep voltage from collapsing over pulse duration of beam. Beam pulse can be as long as voltage can be maintained.

Schematic

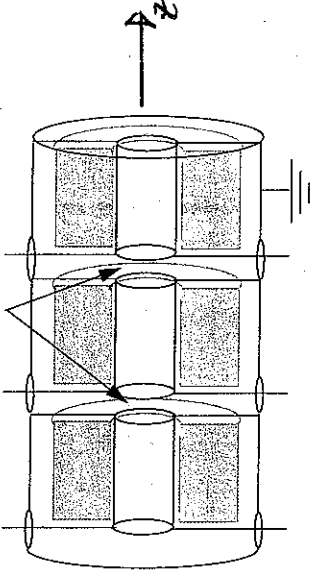


Faraday's law,  $\nabla \times \vec{E} = \frac{\partial \vec{B}}{\partial t}$

$\Rightarrow V \Delta t = A \Delta B$

Longer pulse  $\Rightarrow$  larger cores  $\Rightarrow$  More Volt-sec

Acceleration "gaps"

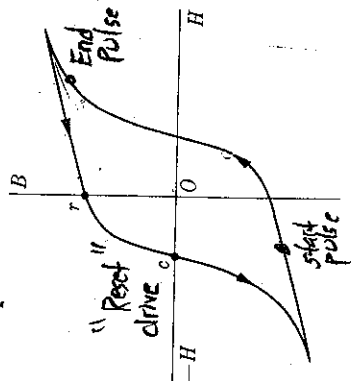
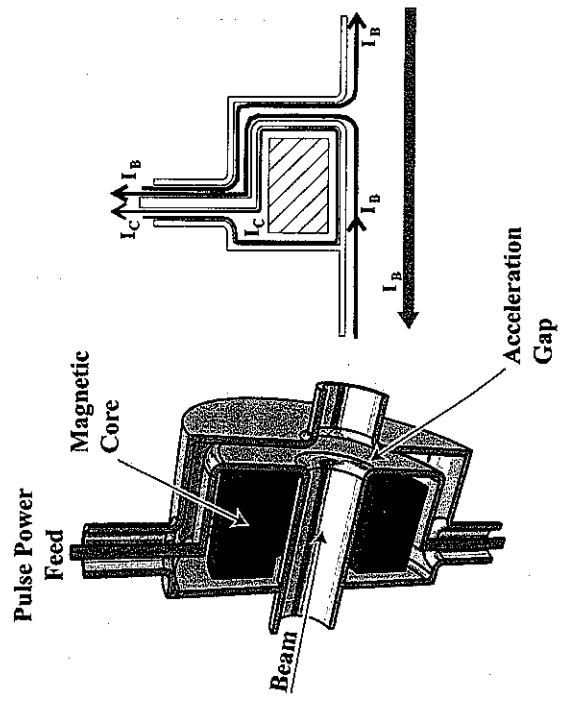


Cross-sectional area A  
 $A = (R_o - R_i) L$

More Realistic Geometry

$\frac{dV}{dz} = (R_o - R_i) \Delta B \left( \frac{\text{Radial Packing Frac}}{\text{Frac}} \right) \left( \frac{\text{Axial Packing Frac}}{\text{Frac}} \right)$   
 $\sim 1 \text{ m} \times 25 \text{ T} \times 0.8 \times 0.8 \sim 1.6 \frac{\text{Volt-sec}}{\text{m}}$

- \* Losses in material heat core + reset time
- $\Rightarrow$  Challenging for Rings or CW = Continuous Wave applications
- \* Easy to shape pulse. Good for low rep rate, high intensity.
- \* Conceptually simple / appealing, and can be efficient, but pulse power control also can be challenge.



"Core reset" to same point on B(H) curve each pulse.

Electrostatic Acceleration

see Livingston and Blewett, "Particle Accelerators" for more info.

Use DC high voltage electric field to accelerate charged particles falling through a potential well. Beam can be continuous or pulsed.

\*  $\Delta E = q \Delta V$      $\Delta V = \text{change in E.S. potential}$   
 $\Delta E = \text{kinetic energy}$

Concept

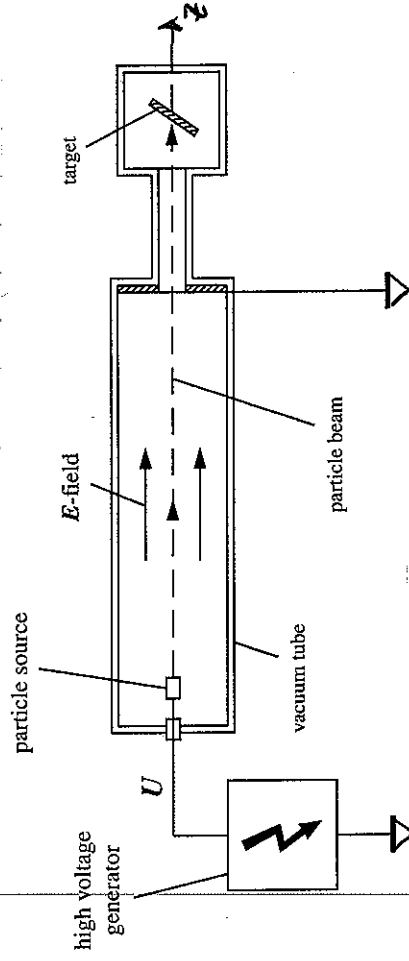
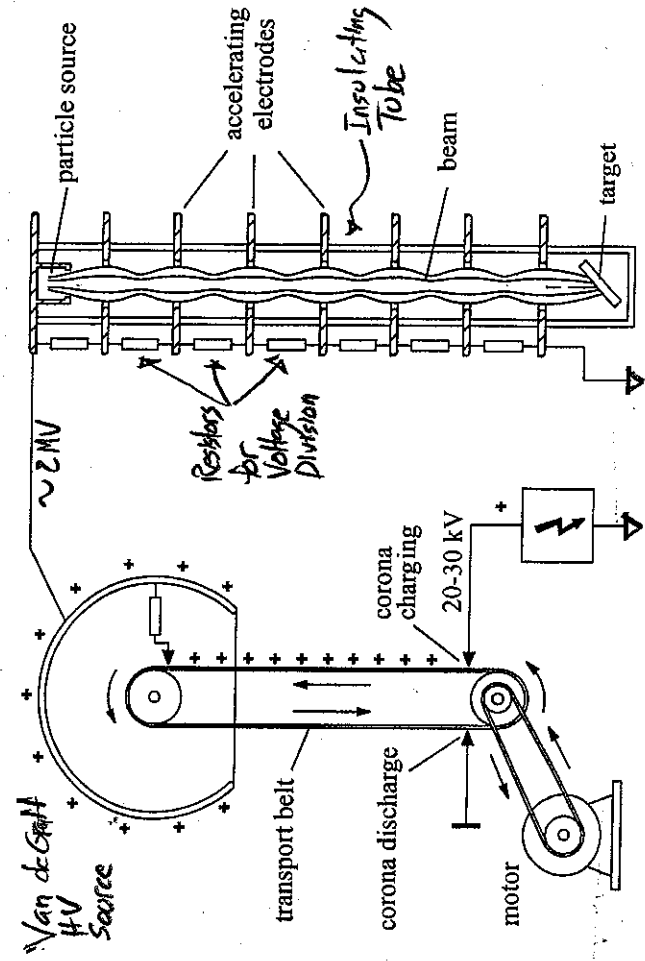


Fig. 1.3 General principle of the electrostatic accelerator.

Wille

closer to Reality!



Wille Fig. 1.7 The Van de Graaff accelerator.

Need DC or long pulse supplies to work!

- Van de Graaff (static electro-mechanical)
- Cockcroft-Walton (AC to DC voltage mult)
- Marx Generator (long pulse)
- ...

Breakdown Scaling

Voltage Holding found to scale  
as (Handbook Accel. Phys., A. Fallens)

$$V_{max} \approx 100kV \begin{cases} \left(\frac{d}{1cm}\right) & d \leq 1cm \\ \left(\frac{d}{1cm}\right)^{1/2} & d > 1cm \end{cases}$$

$d = \text{characteristic distance}$

Scaling can be degraded:

- \* Under "typical" near injector vacuum conditions  $\sim 10^{-7}$  Torr
  - Poor vacuum can degrade.
- \* Assumes steps taken to minimize local peak field.
  - Radsused edges
  - Smooth conductors
- \* Lost particles on conductors or insulators can trigger breakdown.

More Realistic Geometry

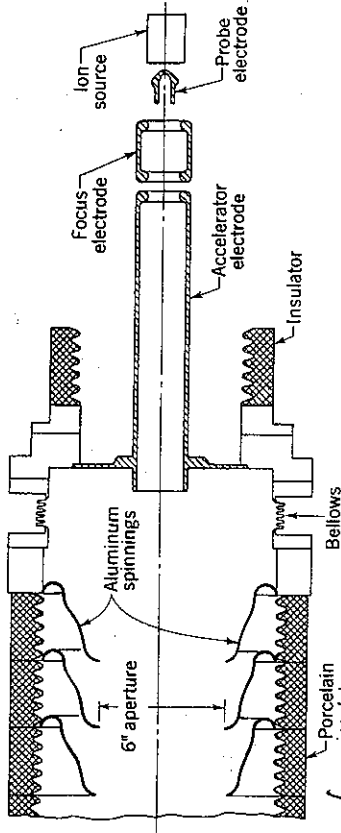


Fig. 3-13. Positive-ion source, focusing electrodes, and accelerating-tube structure for the Brookhaven 4-MV generator.<sup>22</sup>

- \* Gratings and voltage division limit local fields to inhibit electrical breakdown.
- \* Insulators structured to inhibit avalanche breakdown.
- \* Careful attention to details
  - No sharp metal corners near large potential diff.
  - Metal/insulator junctions.

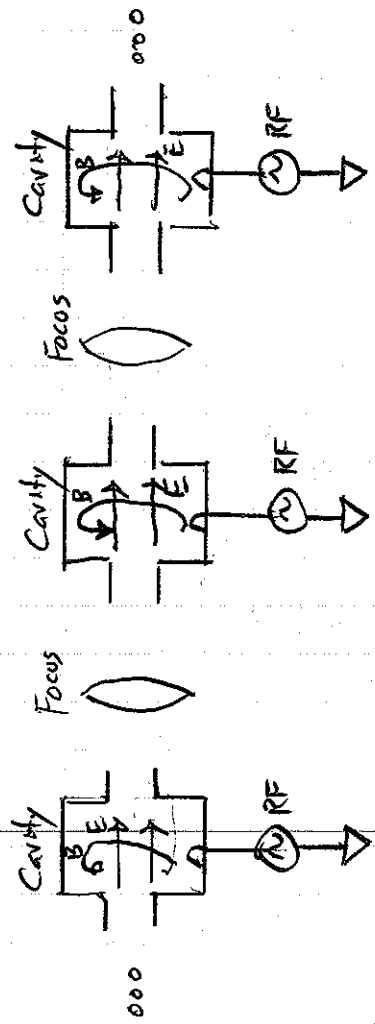
Best Efforts result in only few MV max.

RF Acceleration

We will concentrate primarily on RF acceleration, primarily from the perspective of an RF Linac using resonant cavities. But before proceeding to outline how these works here we frame a range of potential concepts to place in context.

In RF concepts the beam must be longitudinally bunched with bunches maintaining proper synchronism with an oscillating RF wave.

Linear Accelerator with RF Cavities



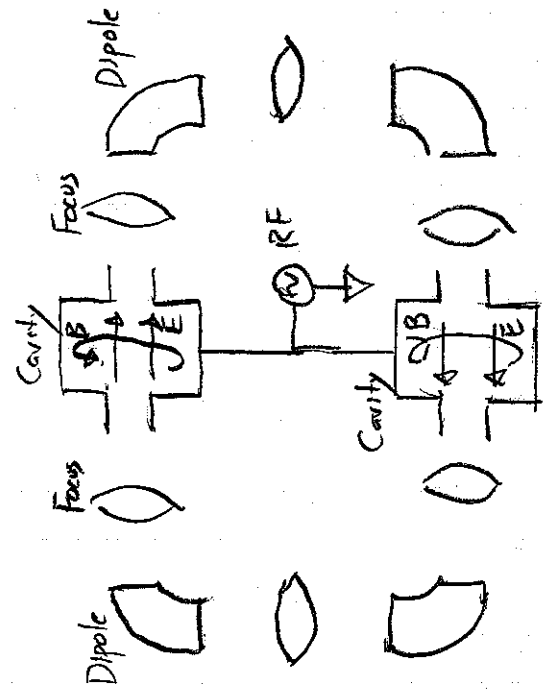
\* Cavities placed where particle transit between cavities is phased for energy gain + longitudinal focusing

\* Transverse focusing provided by optics between cavities.

\* RF sources drive cavities with proper phase control.

- Heavy ions with low  $\beta$  may require individual phase control
- Cavities may also be coupled with established phase relationship.

Circular Accelerator with RF Cavities



\* Cavity phase control (possibly in some high harmonic) setup for energy gain + longitudinal focusing consistent with particle time transit around ring

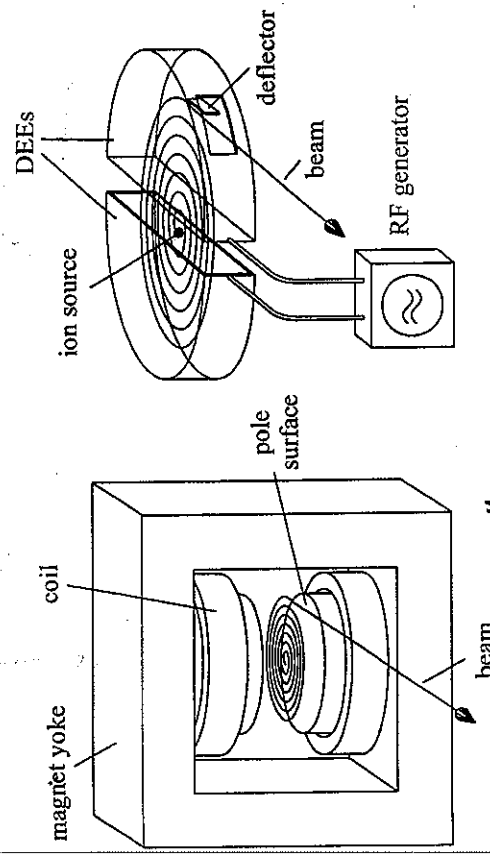
- Path length with  $\beta + slip$  factor must be accounted for

\* Focus + Bending between cavities

\* One or few RF cavities at positions in rings. Cavities have related phase.

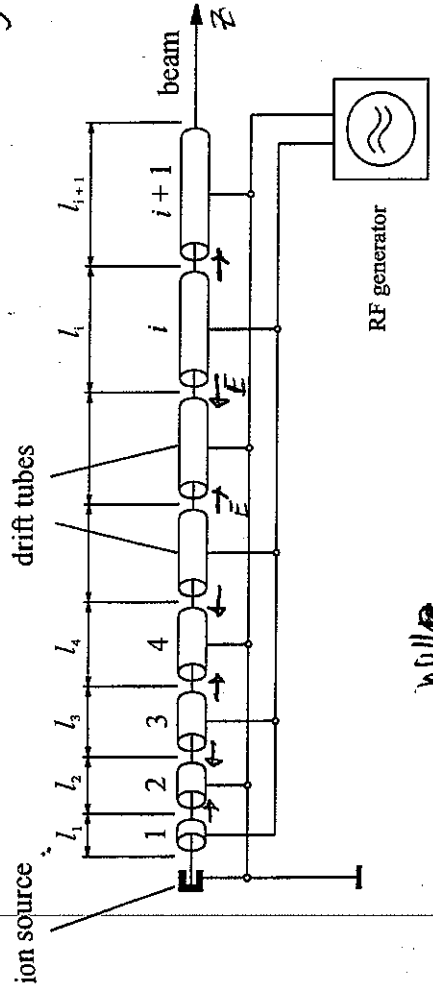
Range of RF Concepts : Very Broad! Only Schematic Outline here.

Cyclotron See Livingston and Blewett, "Particle Accelerators", Chapter 6 for more info.



Willie  
Fig. 1.12 The cyclotron.

Wideröe Linac See historical discussions in many accelerator books: Wiedemann, Conte & McKay, Wangler, etc.



Willie  
Fig. 1.9 Wideröe linear accelerator.

Non-Relativistic:

$$\omega = \frac{qBz}{m} = \text{const}$$

$$\frac{1}{f} = \frac{Bz}{(RF)}$$

p increases  
with energy gain  
till particle  
spirals out to  
deflector.

As particle becomes  
relativistic, synchronism  
will be broken.

- \* Not much focusing possible
- \* Continuous train/bunches possible
- \* Relatively simple.

Already discussed  
1st lectures.

Non-Relativistic

$$W_i = \frac{1}{2} m v_i^2$$

Kinetic Energy

Phase advance  
between gaps

$$\text{Gap Separation } l_i = \frac{2\pi v_i T}{z}$$

$$= \frac{\beta_i c T}{z} = \frac{\beta_i \lambda_{rf}}{z}$$

for resonance acceleration

Wideroe Linac continued

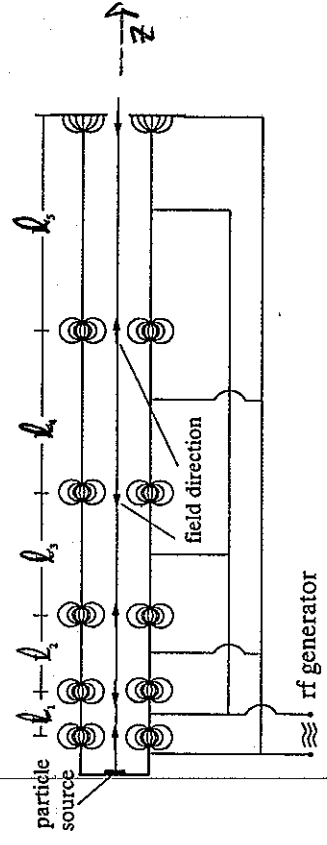


Fig. 2.5. Wideroe linac structure (schematic)  
Widermann

- \* Tubes shield particles from decelerating (wrong phase) RF till they get to the next gap.
- \* Resonance condition established by adjusting the tube length.
- \* Structure is lossy; radiates power.  $\Rightarrow$  Enclose in tube to make cavity  $\Rightarrow$  Alvarez structure.

Alvarez Linac or Drift Tube Linac (DTL)

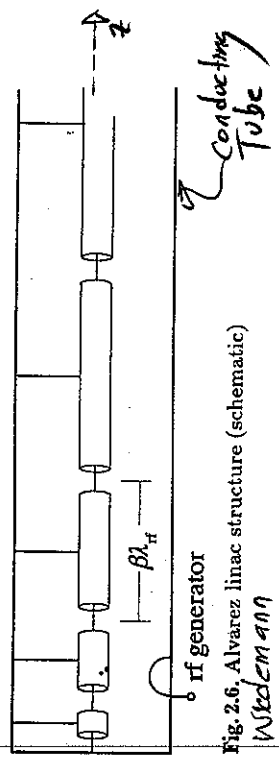


Fig. 2.6. Alvarez linac structure (schematic)  
Widermann

- \* Tube to contain radiation boosts efficiency and allows higher freq. RF
- Can use  $l_1 = \frac{\beta \lambda}{2}$  or  $l_1 = \beta \lambda \pi$
- $\nearrow$  phase advance  $2\pi$  phase advance.
- due to this.

For more info see:

- Widermann, Wille, Wangler,
- Conk & Mackay, Edwards & Syphers
- ....

- \* Still common pre-accelerator for protons/ions from injection to a few hundred MeV  $\beta \approx 0.04 \sim 0.4$
- \* Not used for electrons since  $\beta$  is typically too high from injector

Coupled Cavity Linac See Wangers "RF Linear Accelerators" for more info. 8/

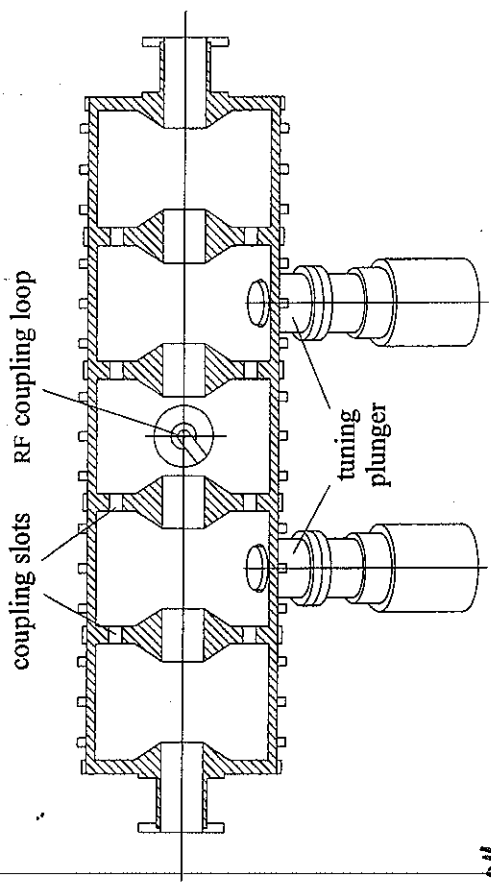


Fig. 5.5 Layout of a five-cell accelerating structure. The power feed is coupled to the middle cell and two tuning plungers are sufficient for the entire structure.

Banks of RF cavities are coupled together to maintain relative RF phase control needed.

- Very common for high  $\beta$  particles.
- Simplifies RF drive and saves cost.
- Many possible geometries.

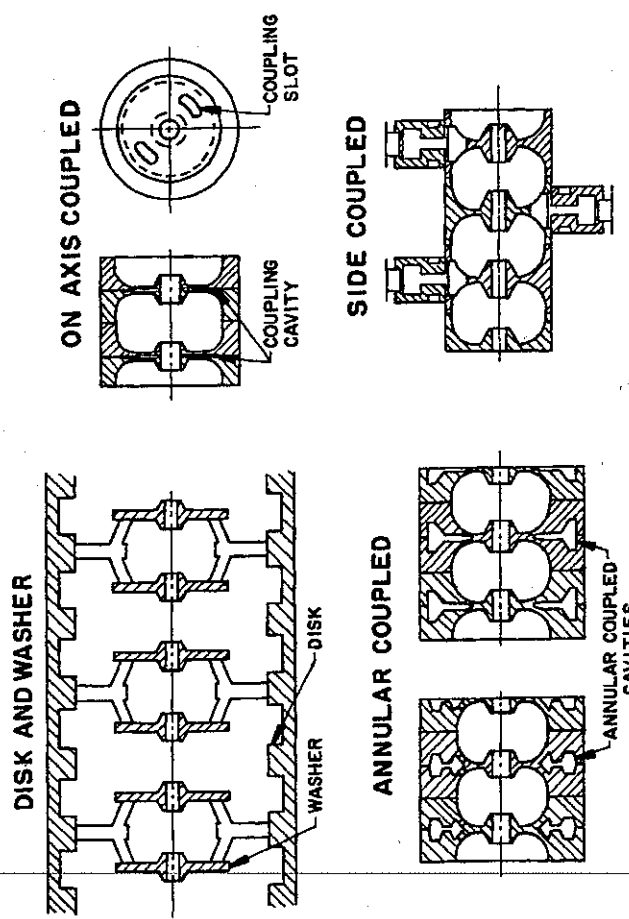


Figure 4.17 Four examples of coupled-cavity linacs.

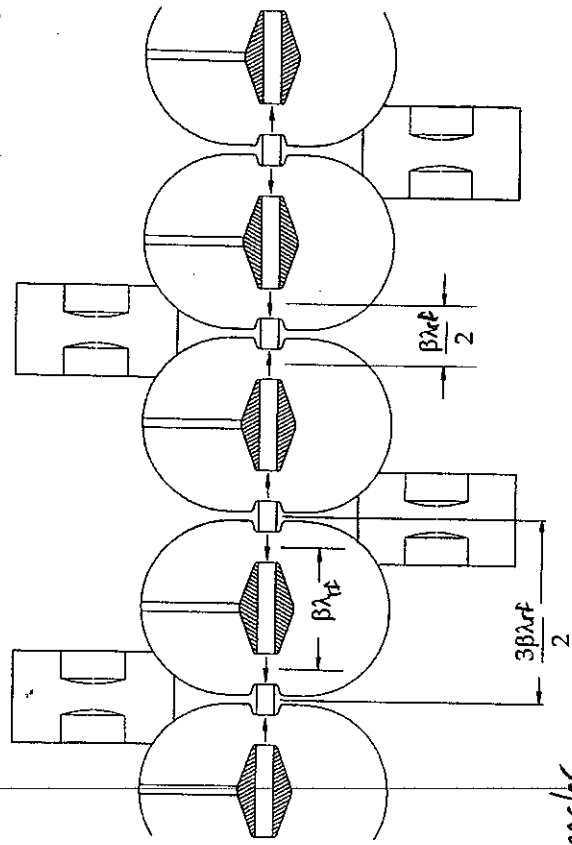
- \* Coupling cavities sometimes in beam line and other times moved off-axis for more efficient packing.
- \* Usually transverse focusing interspersed between banks of coupled RF cavities.

Wanger



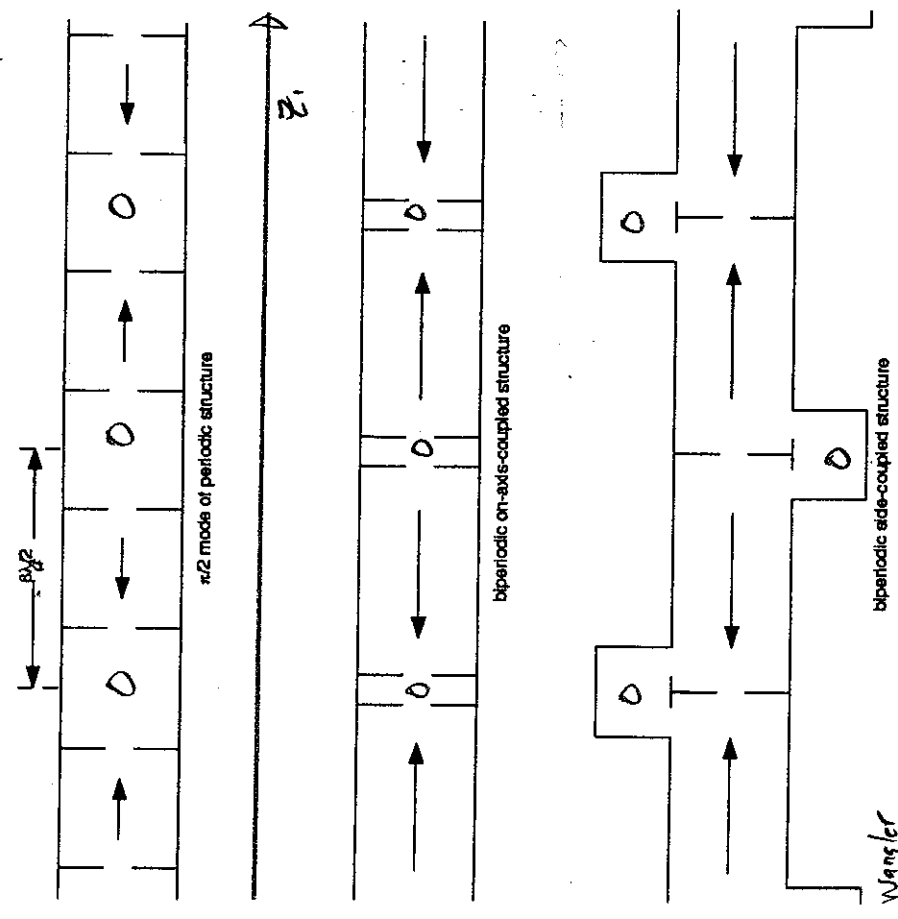
Coupled Cavity Linac

Further examples

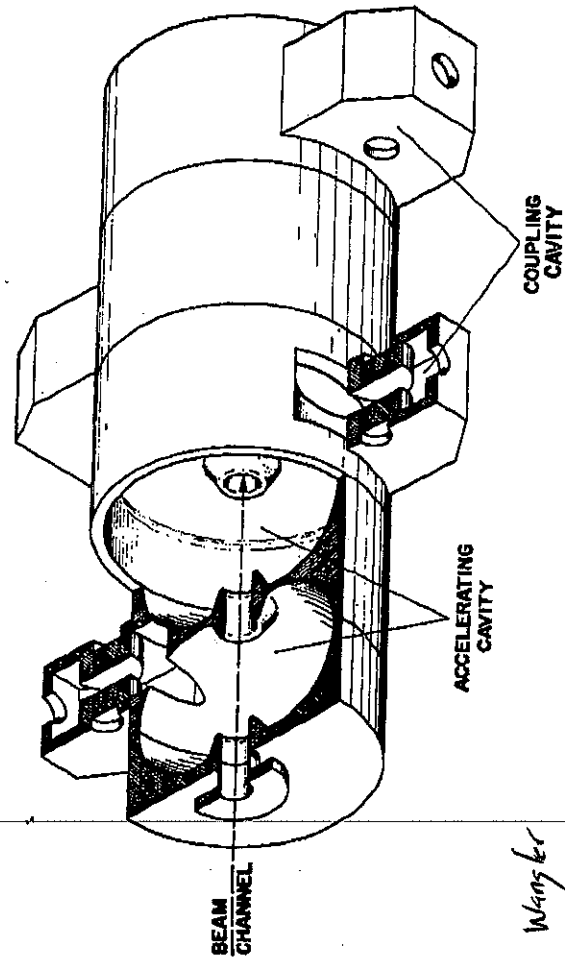


Wangler  
Figure 12.2 Coupled-cavity drift-tube linac (CCDTL) structure with a single drift tube in each accelerating cavity.

Example phase relations of E field between cavities



Wangler  
Figure 4.15  $\pi/2$ -like-mode operation of a cavity resonator chain. From top to bottom are shown a periodic structure in  $\pi/2$  mode, a biperiodic on-axis coupled-cavity structure in  $\pi/2$  mode, and a biperiodic side-coupled cavity in  $\pi/2$  mode.



Wangler  
Figure 4.11 Side-coupled linac structure as an example of a coupled-cavity linac structure. The cavities on the beam axis are the accelerating cavities. The cavities on the side are nominally unexcited and stabilize the accelerating-cavity fields against perturbations from fabrication errors and beam loading.

# Radio Frequency Quadrupole (RFQ)

see Wangler, "RF Linear Accelerators" for more info.

\* Electric quadrupole mode excited in cavity with four quadrupole symmetry vane electrodes.

- Vanes concentrate  $\perp$  E field to provide strong transverse quadrupole (electro) focusing
- Longitudinal ripples of vanes provides  $\parallel$  E field for longitudinal acceleration and focusing.

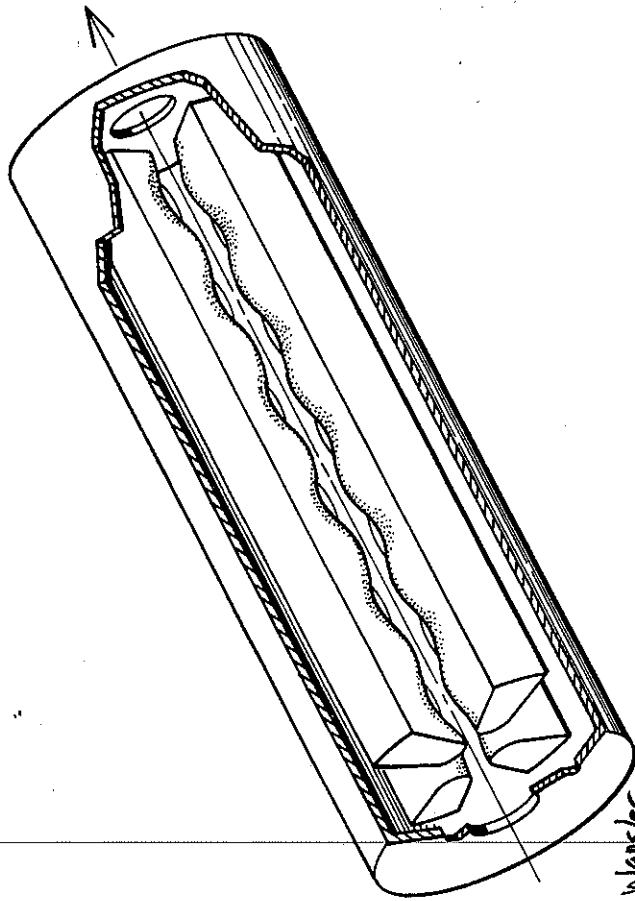
\* Works for  $\beta \approx 0.01 - 0.06$

\* Can be setup to bunch and accelerate a DC injected beam from source to match into required bunch structure of RF accelerator.

- Structure can be tapered to enhance bunching or acceleration. Period  $\beta \dot{t}$  varies with energy gain.

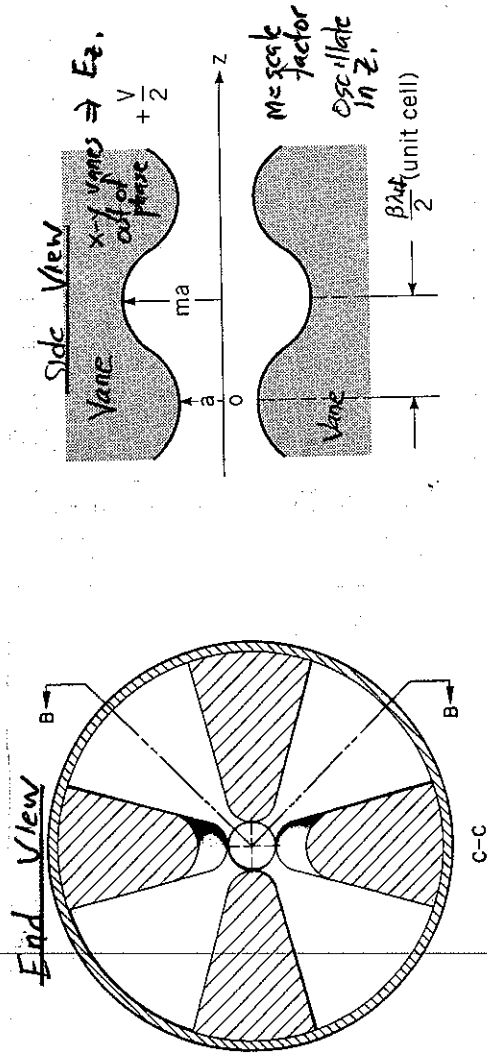
\* Common choice for front ends. - Including FRIB.

\* Not used for electrons since low  $\beta$  structure.



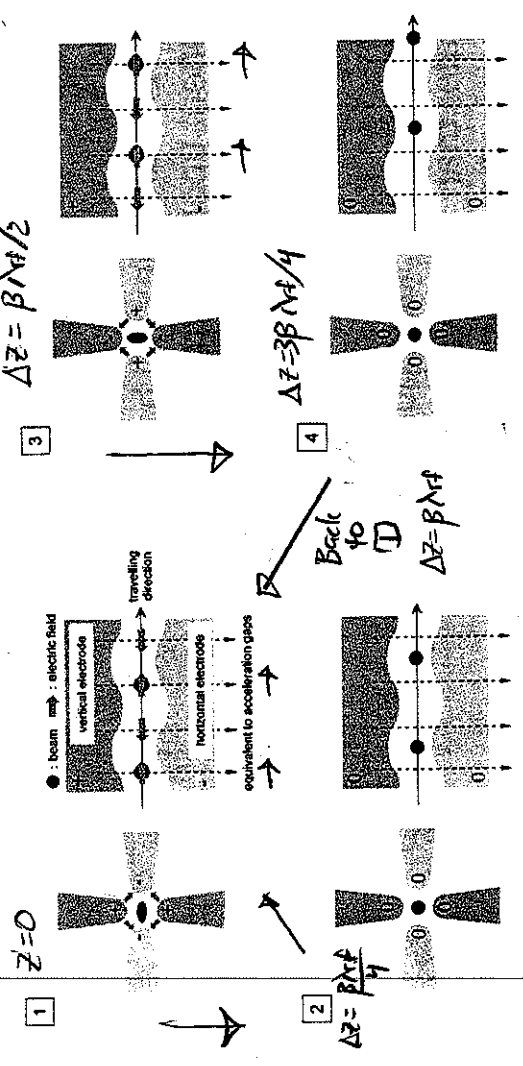
Wangler

Figure 1.7 The radio-frequency quadrupole (RFQ), used for acceleration of low-velocity ions, consists of four vanes mounted within a cylindrical cavity. The cavity is excited in a quadrupole mode in which the RF electric field is concentrated near the vane tips to produce an electric transverse restoring force for particles that are off-axis. The modulation of the vane tips produces a longitudinal electric-field component that accelerates the beam along the axis.



Schematic on how an RFQ works! M. Syphers, USPAS Notes.

# The Radio Frequency Quadrupole (RFQ)



Many variants: 4-vanes, 4-rods, Al/Cu, large/small  
 Typical energy range — up to few MeV (protons, ions typically; ~~also electrons~~)

- 1 de Focus x + phase focus  
Focus y from field variation
- 2 Null
- 3 Focus x + phase focus  
de Focus y from field variation
- 4 Null

Where + Electrode closer  
 $\Rightarrow \phi$  on axis +  
 Where - Electrode closer  
 $\Rightarrow \phi$  on axis -

Comments: An RFQ essentially employs AG electric transverse focusing which is strong for low velocity ( $\beta$ ) particles.

$$x'' + \left(\frac{qB}{\beta p}\right)' x' + r x = 0$$

$$r = \left\{ \begin{array}{l} \frac{B'}{(\beta p)} \text{ Magnetic} \\ \frac{E'}{(\beta c)(\beta p)} \text{ Electric} \end{array} \right.$$

extra factor  $\frac{1}{\beta}$  in denominator

$$B' = \frac{\partial B_x}{\partial x} = \frac{\partial B_x}{\partial y} = \text{Magnetic Quad Gradient}$$

$$E' = -\frac{\partial E_x}{\partial x} = \frac{\partial E_y}{\partial y} = \text{Electric Quad Gradient}$$

See Lund, USPAS notes.

# Travelling Wave Linac

see Wangler,

"RF Linear Accelerators" for more info.  
Chapter 3

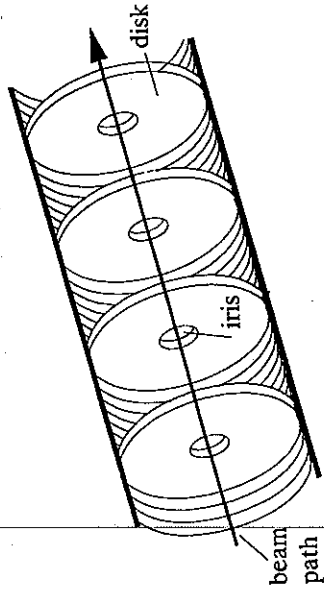
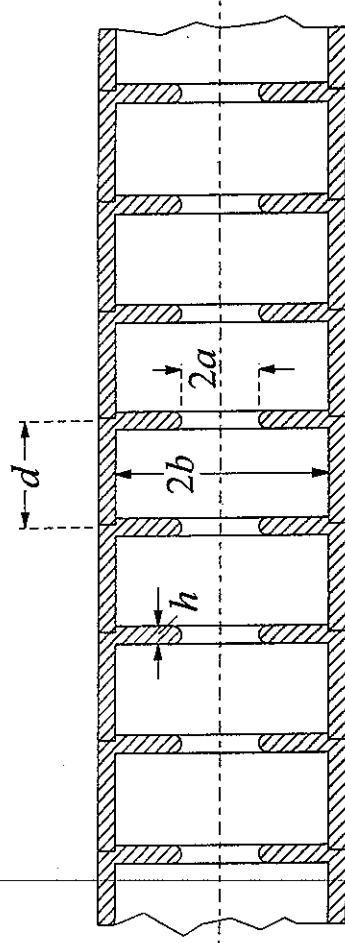


Fig. 2.3. Disk loaded accelerating structure for an electron linear accelerator (schematic) Wilemann



Wille  
Fig. 5.6 Cross-section through a typical linac structure. The phase velocity of the RF wave is reduced to the particle velocity by the insertion of irises.

Why not use a simple waveguide TM mode to have a longitudinal  $E_z$  resonate with beam for acceleration?

Phase velocity of mode  $> c$  so cannot maintain resonance.

But can add periodic structure in waveguide to slow wave and maintain resonance.

- Structure essentially sets up small coupled cavities with part reflections.

- periodic lattice of disks filling cylindrical waveguide commonly used. Example: SLAC electron linac.

Some aspects will be discussed more later:

- Waveguide modes.
- Travelling wave field. to calculate energy gain.

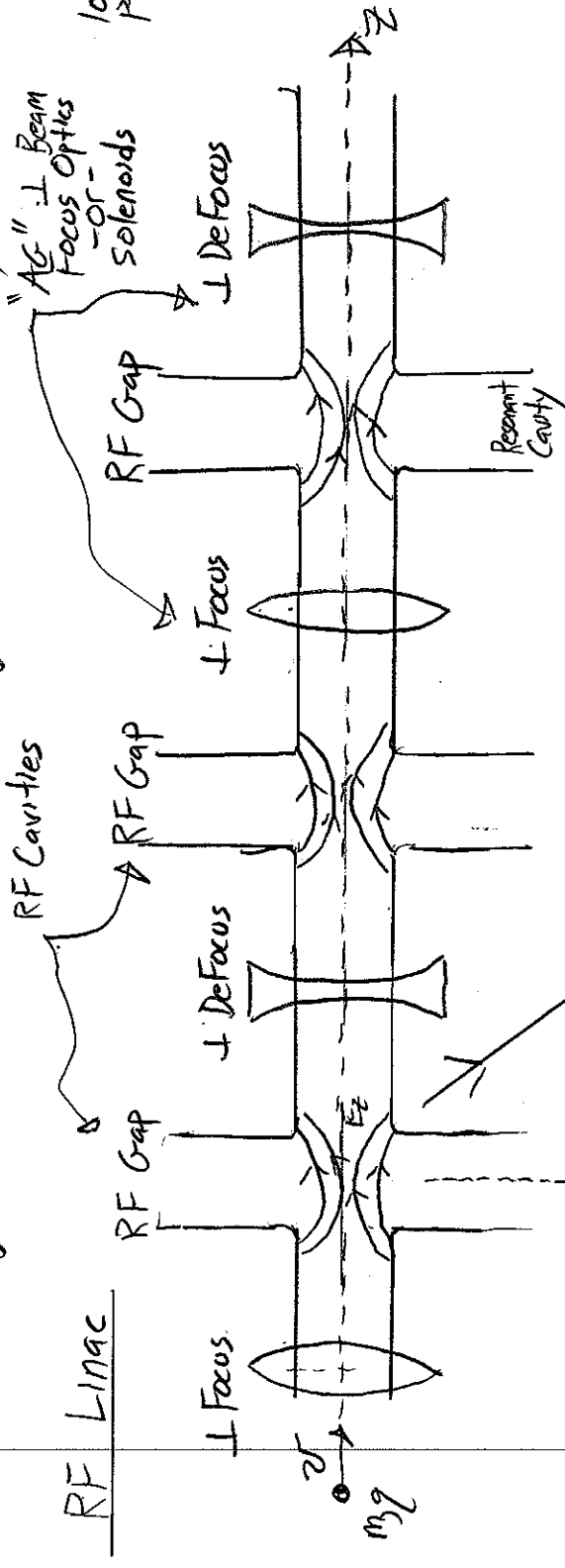
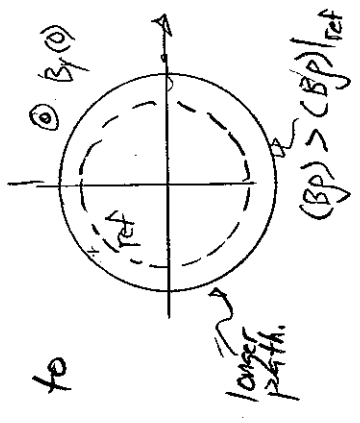
# RF Linear (LINAC) Acceleration

Will follow Wangler "RF Linear Accelerators"

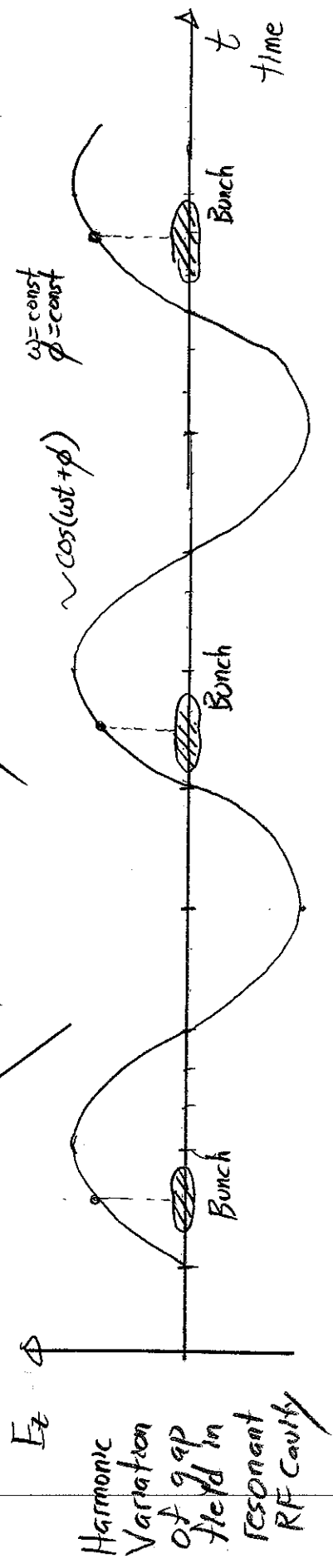
+ info from other sources cited, and Bernard & Lund USPAS

We will first cover RF linacs and then modify the formulation to a form appropriate for rings.

\* Rings require modification of synchronism conditions due to longer path length for larger particle rigidity (BP)

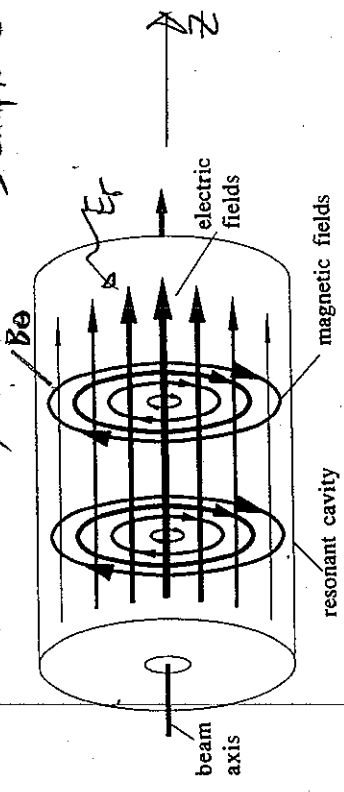


Gap Field in Cavity: all RF "buckets" Filled



RF Cavity Fields  
"All box" Cavity

Wangler, §102  
Corte & Mackey, Chapter 9  
Wiedemann, §20.2  
Wille, Chapter 5

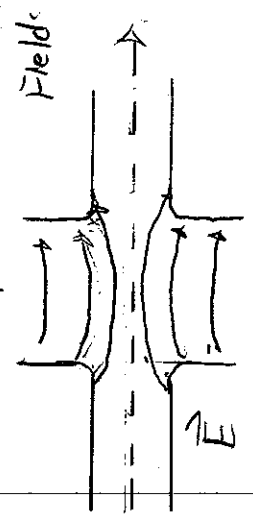
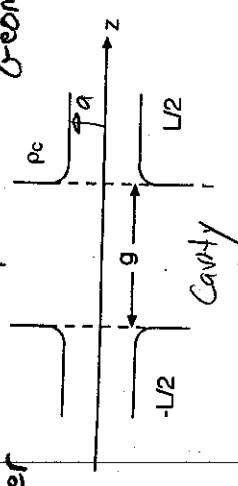


Wiedemann

Structures within the cavity often concentrate the field in an "RF Gap"



Wangler  
Geometry



Simplist Case:

Cavity excited harmonically with a lowest order transverse magnetic mode that primarily generates a longitudinal  $E_z$  for beam acceleration when particles transit at the right phase.

$TM_{010}$  mode shown

- \* Cavities may be coupled (high  $\beta$ ) or independently driven (low  $\beta$ ) with appropriate phase control.
- \* More details on cavities later.

Harmonic  $TM_{010}$  Fields

$\phi = \text{const}$  RF phase  
 $\omega = \text{const}$  RF angular Velocity

$$E_z(r, z, t) = E_z(r, z) \cos(\omega t + \phi)$$

$$B_\theta(r, z, t) = B_\theta(r, z) \sin(\omega t + \phi)$$

$$E_r(r, z, t) = E_r(r, z) \cos(\omega t + \phi)$$

Due to finite beam hole + gap structures

Will discuss cavity fields more later, but for moment motivate form Ok ...

Within cavity (vacuum region)

$$\begin{aligned}
 1) \nabla \cdot \vec{E} &= \frac{\rho}{\epsilon_0} \\
 2) \nabla \times \vec{B} &= \mu_0 \vec{J} + \frac{1}{c} \frac{\partial \vec{E}}{\partial t} \\
 3) \nabla \times \vec{E} &= -\frac{\partial \vec{B}}{\partial t} \\
 \nabla \cdot \vec{B} &= 0
 \end{aligned}$$

$$\begin{aligned}
 E_z(r, z, t) &= E_z(r, z) \cos(\omega t + \phi) \\
 B_\theta(r, z, t) &= B_\theta(r, z) \sin(\omega t + \phi) \\
 E_r(r, z, t) &= E_r(r, z) \cos(\omega t + \phi)
 \end{aligned}$$

$$\nabla \cdot \vec{E} = \left[ \frac{1}{r} \frac{\partial}{\partial r} (r E_r) + \frac{\partial E_z}{\partial z} \right] \cos(\omega t + \phi) = 0$$

$$\Rightarrow \frac{1}{r} \frac{\partial}{\partial r} (r E_r) + \frac{\partial E_z}{\partial z} = 0$$

$$\nabla \times \vec{B} = \left[ -\frac{\partial B_\theta}{\partial z} \hat{r} + 0 \hat{\theta} + \frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) \hat{z} \right] \sin(\omega t + \phi)$$

$$= \frac{1}{r} \frac{\partial \vec{E}}{\partial t} = \frac{1}{r} \frac{\partial}{\partial t} \left[ E_r \hat{r} + E_z \hat{z} \right] \sin(\omega t + \phi)$$

$$\Rightarrow \hat{r}: -\frac{\partial B_\theta}{\partial z} = -\omega \frac{E_r}{c^2} \quad \hat{z}: \frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) = -\omega \frac{E_z}{c^2}$$

$$\nabla \times \vec{E} = \left[ 0 \hat{r} + \frac{1}{r} \frac{\partial}{\partial z} (r E_r) \hat{\theta} + 0 \hat{z} \right] \cos(\omega t + \phi)$$

$$= -\frac{\partial \vec{B}}{\partial t} = -\omega \frac{B_\theta}{c} \cos(\omega t + \phi)$$

$$\Rightarrow \frac{1}{r} \frac{\partial}{\partial z} (r E_r) - \frac{\partial E_z}{\partial z} = -\omega \frac{B_\theta}{c}$$

$$4) \nabla \cdot \vec{B} = \frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) = 0 \quad \checkmark \text{ Satisfied}$$

Cavity Field Constraints

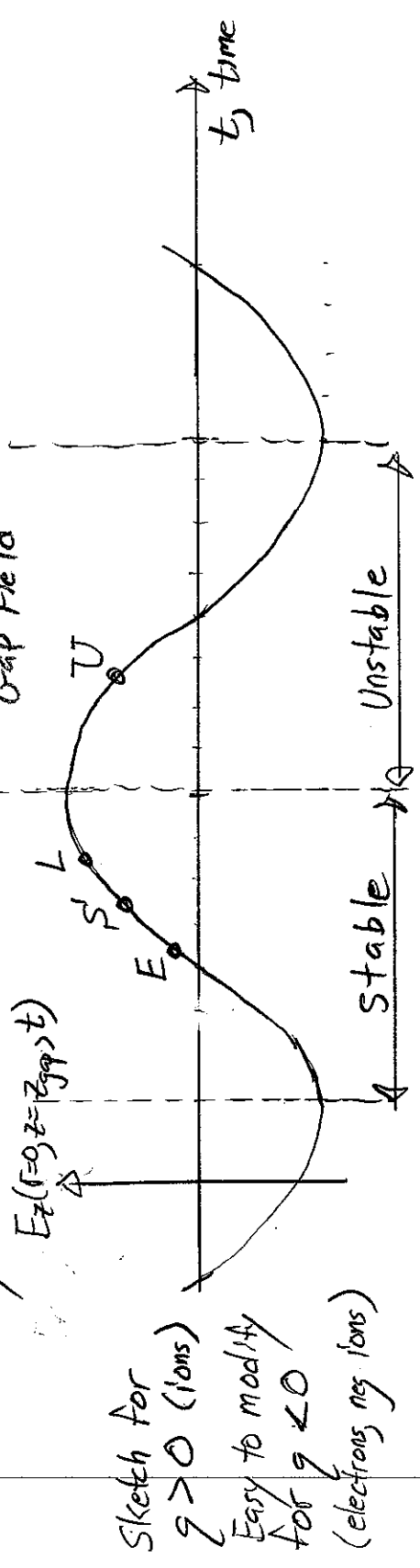
$$\frac{1}{r} \frac{\partial}{\partial r} (r E_r) + \frac{\partial E_z}{\partial z} = 0$$

$$-\frac{\partial B_\theta}{\partial z} = \omega \frac{E_r}{c^2} \quad \frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) = -\omega \frac{E_z}{c^2}$$

$$\frac{\partial E_r}{\partial z} - \frac{1}{r} \frac{\partial}{\partial r} (r E_z) = -\omega \frac{B_\theta}{c}$$

Phase Stability: Basic Idea.

see Wangler, § 1.3.



Sketch for  $q > 0$  (ions)  
Easy to modify for  $q < 0$  (electrons or ions)

Stable on Rising  $E_z$ -Field  $dE_z/dt > 0$

$S'$ : "Synchronous" Particle: Will reach next gap at design time to same position on RF wave.

$E$ : Early: More energetic particle arrives early  
 $E_z$  lower  $\Rightarrow$  less energy gain  $\Rightarrow$  smaller  $v$  increase  
 $\Rightarrow$  moves toward  $S'$  at next gap.

$L$ : Late: Less energetic particle arrives late  
 $E_z$  higher  $\Rightarrow$  more energy gain  $\Rightarrow$  larger  $v$  increase  
 $\Rightarrow$  moves toward  $S'$  at next gap

Unstable on Falling  $E_z$ -Field  $dE_z/dt < 0$

Cases reversed: early 'late' will move away from any design particle choice. at next gap.



Particle Dynamics in Gap

see Wangler's Chapter 2

RF Gap Fields — TM<sub>010</sub> - like excitation

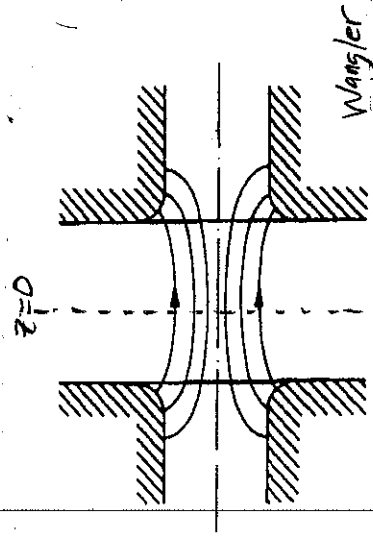


Figure 1.9 Electric-field lines in an accelerating gap.

$$E_z(r, z, t) = E_z(r, z) \cos(\omega t + \phi)$$

$$B_\theta(r, z, t) = B_\theta(r, z) \sin(\omega t + \phi)$$

$$E_r(r, z, t) = E_r(r, z) \cos(\omega t + \phi)$$

Lorentz Force

$$\frac{d\vec{p}}{dt} = q \vec{E} + q \vec{v} \times \vec{B}$$

$$= q E_r \hat{r} + q E_z \hat{z} - q v_\theta B_\theta \hat{r} + q v_r B_\theta \hat{z}$$

$$\hat{z}: \frac{dp_z}{dt} = q E_z(r, z) \cos(\omega t + \phi) + q v_r B_\theta(r, z) \sin(\omega t + \phi)$$

$$\hat{r}: \frac{dp_r}{dt} = q E_r(r, z) \cos(\omega t + \phi) - q v_\theta B_\theta(r, z) \sin(\omega t + \phi) + F_r$$

Focusing Optics

From ⊥ focusing elements

$$\hat{\theta}: \frac{dp_\theta}{dt} = 0$$

Estimate the kinetic energy gain of a particle in the gap from the on-axis ( $r=0$ ) fields.

$$E_z(r=0, z, t) \equiv E(0, z) \cos(\omega t(z) + \phi)$$

$$B_\theta(r=0, z, t) = 0$$

Will find later  $B_\theta \propto r/r_{cavity}$   
 $\Rightarrow B_\theta$  small on axis of gap of small radial extent in cavity

Insert in equations of motion

$$t(z) = \int \frac{dz}{v(z)} + const$$

\* Ref:  $t=0$  particle at center gap ( $z=0$ )

\*  $v(z) \approx v$  Paraxial Approx

$$t(z) \approx \int_0^z \frac{dz'}{v(z')}$$

Note: At time  $t=0$ ,  $\phi$  is the phase of the E-field relative to the peak value

$$E_z(r=0, z, t=0) = E(0, z) \cos \phi$$

In one gap examined, But will now vary  $\phi$  in other gaps to keep this relation true.

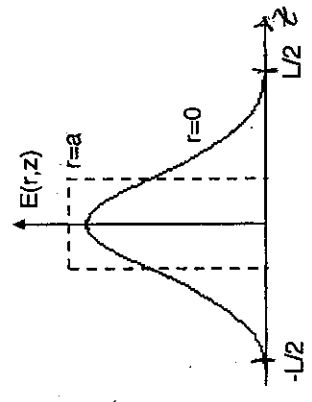


Figure 2.1 Gap geometry and field distribution.

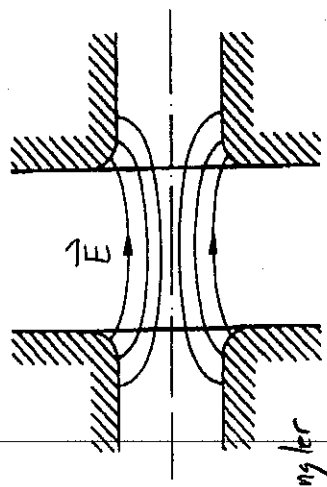


Figure 1.9 Electric-field lines in an accelerating gap.

Wangler

Wangler

Kinetic Energy Gain. See Wangler Chapter 2

$$\boxed{W = (\gamma - 1) mc^2}$$

= Particle Kinetic Energy

\* Use  $W$  = kinetic energy in longitudinal dynamics to be consistent with usual notation.

Denote:

$\Delta W$  = KE gain through gap.

Denote  $E_z(r=0, z) \equiv E(0, z)$

Comment  
Use capital  $W$  for KE to later distinguish from another variable  $w$ .

$$\begin{aligned} \Delta W &= \int_{gap} \vec{E} \cdot d\vec{l} = \int_{-L/2}^{L/2} E(0, z) \cos(\omega t(z) + \phi) dz \\ &= \int_{-L/2}^{L/2} E(0, z) \{ \cos(\omega t(z)) \cos \phi - \sin(\omega t(z)) \sin \phi \} dz \end{aligned}$$

$\hookrightarrow$  some axial length large enough to contain field

$$\begin{aligned} \Delta W &= q V_0 T \cos \phi \\ V_0 &\equiv \int_{-L/2}^{L/2} E(0, z) dz = \text{RF Voltage} \quad [V_0] = eV \\ T &\equiv \frac{\int_{-L/2}^{L/2} E(0, z) \cos(\omega t(z)) dz - \tan \phi \frac{\int_{-L/2}^{L/2} E(0, z) \sin(\omega t(z)) dz}{\int_{-L/2}^{L/2} E(0, z) dz}}{\int_{-L/2}^{L/2} E(0, z) dz} \\ &\equiv \text{Transit-Time Factor} \quad [T] = 1 \end{aligned}$$

Sometimes denote  $\boxed{V_0 \equiv E_0 L}$  to define avg field  $E_0$  over gap field extent  $L$   
\* Important: Specify  $L$  used here or ambiguous!

$$\Rightarrow \Delta W = \int E_0 L T \cos \phi = \text{Panofsky Equation}$$

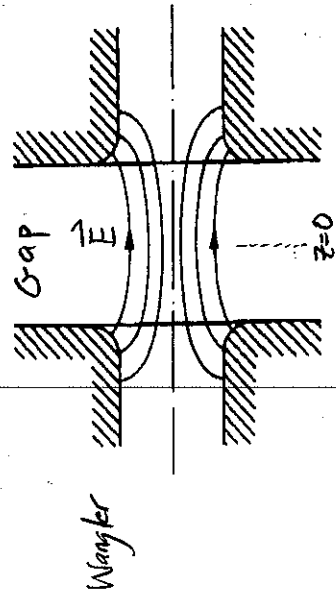
Panofsky eqn is deceptively simple appearing: contains much physics via  $T$ .

Transit Time Wangler, §202

Much physics contained within the transit time factor  $T$ .

\* Time variation of field in gap always reduces energy gain relative to static case; for any RF phase  $\phi$ .

-  $T$  provides normalized measure of reduction;  $T=1 \Rightarrow$  static



$E(z)$  even function of  $z$  in typical gap

$$\Rightarrow \int_{-L/2}^{L/2} E(z) \sin(\omega t(z)) dz \approx 0$$

if change in  $v$  within gap negligible;  $v = \text{const}$

Figure 1.9 Electric-field lines in an accelerating gap.

If  $v \approx \text{const}$  in gap:

$$t(z) = \frac{z}{v} = \frac{z}{v} \omega \Rightarrow \omega t(z) = \frac{\omega z}{v} = \frac{2\pi z}{\beta \lambda v} = \frac{2\pi z}{\beta c \lambda} \lambda f \equiv C \lambda f = \frac{RF}{\text{Wavelength}}$$

Using this

$$T \equiv \frac{\int_{-L/2}^{L/2} E(z) \cos(\omega t(z)) dz}{\int_{-L/2}^{L/2} E(z) dz} - \tan \phi \frac{\int_{-L/2}^{L/2} E(z) \sin(\omega t(z)) dz}{\int_{-L/2}^{L/2} E(z) dz}$$

$$T \approx \frac{\int_{-L/2}^{L/2} E(z) \cos\left(\frac{2\pi z}{\beta \lambda v}\right) dz}{\int_{-L/2}^{L/2} E(z) dz}$$

This formula often found in texts.

Reduced transit-time factor:  
Applicable to most usual situations  
\* Go back to original definition in exceptional cases.

Take a simple approximation for the gap field to illustrate T  
 Constant field in gaps zero outside.

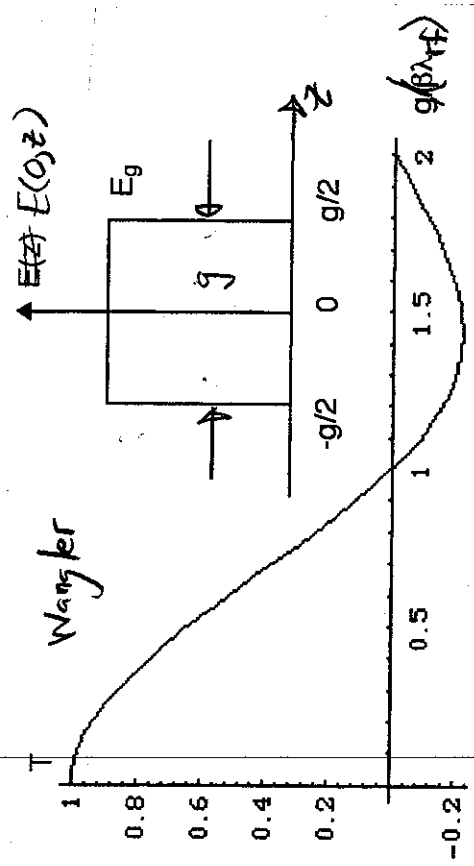


Figure 2.2 Transit-time factor for square-wave electric-field distribution.

Take:  $E(0,z) = E_0 = \text{const}$   
 $L = g$

Then:

$$T = \frac{\int_{-g/2}^{g/2} E(0,z) \cos\left(\frac{2\pi z}{\beta\lambda_{rf}}\right) dz}{\int_{-g/2}^{g/2} E(0,z) dz}$$

$$= \frac{E_0 \int_{-g/2}^{g/2} \cos\left(\frac{2\pi z}{\beta\lambda_{rf}}\right) dz}{E_0 g}$$

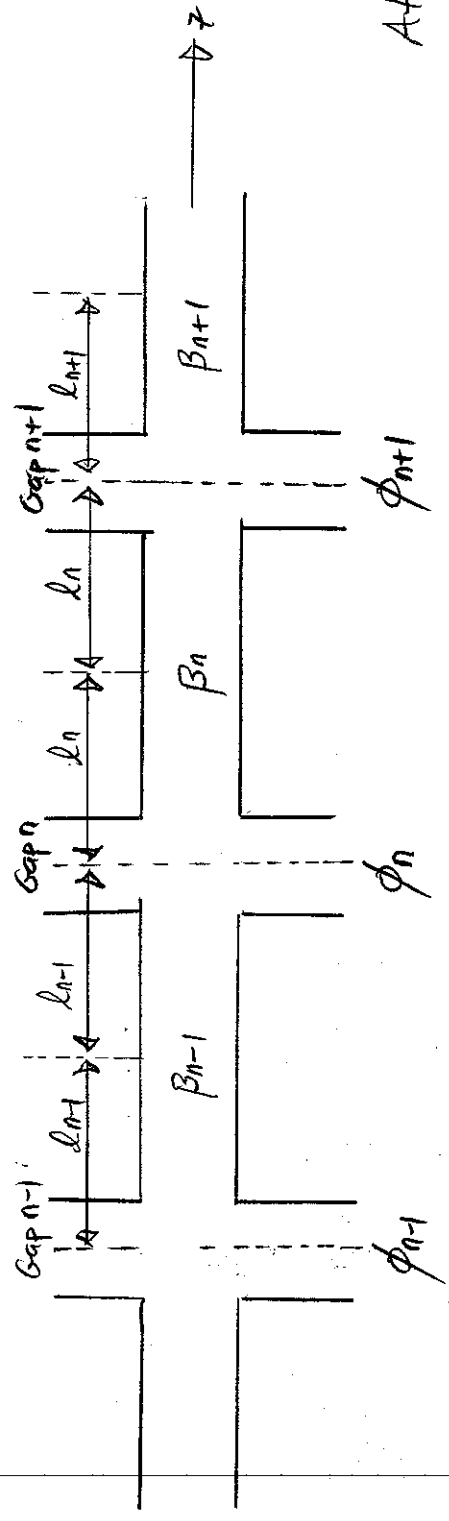
$$T = \frac{\sin\left(\frac{\pi g}{\beta\lambda_{rf}}\right)}{\left(\frac{\pi g}{\beta\lambda_{rf}}\right)}$$

- \*  $T \rightarrow 1$  when  $g \ll \beta\lambda_{rf}$
- Want short gap relative to  $\beta\lambda_{rf}$  for efficient use of RF cavity accelerating potential.
- For electrons or very energetic protons  $\beta \approx 1$  and want  $g \ll \lambda_{rf}$ . Approximation  $T \approx \text{const}$  in gap very good for  $\beta \approx 1$ .

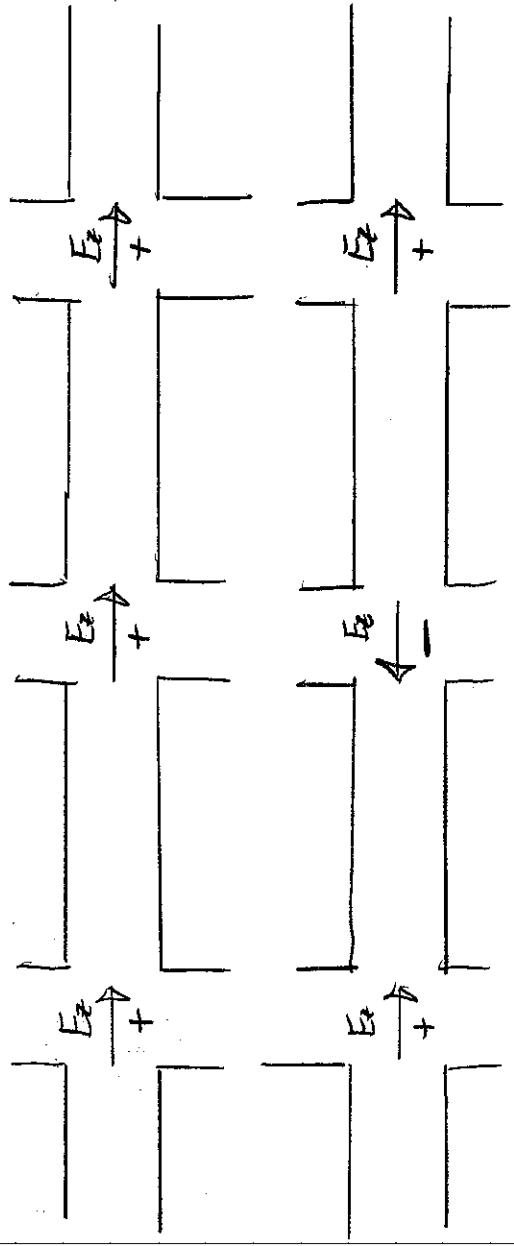
Numerous expressions for T can be found in literature for a variety of cavities under a range of approximations and idealizations. For examples see Wangler. Some cavities have 2 or more gaps that may be lumped into T.

Difference Equations for longitudinal motion in a standing-wave linac  
 Now have parts needed to analyze the longitudinal dynamics.

See Womersley Chapter 6  
 Lund and Barmann  
 USPAS Notes



At time  $t_1$ :



"0" Mode  
 all gap \$E\_z\$ same direction

"\$\pi\$" Mode  
 all neighboring gap \$E\_z\$ opposite direction.

$z_{n-1}$  = distance from z-center  
 nth gap to  $n+1$ 'th gap  
 $B_n = B$  after  $n$ th gap  
 (constant between gaps)

$W_n$  = kinetic energy at  
 end  $n$ th gap (const between  
 gaps)  
 $\phi_n$  = RF phase at z-center  
 each gap.

$\beta_{sn}, W_{sn}, \phi_{sn}$   
 = synchronous  
 (design)  
 particle values

Particle Phase

In gaps  $\Delta t |_{n-1 \rightarrow n} = \frac{(2L_{n-1})}{\beta_{n-1} \cdot c}$

For an arbitrary particle:

$$\phi_n = \phi_{n-1} + \frac{\omega(2L_{n-1})}{\beta_{n-1} c} + \begin{cases} 0 & \text{O-Mode} \\ \pi & \text{\pi-Mode} \end{cases}$$

For the synchronous particle:

$$\phi_{SN} = \phi_{SN-1} + \frac{\omega(2L_{n-1})}{\beta_{SN-1} c} + \begin{cases} 0 & \text{O-Mode} \\ \pi & \text{\pi-Mode} \end{cases}$$

For both cases so  $\phi_{SN} = \phi_{SN-1} \text{ modulo } 2\pi$

$$\Rightarrow (2L_{n-1}) \frac{\omega}{\beta_{SN-1} c} = \begin{cases} 2\pi & \text{O-Mode} \\ \pi & \text{\pi-Mode} \end{cases}$$

But  $\frac{\omega}{c} = \frac{2\pi f}{\lambda_{rf}} = \frac{2\pi}{\lambda_{rf}}$

$$\Rightarrow (2L_{n-1}) = \lambda_{rf} \beta_{SN-1} \begin{cases} 1 & \text{O-Mode} \\ 1/2 & \text{\pi-Mode} \end{cases}$$

Use this to eliminate the inter-gap length ( $2L_{n-1}$ ):

$$\phi_n = \phi_{n-1} + \left(\frac{\omega}{c} \lambda_{rf}\right) \frac{\beta_{SN-1}}{\beta_{n-1}} \cdot \begin{cases} 1 & \text{O-Mode} \\ 1/2 & \text{\pi-Mode} \end{cases} + \begin{cases} 0 & \text{O-Mode} \\ \pi & \text{\pi-Mode} \end{cases}$$

$$\phi_n = \phi_{n-1} + 2\pi \frac{\beta_{S,n-1}}{\beta_{n-1}} \cdot \begin{cases} 1 & \text{O-Mode} \\ 1/2 & \text{PI-Mode} \end{cases} + \begin{cases} 0 & \text{O-Mode} \\ \pi & \text{PI-Mode} \end{cases}$$

For synchronous particle:

$$\phi_{S,n} = \phi_{S,n-1} + 2\pi \frac{\beta_{S,n-1}}{\beta_{S,n-1}} \cdot \begin{cases} 1 & \text{O-Mode} \\ 1/2 & \text{PI-Mode} \end{cases} + \begin{cases} 0 & \text{O-Mode} \\ \pi & \text{PI-Mode} \end{cases}$$

Subtract to measure phase change relative to the synchronous particle going from the n-1'th gap to the n'th gap as:

$$(\phi_n - \phi_{S,n}) - (\phi_{n-1} - \phi_{S,n-1}) = 2\pi \beta_{S,n-1} \left[ \frac{1}{\beta_{n-1}} - \frac{1}{\beta_{S,n-1}} \right] \cdot \begin{cases} 1 & \text{O-Mode} \\ 1/2 & \text{PI-Mode} \end{cases}$$

Denote  $N \equiv \begin{cases} 1 & \text{O-Mode} \\ 1/2 & \text{PI-Mode} \end{cases}$

GIVING

$$(\phi_n - \phi_{S,n}) - (\phi_{n-1} - \phi_{S,n-1}) = 2\pi N \beta_{S,n-1} \left[ \frac{1}{\beta_{n-1}} - \frac{1}{\beta_{S,n-1}} \right]$$

But

$$\beta_{S,n-1} \left[ \frac{1}{\beta_{n-1}} - \frac{1}{\beta_{S,n-1}} \right] = + \left[ 1 - \frac{\beta_{S,n-1}}{\beta_{n-1}} \right] = - \frac{\Delta \beta_{n-1}}{\beta_{S,n-1} + \Delta \beta_{n-1}} \approx - \frac{\Delta \beta_{n-1}}{\beta_{S,n-1}}$$

Phase change rel. to sync particle n-1'th gap to n'th gap.

$$\Delta \beta_n \equiv \beta_n - \beta_{S,n}$$

$$\Delta W = (\gamma - 1) m c^2 \quad \Delta W = \Delta \gamma m c^2 = (1 - \beta^2)^{-3/2} \beta \Delta \beta m c^2 = \gamma^3 \beta m c^2 \Delta \beta$$

$$\gamma = (1 - \beta^2)^{-1/2} \quad \delta = (1 - \beta^2)^{1/2}$$



$$\Delta W_{n-1} \equiv W_{n-1} - W_{s,n-1} \approx \gamma_{s,n-1}^3 \beta_{s,n-1}^2 \Delta \beta_{n-1} \quad (1)$$

Thus

Using these we immediately obtain:

$$\Delta \phi_n - \Delta \phi_{n-1} = -2\pi N \Delta \beta_{n-1} \approx \frac{-2\pi N \Delta W_{n-1}}{\gamma_{s,n-1}^3 \beta_{s,n-1}^2}$$

or

$$\Delta \phi_n - \Delta \phi_{n-1} = -2\pi N \frac{\Delta W_{n-1}}{\gamma_{s,n-1}^3 \beta_{s,n-1}^2} \quad (1)$$

$$\frac{\Delta \phi_n}{\Delta W_n} = \frac{\phi_n - \phi_{s,n}}{W_n - W_{s,n}}$$

Next we apply Panofsky's equation

$$W_n - W_{n-1} = 2 E_{0n} L_n T_n(\beta_n) \cos \phi_n$$

KE energy gain n<sup>th</sup> gap\*  $T_n$  = Transit time factor depends on  $\beta_n$ , but expect little difference between  $T_n$  for  $\beta_n$  and  $\beta_{s,n}$ .

For synchronous particle:

$$W_{s,n} - W_{s,n-1} = 2 E_{0n} L_n T_n(\beta_{s,n}) \cos \phi_{s,n}$$

Subtract

$$(W_n - W_{s,n}) - (W_{n-1} - W_{s,n-1}) = 2 E_{0n} L_n T_n(\beta_{s,n}) [\cos \phi_n - \cos \phi_{s,n}]$$

$$\Delta W_n - \Delta W_{n-1} = 2 E_{0n} L_n T_n(\beta_{s,n}) [\cos \phi_n - \cos \phi_{s,n}] \quad (2)$$

$\Delta$  (Measure)  $\equiv$  Measure - Measures  
 Synchronous

(\*)

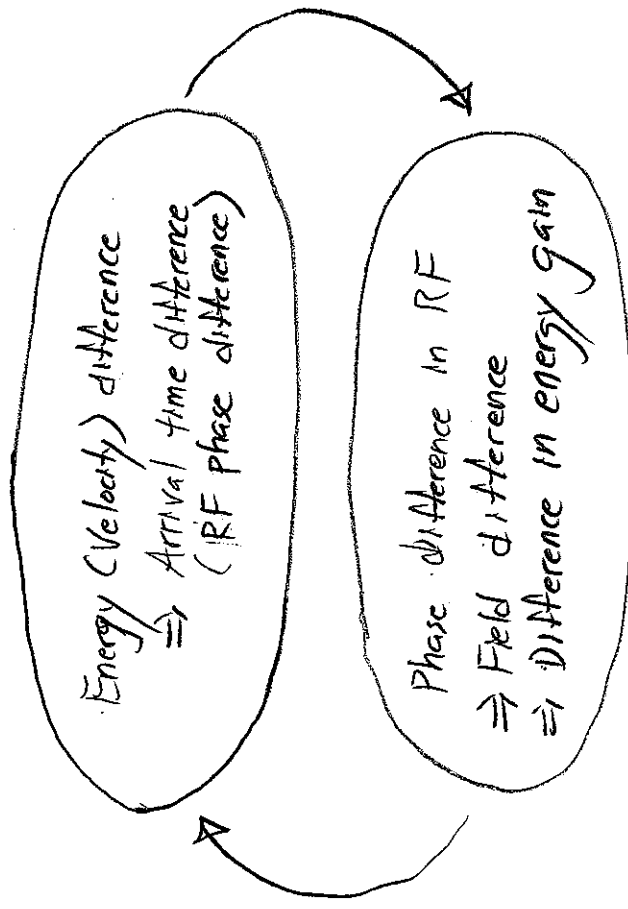
$$(\phi_n - \phi_{s,n}) - (\phi_{n-1} - \phi_{s,n-1}) = \frac{-2\pi N \Delta W_{n-1}}{\beta_{s,n-1}^3 \beta_{s,n}^2 m c^2}$$

$$\Delta W_n - \Delta W_{n-1} = \sum E_{0n} \ln \ln(\beta_{s,n}) [\cos \phi_n - \cos \phi_{s,n}]$$

Difference Equations

System (\*) is a nonlinearly coupled system of difference equations that can be analyzed for the relative phase and energy changes of a particle.

- \* Solve numerically for initial values of  $\phi_n, \Delta W_n$  for specified lattice.
- \* Study phase/stability of longitudinal oscillations about synchronous particle in terms of the evolution of  $\phi$  and  $\Delta W$ .



Difference eqns easy to solve on computer... but insight can be gained by converting to continuous variables and differential eqns for small changes to analyze stability.

\* System should be solved together with the Panofsky equation for the design (synchronous) particle

$$W_{s,n} - W_{s,n-1} = \sum E_{0i} \ln \ln(\beta_{s,i}) \cos \phi_{s,i}$$

Need this for variation of  $\beta_{s,n}, \phi_{s,n}$  etc.

Avg Accel Gradient  
 On the equation for  $\Delta W_n$ :

$$E_{on} \cdot L_n = V_{on} = \int_{-L_n/2}^{L_n/2} E(z) dz$$

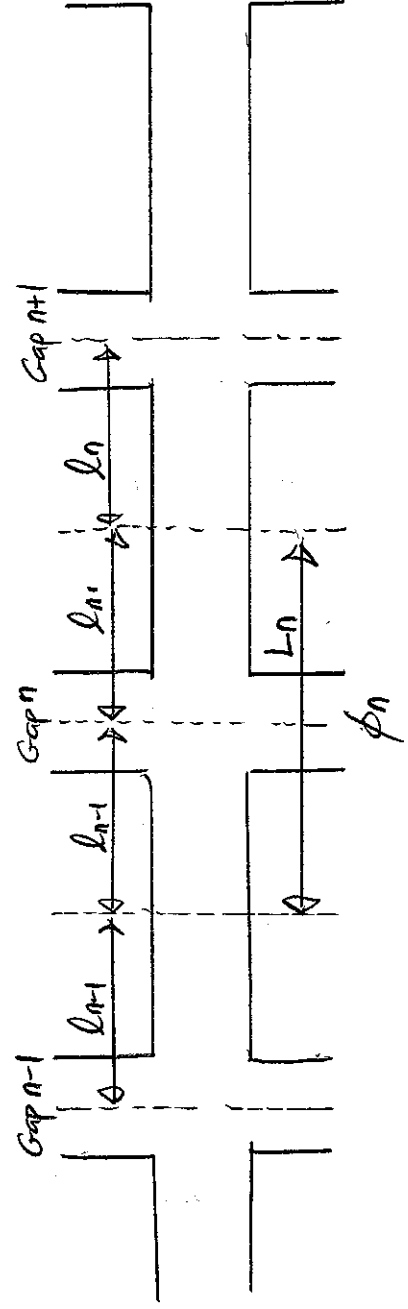
n<sup>th</sup> gap

$V_{on}$  = Accel potential n<sup>th</sup> gap  
 $L_n$  = Length containing full gap  
 fringe field.

$E_{on}$  = Avg. E-field over  
 gap extent defined by  
 $Z_{gap} \pm L_n/2$ .

Sometimes one defines  $E_{on}$  over a length  $L_n$   
 about the n<sup>th</sup> gap mid-way between neighboring  
 gaps upstream and downstream.

\* Convenient to define avg gradient over "cell"  
 in a periodic or quasi-periodic lattice.



But  $(2L_{n-1}) = \beta_{s,n-1} \lambda_{rf} \begin{cases} 1 & \text{O-Mode} \\ 1/2 & \text{\pi-Mode} \end{cases} \Rightarrow L_{n-1} = \frac{N}{2} \beta_{s,n} \lambda_{rf}$

$$\Rightarrow L_n = L_{n-1} + L_n = N (\beta_{s,n-1} + \beta_{s,n}) \frac{\lambda_{rf}}{2}$$

This should safely contain  
 the gap fringe extent and  
 define  $E_{on}$  naturally as the  
 average gradient in the  
 cell.

Continuous Differential Equations to Model Longitudinal Dynamics

See: Wangler §6.3  
Lund and Bernard USPAS notes.

Derived "kick" difference equations to model longitudinal dynamics about the synchronous particle:

$$(\phi_n - \phi_{sn}) - (\phi_{n-1} - \phi_{s,n-1}) = \frac{-2\pi N}{\beta_{s,n-1}} \frac{\Delta W_{n-1}}{\beta_{s,n-1}^2 m c^2} \Delta W_n = W_n - W_{s,n}$$

$$\Delta W_n - \Delta W_{n-1} = g E_0 n L_n (\beta_{sn}) [\cos \phi_n - \cos \phi_{sn}]$$

For small gap-to-gap changes replace discrete kicks by a continuous variation / field.

$$(\phi_n - \phi_{sn}) - (\phi_{n-1} - \phi_{s,n-1}) \longrightarrow \frac{d(\phi - \phi_s)}{dn}$$

$$\Delta W_n - \Delta W_{n-1} \longrightarrow \frac{d\Delta W}{dn}$$

\* Treat n as continuous.

Convert from gap index n to axial coordinate s as an independent variable

$$n = \frac{(S - S_n)}{N\beta_s \lambda r_f} \equiv \frac{S}{N\beta_s \lambda r_f}$$

$S_n$  = axial position of n<sup>th</sup> gap along reference trajectory  
For notational simplicity

$$\frac{d}{dn} = N\beta_s \lambda r_f \frac{d}{ds}$$

$$\left\{ \begin{aligned} (\phi_n - \phi_{s,n}) - (\phi_{n-1} - \phi_{s,n-1}) &= -\frac{2\pi N}{\lambda_{s,n-1}} \frac{\Delta W_{n-1}}{\beta_{s,n-1}^2 mc^2} \\ \Delta W_n - \Delta W_{n-1} &= g E_0 L_n \cdot I_n(\beta_{s,n}) [\cos \phi_n - \cos \phi_{s,n}] \end{aligned} \right.$$

$$N \beta_{s,n} \lambda_A \frac{d}{ds} (\phi - \phi_s) = -\frac{2\pi N \cdot \Delta W}{\lambda_s \beta_s^2 mc^2} \quad \Delta W = W - W_s$$

$$N \beta_{s,n} \lambda_A \frac{d \Delta W}{ds} = g E_0(s) T(\beta_s(s)) L(s) [\cos \phi - \cos \phi_s]$$

Also, the synchronous particle equation must also be integrated for the gain in energy for the  $\beta_s, \beta_s$  factors etc.

$$W_n - W_{n-1} = g E_0 L_n \cdot I_n(\beta_{s,n}) \cos \phi_{s,n}$$

$$\rightarrow N \beta_{s,n} \lambda_A \frac{d W_s}{ds} = g E_0(s) T(\beta_s(s)) L(s) \cos \phi_s$$

Then:

→

For simplicity, denote  $E_0(s) = E_0$   
 $T(\beta_3 s) = T$  } Constants in a  
 $L(s) = L$  } periodic lattice.

$$\Rightarrow (\chi_s \beta_3)^3 \frac{d}{ds} (\phi - \phi_s) = -\frac{2\pi}{\lambda T} \left( \frac{\Delta W}{mc^2} \right)$$

$$\Delta W = W - W_s$$

$$\frac{d}{ds} \Delta W = \int E_0 T \left( \frac{L}{N \beta_3 \lambda T} \right) (\cos \phi - \cos \phi_s)$$

$$L = N (\beta_{3n-1} + \beta_{3n}) \frac{\Delta T}{2} \Rightarrow \frac{L}{N \beta_3 \lambda T} = 1$$

Giving

$$\boxed{(\chi_s \beta_3)^3 \frac{d}{ds} (\phi - \phi_s) = -\frac{2\pi}{\lambda T} \left( \frac{\Delta W}{mc^2} \right)}$$

$$\frac{d}{ds} \Delta W = \int E_0 T (\cos \phi - \cos \phi_s) \quad (*)$$

These can be combined to eliminate  $W - W_s$  as:

$$\boxed{\frac{d}{ds} \left[ (\chi_s \beta_3)^3 \frac{d}{ds} (\phi - \phi_s) \right] = -\frac{2\pi}{\lambda T} \int \frac{E_0 T}{mc^2} (\cos \phi - \cos \phi_s)}$$

provided we take  $L$  to be the cell spacing; in this context  $E_0$  is the avg. gradient over the cell length.

Notes:  $N$  has been eliminated. Same formulae for O-Mode and  $\pi$ -Mode  
 \* Nonlinear equations

\* 2nd order nonlinear equation for evolution of  $\phi(s)$

Small Amplitude Phase Excursions

see Wanyer §6.6, Lund and Bernard, OSPAS notes

Nonlinear  
Phase evolution  
Equation

$$\frac{d}{ds} \left( (\gamma_s \beta_s)^3 \frac{d}{ds} \Delta\phi \right) = -\frac{2\pi}{\lambda r} \frac{2 E_0 T}{c m c^2} \left[ \cos(\phi_s + \Delta\phi) - \cos\phi_s \right]$$

$$\Delta\phi = \phi - \phi_s$$

Assume:

$\gamma_s \beta_s \sim$  varies slowly  $\Rightarrow$  pull through  $\frac{d}{ds}$

$|\Delta\phi| \ll 1 \Rightarrow$  small phase excursions about synchronous particle.

Then:

$$\cos(\phi_s + \Delta\phi) = \cos\phi_s \cos\Delta\phi - \sin\phi_s \sin\Delta\phi + \mathcal{O}(\Delta\phi^2)$$

$$\approx \cos\phi_s - \sin\phi_s \Delta\phi + \mathcal{O}(\Delta\phi^2)$$

To obtain:

$$\frac{d^2 \Delta\phi}{ds^2} + k_s^2 \Delta\phi = 0$$

$$k_s \equiv \sqrt{\frac{2\pi}{\lambda r} \frac{2 E_0 T}{c m c^2} \frac{\sin(-\phi_s)}{(\beta_s \gamma_s)^3}}$$

= Synchrotron Wavenumber

Linear equation for small phase excursions about synchronous particle.

This implies for:

$-\pi < \phi_s < 0 \Rightarrow k_s^2 > 0$

Small amplitude oscillations about synchronous particle Stable

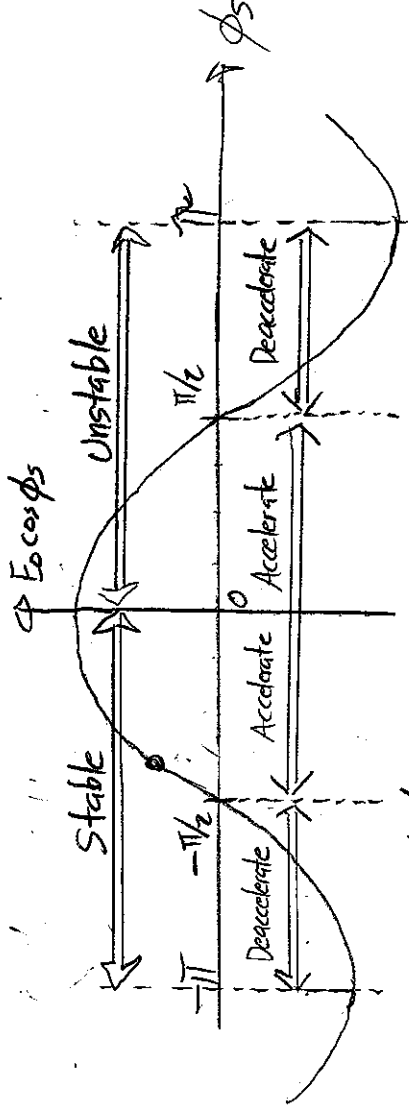
$0 < \phi_s < \pi \Rightarrow k_s^2 < 0$

Small amplitude oscillations about synchronous particle unstable

Recall the phase is defined relative to the RF wave peak

$$\frac{dW_s}{ds} \sim qE_0 \cos \phi_s$$

$$k_s = \sqrt{\frac{2qE_0 T \sin(\phi_s)}{\lambda v \frac{1}{c^2} (\gamma \beta)^3}}$$



Stable range  $\Rightarrow$  particle arrives at gap in rising field } consistent with  
 Unstable range  $\Rightarrow$  particle arrives at gap in falling field. } qualitative expectation  
 Particle accelerates and is stable for  $-\frac{\pi}{2} < \phi_s < 0$

\* A commonly taken value of  $\phi_s$  to accelerate with a reasonable phase width for stability (k<sub>s</sub> large) is to take:

$$\phi_s \approx -\frac{\pi}{6} = -30^\circ$$

\* If RF is used for beam bunching rather than acceleration, the strength of k<sub>s</sub> is maximized by taking

$$\phi_s = -\frac{\pi}{2}$$

\* If E<sub>0</sub>T and  $\phi_s$  remain nearly constant in acceleration:

$$k_s \sim \frac{1}{(k_s \beta_s)^{3/2}}$$

Showing that synchrotron oscillations will slow down (weaker focusing) as the beam accelerates.



The corresponding angular frequency to  $k_s$  is

$$\omega_s \equiv k_s(\beta c) \quad \text{Synchrotron angular Freq.}$$

Relative to the RF freq:  $\beta \approx \beta_s$

$$\frac{\omega_s}{\omega} = \frac{f_s}{f_{rf}} = \sqrt{\frac{2\pi}{\lambda_{rf}} \frac{\beta_s^2 c^2}{\omega^2} \frac{g E_0 T \sin(-\phi_s)}{mc^2 (\delta\beta_s)^3}}$$

$$\frac{\omega_s}{\omega} = \frac{f_s}{f_{rf}} = \sqrt{\frac{1}{2\pi (\delta\beta_s)^3} \left( \frac{g E_0 T \lambda_{rf}}{mc^2} \right) \sin(-\phi_s)}$$

From this expect:

\*  $f_s \ll f_{rf}$  as beam becomes more relativistic,

The linear synchrotron equation of motion can be solved for  $k_s = \text{const}$ :

$$d^2 \Delta\phi / ds^2 + k_s^2 \Delta\phi = 0$$

Initial condition

$$\Delta\phi(s=s_i) = \Delta\phi_0$$

$$d\Delta\phi / ds (s=s_i) = \Delta\phi_0'$$

$$1 = \frac{d}{ds}$$

Solution:

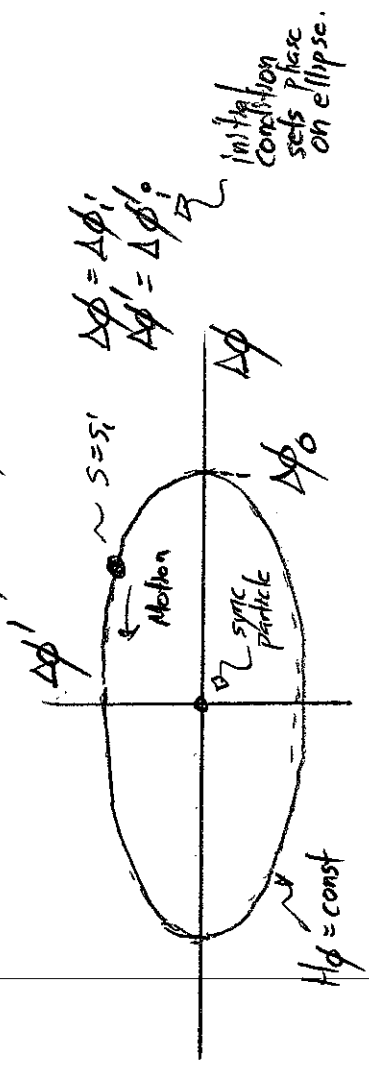
$$\Delta\phi(s) = \Delta\phi_0 \cos[k_s(s-s_i)] + \frac{\Delta\phi_0'}{k_s} \sin[k_s(s-s_i)]$$

$$\Delta\phi'(s) = -\Delta\phi_0 k_s \sin[k_s(s-s_i)] + \Delta\phi_0' \cos[k_s(s-s_i)]$$

Conservation of H (qm) Hamilton H:

$$H_\phi = \frac{1}{2}(\Delta\phi)^2 + \frac{1}{2}k_s^2(\Delta\phi)^2 = \frac{1}{2}(\Delta\phi_0')^2 + \frac{1}{2}k_s^2(\Delta\phi_0)^2 = \text{const.}$$

Phase-space in  $\Delta\phi - \Delta\phi'$  is an ellipse



When  $k_s (s-s_1) = 2\pi$  particle cycles around ellipse.

Denote for convenience:

$$\Delta\phi_0 = \text{Max Phase excursion} \Rightarrow H_\phi = \frac{1}{2} k_s^2 \Delta\phi^2$$

Then the Hamiltonian conservation is expressed as

$$H_\phi = \frac{1}{2} (\Delta\phi')^2 + \frac{1}{2} k_s^2 (\Delta\phi)^2 = \text{const}$$

Using this and:

$$(k_s \beta_s)^3 \Delta\phi' = -\frac{2\pi}{\lambda r} \frac{\Delta W}{mc^2} \equiv -\frac{2\pi}{\lambda r} \frac{W}{mc^2} \rightarrow \frac{1}{2} (\Delta\phi')^2 = \frac{1}{2} \frac{W}{\Delta\phi_0} W^2$$

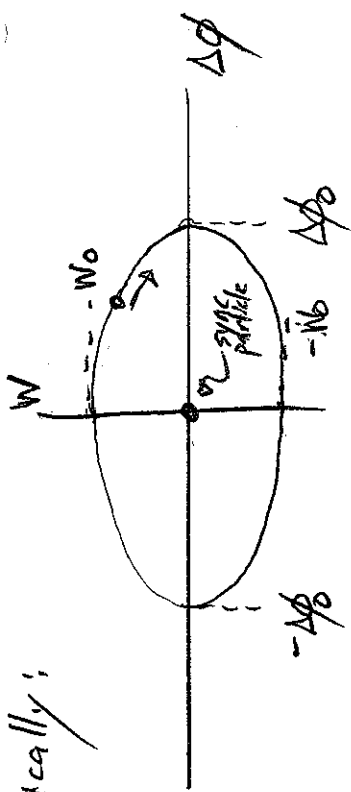
The ellipse becomes

$$\left(\frac{W}{W_0}\right)^2 + \left(\frac{\Delta\phi}{\Delta\phi_0}\right)^2 = 1$$

$\swarrow$  small  $W$        $\swarrow$  capital  $W$   
 $W \equiv \frac{\Delta W}{mc^2}$

$$W_0 = \frac{1}{\lambda r} \frac{2\pi}{k_s \beta_s} \Delta\phi_0 = \frac{1}{2} \text{width norm energy deviation} = \sqrt{\frac{(k_s \beta_s)^3 (2\pi \lambda r)^2 \sin^2(\phi_s) \Delta\phi_0^2}{2\pi}} = \sqrt{\frac{2\pi \lambda r}{k_s \beta_s} \sin^2(\phi_s) \Delta\phi_0^2}$$

Graphically:



The phase-space area of the ellipse is:

$$\begin{aligned} \text{Area} &= \pi \left( \frac{1}{2} \text{width} \right) \left( \frac{1}{2} \text{width} \right) \\ &= \pi \Delta\phi_0 W_0 \\ &= \sqrt{\frac{\pi}{2}} (\Delta\phi_0)^3 \left( \frac{2E_0 \Delta\phi_0}{mc^2} \sin(\phi_0) \right) \Delta\phi_0^2 \end{aligned}$$

Many choices of longitudinal coordinates are employed to study longitudinal dynamics. Some include:

(coord, momentum)

$(\phi, \bar{W})$

$(z, \Delta P_z)$

$(\Delta t, -\Delta W)$

⋮

$$\bar{W} = (\gamma - 1) mc^2 = \text{Kinetic Energy}$$

Proper sets of canonical variables (perhaps rescaled by constants like  $mc^2$ ) should be employed to measure phase-space areas. Canonical transforms can be applied to connect to other variable choices.

Nonlinear Phase-Space Structure of RF Bucket.

See Wanglers §6.4  
Lind and Barnard, USPAS notes

Cannot use small phase excursion approximation to analyze.  
Return to nonlinear coupled equations:

$$\begin{aligned} (\gamma_s \beta_s)^3 \frac{d \Delta \phi}{ds} &= -\frac{2\pi}{\lambda_A} \frac{\Delta W}{mc^2} \\ \frac{d \Delta W}{ds} &= q E_0 T [\cos \phi - \cos \phi_s] \end{aligned}$$

$$\begin{aligned} \Delta W &= W - W_s \\ \Delta \phi &= \phi - \phi_s \end{aligned}$$

Denote:

$$W \equiv \frac{\Delta W}{mc^2} \quad A \equiv \frac{2\pi}{\lambda_A (\gamma_s \beta_s)^3} \quad B \equiv \frac{q E_0 T}{mc^2}$$

$$\phi = \phi_s + \Delta \phi \Rightarrow \Delta \phi' = \phi' \quad \text{since we take } \phi_s = \text{const (simplifying)}$$

Then the nonlinear equations can be expressed as:

$$\begin{aligned} \phi' &= -A W \\ W' &= B [\cos \phi - \cos \phi_s] \end{aligned}$$

Assume that A and B vary weakly in s  
\* Likely need for continuous approx anyway

$$\begin{aligned} \Rightarrow \phi'' &= -A W' = -AB [\cos \phi - \cos \phi_s] \\ \phi'' &= -AB (\cos \phi - \cos \phi_s) \end{aligned}$$

Multiply by  $\phi'$  and integrate:

$$\phi' \phi'' = -AB(\cos\phi - \cos\phi_s) \phi'$$

$$\int \phi' \phi'' ds = -AB \int (\cos\phi - \cos\phi_s) \phi' ds \Rightarrow$$

$$\frac{\phi'^2}{2} + AB(\sin\phi - \phi_s \cos\phi_s) = \text{const.}$$

Now use  $\phi' = -Aw$  and divide by  $A$ :

$$\frac{Aw^2}{2} + B(\sin\phi - \phi_s \cos\phi_s) = \text{const} \equiv H\phi$$

$H\phi =$  Synchrotron Hamiltonian.

Analogy:  $A \frac{w^2}{2} \Rightarrow$  Interpret as "Kinetic Energy"  
 $B(\sin\phi - \phi_s \cos\phi_s) \Rightarrow$  Interpret as "Potential Energy"

To exploit this analogy, denote:

$$V(\phi) = B(\sin\phi - \phi_s \cos\phi_s)$$

$$\frac{\partial V(\phi)}{\partial \phi} = B(\cos\phi - \cos\phi_s) \sim \text{focus strength}$$

$$\frac{\partial^2 V(\phi)}{\partial \phi^2} = -B \sin\phi \sim \text{concavity}$$

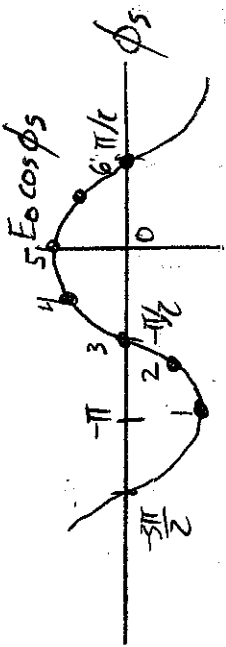
Want for stability about synchronous particle:

$$\frac{\partial^2 V(\phi)}{\partial \phi^2} \Big|_{\phi=\phi_s} > 0 \Rightarrow -B \sin\phi_s > 0 \Rightarrow B > 0$$

Same result obtained in small phase excursion limit as should be expected.

$$\sin\phi_s < 0$$
$$\pi < \phi_s < 2\pi$$

for stability



Plots of

$$V(\phi) = B(\sin \phi - \phi \cos \phi_s)$$

$$B = \frac{qE_0 T}{c m c^2} \geq 0$$

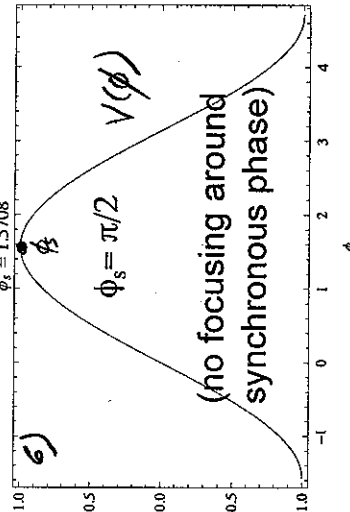
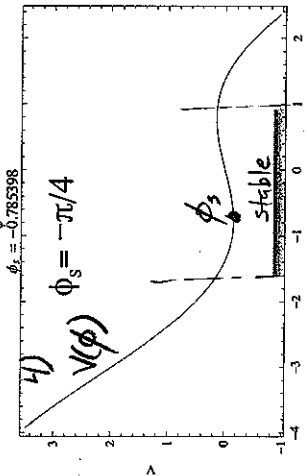
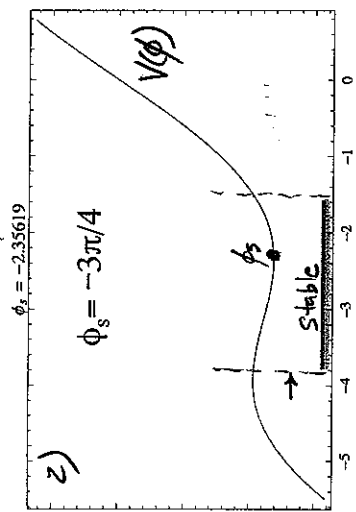
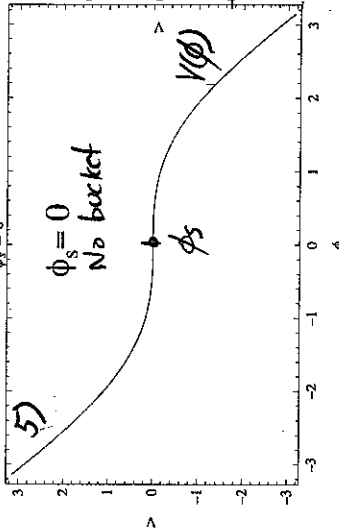
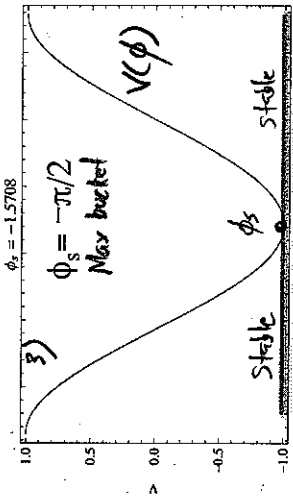
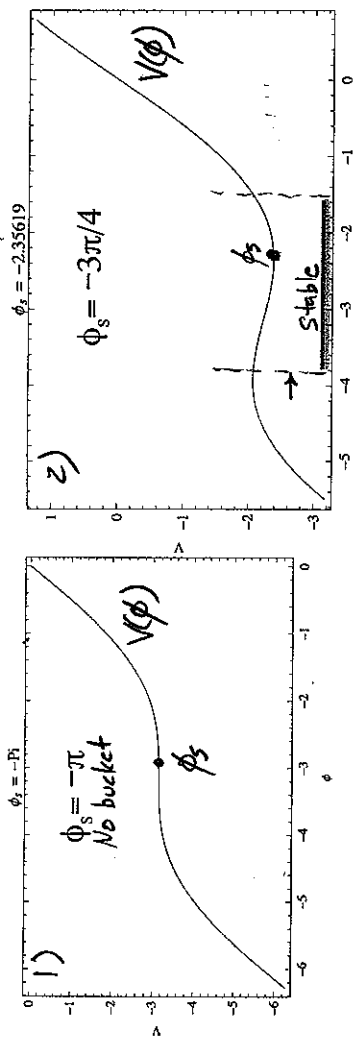
$\phi_s =$  various values

$-\pi < \phi_s < 0$  : Stable

$-\pi/2 < \phi_s < \pi/2$  : Accel

$\pi/2 < \phi_s < 0$  Accel and Focus.

$\phi_s \approx -30^\circ = -\pi/6$   
typical value





The total phase width of the separatrix about the synchronous particle is:

$$\Psi \equiv \text{Phase width} = |\phi_s| + |\phi_2| = -\phi_s - \phi_2 \quad \text{for } \phi_s < 0$$

$\phi = -\phi_s$        $\phi = -\phi_2$   
 Right X point      Left Turning point

From the separatrix eqn:

$$H_\phi(\phi = \phi_2, W=0) = H_\phi(-\phi_s)$$

$$\Rightarrow \sin \phi_2 - \phi_2 \cos \phi_2 = -[\sin \phi_s - \phi_s \cos \phi_s] \quad *$$

\* can be solved numerically for  $\phi_2$  to calculate the phase width  $\Psi$  for a given value of  $\phi_s$ .

Approximately:

$$\phi_2 = -\phi_s - \psi$$

$$\sin \phi_2 = -\sin(\phi_s + \psi) = -(\sin \phi_s \cos \psi + \sin \psi \cos \phi_s)$$

$$\sin \phi_s \cos \psi + \sin \psi \cos \phi_s - \phi_s \cos \phi_s - \psi \cos \phi_s = \sin \phi_s - \phi_s \cos \phi_s$$

$$\tan \phi_s = \frac{\sin \psi - \psi}{1 - \cos \psi} = \frac{(\sin \psi - \psi) \cos \phi_s}{\psi - \psi^3/6 + \dots - \psi} \approx \frac{-\psi}{3}$$

$$\psi \approx -3 \tan \phi_s$$

Numerical checks show works well up to  $|\phi_s| \approx \pi$ .

substitute in separatrix eqn \*



For case of  $\phi_s = -\pi/2$

separatrix eqn \* gives.

$$\sin \phi_2 = \phi_2 \cos(\pi/2) = -[-\sin(\pi/2) + (\pi/2) \cos(\pi/2)]$$

$$\sin \phi_2 = 1 \Rightarrow \phi_2 = -3\pi/2 = 270^\circ$$

$$\Rightarrow \psi = \frac{\pi}{2} - \phi_2 = \frac{\pi}{2} - 270^\circ = 360^\circ \text{ Focuses for full RF phase width } \phi$$

This choice will give no acceleration

but will be most efficient for beam bunching. Note also that the synchrotron wavenumber  $k_s = \sqrt{\frac{2\pi}{\lambda_{rf}} \frac{2E_0 T \sin(-\phi)}{c(\gamma_s \beta_s)^3 m c^2}}$  is largest for  $\phi_s = -\pi/2$ .

To estimate the vertical  $1/2$ -width in  $w$  of the separatrix for arb  $\phi_s$ :

$$w = w_{max}, \phi = -\phi_s \text{ in separatrix eqn:}$$

$$\Rightarrow H\phi = H\phi(-\phi_s)$$

$$\frac{A w_{max}^2}{2} + B [\sin \phi_s - \phi_s \cos \phi_s] = -B [\sin \phi_s - \phi_s \cos \phi_s]$$

$$w_{max} = \sqrt{4 \frac{B}{A} [\phi_s \cos \phi_s - \sin \phi_s]}$$

$$w_{max} = \frac{\Delta W_{max}}{m c^2} = \sqrt{\frac{2g E_0 T}{c \pi m c^2} (\gamma_s \beta_s)^3 \lambda_{rf} (\phi_s \cos \phi_s - \sin \phi_s)}$$

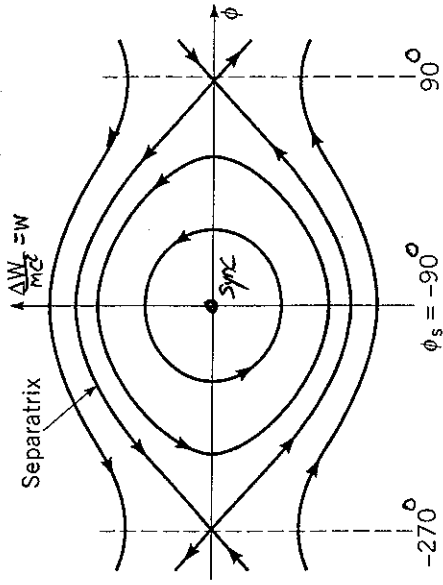


Figure 6.4. Separatrix for  $\phi_s = -90^\circ$  (no acceleration).

$$A = \frac{2\pi}{\lambda_{rf}} \frac{1}{(\gamma_s \beta_s)^3}$$

$$B = \frac{g E_0 T}{c m c^2}$$

$$W_{min} = -W_{max}$$

$$W\text{-width} = 2W_{max}$$

Approximating crudely, the  $\phi - W$  phase-space area of the bucket is:

$$\text{Area-Bucket} = \int_{\text{Bucket}} d\phi dW \approx \pi(W_{\text{max}}) \left(\psi/2\right)$$

$\approx \left(-\frac{3\pi}{2} \tan \phi_s\right) \cdot W_{\text{max}}$

Approx as an ellipse with area  $\pi \times (\text{x-radius}) \times (\text{y-radius})$

$$\text{Area Bucket} \approx \frac{3\pi}{2} \tan(\phi_s) \sqrt{\frac{2q E_0 T (\cos \beta_s)^3}{2 \pi m c^2}} \text{Ar} (\sin(\phi_s) - \phi_s \cos \phi_s)$$

This provides an estimate of the phase-space area that can be accelerated.

Comments:

Relativistic ( $\beta_s \approx 1$ )  $\Rightarrow$  Field errors ( $E_0 T \propto E_0; T \approx 1$ ) do not change synchronous condition, but shift final energy.

Non-Relativistic ( $\beta_s \ll 1$ )  $\Rightarrow$  Field errors ( $E_0 T$ ) cause shift to a new synchronous phase.

41/

Adiabatic Phase Damping Ref: Wangler, "RF Linear Accelerators" Secs. 5.12, 6.7.

If parameters (focus well) of an oscillator are changed slowly relative to the period of the oscillation, then expect an adiabatic invariant:

"Action" =  $\oint p dq$  = const.

cycle

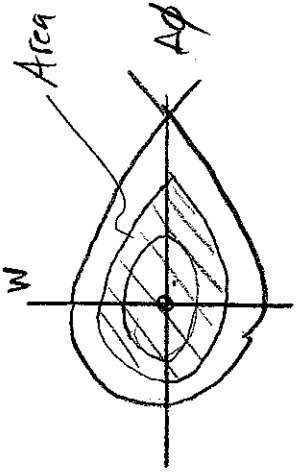
See Landau & Lifshitz  
 "Mechanics", 3rd Edition,  
 p. 154.

\* True for any number of parameters varying simultaneously

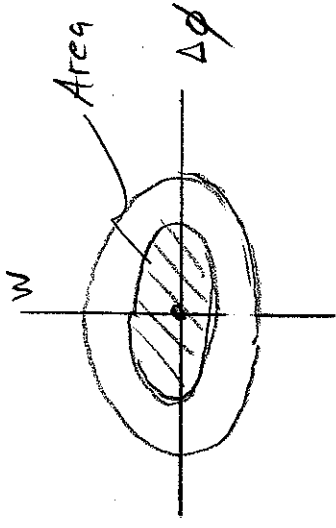
\* For synchrotron motion synchrotron wavenumber  $k_s$  sets the scale to measure slowness for validity.

$$k_s = \sqrt{\frac{2\pi}{\lambda_0} \frac{2 E_0 T \sin(-\phi_s)}{(ds/\beta_s)^3 m c^2}}$$

Nonlinear RF



Linear RF



This result tells us that the longitudinal phase-space area (or emittance) will be conserved as the focusing parameters (say due to acceleration) vary slowly on the synchrotron oscillation period.

Reminder:  $k_s = \sqrt{\frac{2\pi}{\lambda_0} \frac{2 E_0 T \sin(-\phi_s)}{m c^2 (ds/\beta_s)^3}}$  = Synchrotron Wavenumber

For the case of linear motion with small phase excursions about the synchronous particle:

$$\begin{aligned} \text{"Action"} &= \pi \Delta\phi_0 W_0 = \text{const} \\ &= \pi (\Delta\phi_0)^2 \sqrt{\frac{2E_0 T \Delta f}{2\pi}} \left( \frac{2E_0 T \Delta f}{mc^2} \right) \sin(-\phi_s) \end{aligned}$$

$$\Delta\phi_0 = \frac{\text{const}}{\left[ \left( \frac{2E_0 T \Delta f}{mc^2} \right) \sin(-\phi_s) \right]^{1/4}}$$

If we take

$$\begin{aligned} \phi_s &\approx \text{const} \\ E_0 T \Delta f &\approx \text{const} \end{aligned}$$

$$\Delta\phi_0 = \frac{\text{const}}{\left( \frac{2E_0 T \Delta f}{mc^2} \right)^{3/4}}$$

$\Rightarrow$

$$W_0 = \text{const} \left( \frac{2E_0 T \Delta f}{mc^2} \right)^{3/4}$$

and

\* called "phase damping" with adiabatic accel.

\* Energy deviation grows with adiabatic accel. with const phase-space area.

$$W \equiv \frac{\Delta W}{mc^2}$$

Recall

$$\Delta W_0 = \text{const} \left( \frac{2E_0 T \Delta f}{mc^2} \right)^{3/4}$$

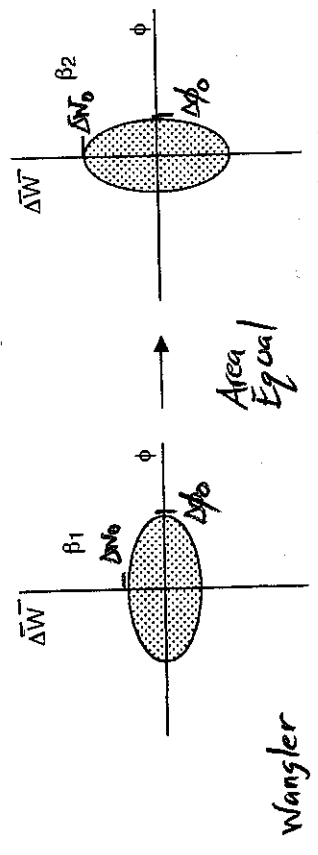
$\Delta\phi_0 =$  phase  $1/2$ -width linear orbit.

$\Delta\phi_0$  Normalized energy deviation of linear orbit.

or equivalently:  $\Delta\phi_0|_i = \text{initial value of } \Delta\phi_0$

$$\frac{\Delta\phi_0}{\Delta\phi_0|_i} = \left( \frac{(\chi_s \beta_s)|_i}{(\chi_s \beta_s)} \right)^{3/4} = \left( \frac{(\chi_s \beta_s)}{(\chi_s \beta_s)|_i} \right)^{3/4}$$

Graphically:



For RF high energy synchrotrons,  $\chi\beta$  will vary slowly over many laps and the adiabatic approximation can be well satisfied. For RF linacs,  $\chi\beta$  may change too rapidly for validity of the adiabatic approximation.

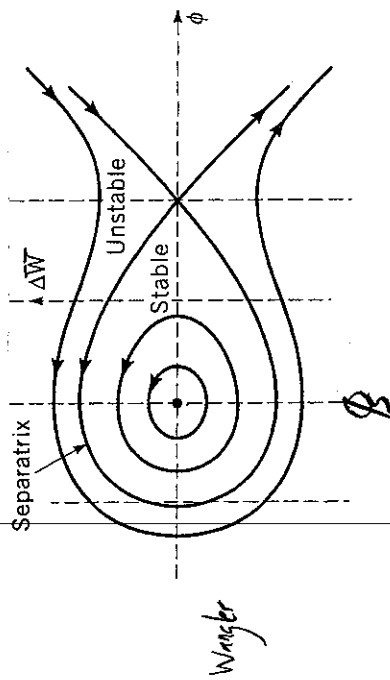
For FRIB linac segment #1:  $\chi_s \cdot \text{Length} \sim (2\pi)(\sim 10) \Rightarrow 10 \text{ oscillations}$

Ref: Q. Zhao

When  $\chi B_s \neq \text{const}$ ,  $H_0 \neq \text{const}$  and the RF "fish" structure becomes distorted to a more characteristic "golf-club" shape.

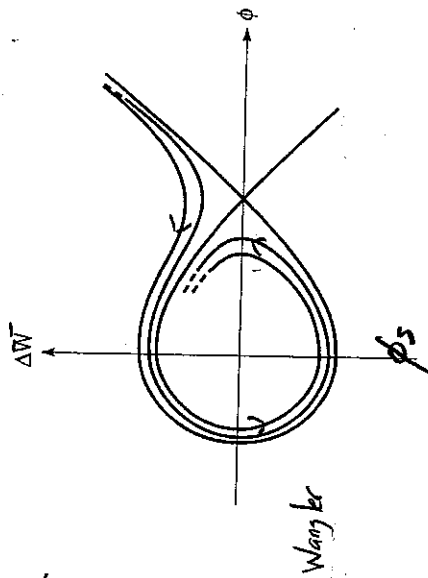
- \* Density in phase-space of non-interacting particles governed by Hamiltonian is invariant even if Hamiltonian  $H$  is non-constant by Liouville's Theorem.
- $\Rightarrow$  Phase volume enclosed by surface of fixed density is constant.
- $\Rightarrow$  Shape can distort due to acceleration.

$\chi B_s = \text{const}$



\* Use  $H_0 = \text{const}$  to analyze

$\chi B_s \neq \text{const}$  accelerating



\* Use difference equations to analyze general case.

\* Untapped for  $H_0 = \text{const}$  can move within for bounded orbit.

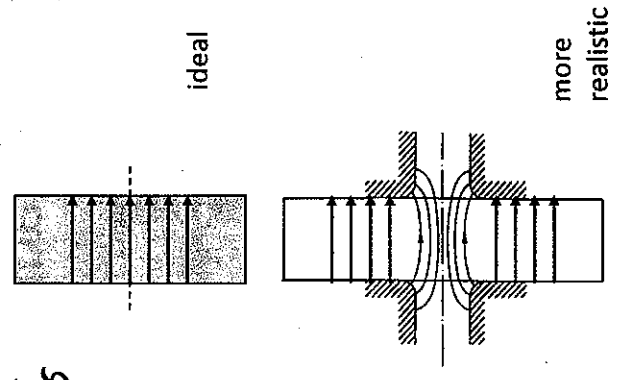
# Transverse RF Defocusing

Qualitative:

## RF Defocusing

Syphers  
USPAS

- When a particle enters a cavity off center, the field lines will have an inward component; and they will have an outward component upon exit from the cavity.
- However, the strength of the field is changing — typically, increasing — during transit.
- Thus, the outward “kick” due to the field will be greater than the inward kick — defocusing effect
- This “RF defocusing” is more important at lower energies



⇐ Ideal pillbox cavity has no radial E-field. E<sub>r</sub> to lead to transverse focusing / defocusing.

⇐ When aperture added to cavity to allow beam to enter / exit this produces an E<sub>r</sub> and transverse focusing / defocusing now possible.

Defocusing kick generally larger due to exit field gaining strength due to variation during transit. Part offset due to velocity gain within gap (Einzel lens effect).

see T. Wangler, RF Linear Accelerators

$$\frac{1}{f} = \frac{\Delta x'}{x} \approx \pi \frac{eV_{\text{eff}}}{mc^2} T \cos \phi_s \frac{\lambda(\beta\gamma)^2}{\lambda}$$

Transverse RF Defocusing Ref: Wangler "RF Linear Accelerators" § 7.3  
 Conte and Mackay, "Intro to the Physics of Particle Accelerators" Chapter 9

The field structure of an RF gap can also lead to transverse (radial) beam defocusing. Here we present a simple analysis to calculate the radial impulse a particle experiences when traversing the gap.

Qualitative Picture

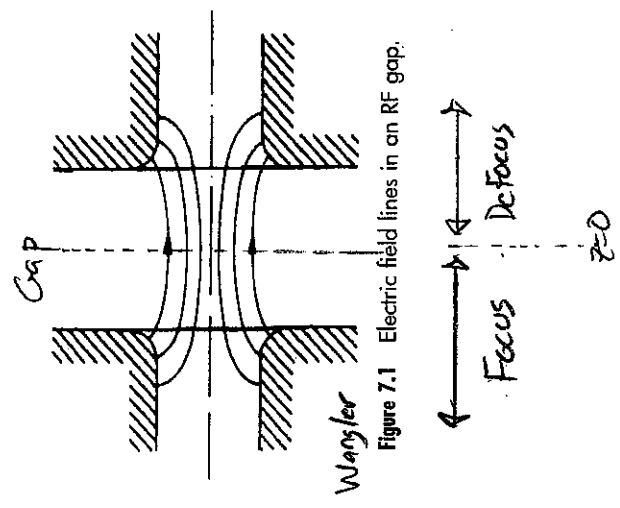
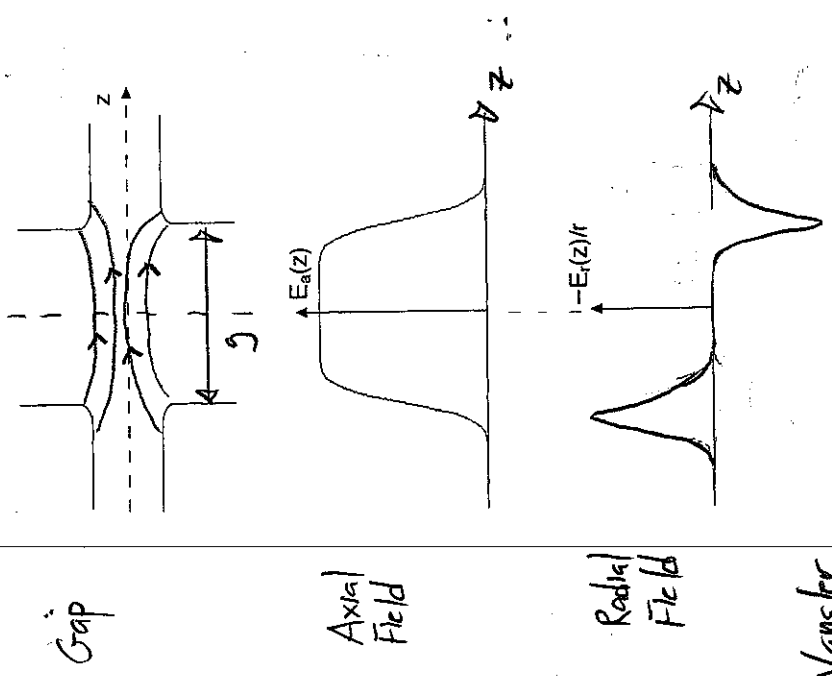


Figure 7.1 Electric field lines in an RF gap.

- \* Symmetric if field static and  $v \ll c$  const (negligible energy gain)  $\Rightarrow$  No optic
- \* But: RF field rising in time as particle traverses gap  $\Rightarrow$  Larger Defocus expected Net defocus.
- \* Counter: larger to right  $\Rightarrow$  less dwell time in defocus. Can have RF focusing if energy gain large. Like Einzel lens.
- \* BE also present but weaker.



Maxwell's Equations in Cavity!

$$\nabla \cdot \vec{E} = 0$$

$$\Rightarrow \frac{1}{r} \frac{\partial}{\partial r} (r E_r) + \frac{\partial E_z}{\partial z} = 0 \quad (1)$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\Rightarrow \frac{\partial E_r}{\partial z} - \frac{\partial E_z}{\partial r} = \frac{\partial B_\theta}{\partial t} \quad (2)$$

$$\nabla \times \vec{B} = \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t}$$

$$\Rightarrow -\frac{\partial B_\theta}{\partial z} = \frac{1}{c^2} \frac{\partial E_r}{\partial t} \quad (3)$$

$$\frac{\partial E_r}{\partial r} (r B_\theta) = \frac{1}{c^2} \frac{\partial E_z}{\partial t} \quad (4)$$

$\nabla \cdot \vec{B} = 0$   
satisfied by symmetry

Use these equations to approximate the fields near the axis ( $r=0$ ) where we take  $E_z$  to be independent of  $r$

For cavity assume:

$$\vec{E} = E_r(r, z, t) \hat{r} + E_z(r, z, t) \hat{z}$$

$$\vec{B} = B_\theta(r, z, t) \hat{\theta}$$

} TM<sub>10</sub> type Mode

Then Lorentz Force Eqn:

$$\frac{d\vec{p}}{dt} = q \vec{E} + q \vec{v} \times \vec{B}$$

gives

$$\frac{dp_r}{dt} = q E_r - \gamma v z B_\theta$$

$$\frac{dp_r}{dt} = q E_r - \gamma \beta c B_\theta$$

But

$$p_r = m \gamma \frac{dr}{dt} \approx m \gamma \beta c r'$$

$$r' = \frac{dr}{ds}$$

Giving a radial impulse (change in ang. momentum)

$$\Delta(\gamma \beta r') = \frac{q}{mc} \int [E_r - \beta c B_\theta] dt$$

Gap Transit

Approximate cavity fields near axis where  $E_z$  independent of  $r$ .  
 \* Need  $E_z$  and  $B_\theta$  near  $r=0$  to calculate impulse.

Using 1) with  $\partial E_z / \partial r \approx 0$ :

$$\frac{1}{r} \frac{\partial}{\partial r} (r E_r) + \frac{\partial E_z}{\partial z} = 0 \Rightarrow \frac{\partial}{\partial r} (r E_r) = - \frac{\partial E_z}{\partial z} r$$

$$\textcircled{1} \quad E_r = - \frac{\partial E_z}{\partial z} \frac{r}{2}$$

Using 3):

$$\frac{\partial B_\theta}{\partial z} = - \frac{\partial E_r}{\partial r} = \frac{r}{2} \frac{\partial^2 E_z}{\partial z^2} \frac{\partial}{\partial t} \Rightarrow B_\theta = \frac{r^2}{4} \frac{\partial^2 E_z}{\partial z^2}$$

$$\textcircled{2} \quad B_\theta = \frac{r^2}{4} \frac{\partial^2 E_z}{\partial z^2}$$

We take for the gap:

$$\textcircled{3} \quad E_z = E_0(z) \cos(\omega t + \phi)$$

harmonic accel. field,  $E_z = E_0(z) \cos \phi$   
 $t=0 \Rightarrow z=0$

Using ① and ② in the radial impulse formula:

$$\Delta(\chi p r') = \frac{q}{2mc} \int_{\text{Gap TransH}} \left[ E_r - \beta c B_\theta \right] dt = \frac{q}{2mc} \int_{-l/2}^{l/2} \left[ - \frac{\partial E_z}{\partial z} \cdot \frac{r}{2} - \beta \frac{r}{c} \frac{\partial E_z}{\partial t} \right] dt$$

$$= \frac{q}{2mc} \int_{-l/2}^{l/2} \left[ \frac{\partial E_z}{\partial z} \frac{r}{2} + \beta \frac{\partial E_z}{\partial t} \right] dt = \frac{q}{2mc} \frac{r}{\beta c}$$

$$dt = \frac{dz}{\beta c}$$

Approximate further in single gap

$r \approx \text{const}$  Impulse approx.  
 $\beta \approx \text{const}$  Accel weak

These may break down at very low energies. Then more detailed analysis needed.

Then we can pull  $\Gamma$  and  $\beta$  through the integral

$$\Delta(\mathcal{R}\beta') = \frac{-q\Gamma}{2\beta mc^2} \int_{-1/2}^{1/2} \left[ \frac{\partial E_z}{\partial z} + \beta \frac{\partial E_z}{\partial t} + \frac{z\beta}{r^2} \right] dz$$

But

$$\frac{\partial E_z}{\partial z} = \frac{\partial E_z}{\partial z} + \frac{z\beta}{r^2} = \frac{\partial E_z}{\partial z} + \frac{z\beta}{r^2} + \frac{z\beta}{r^2} + \frac{z\beta}{r^2} + \frac{z\beta}{r^2} + \frac{z\beta}{r^2}$$

Using this result to eliminate  $\frac{\partial E_z}{\partial z}$ :

$$\Delta(\mathcal{R}\beta') = \frac{-q\Gamma}{2\beta mc^2} \int_{-1/2}^{1/2} \left[ \frac{\partial E_z}{\partial t} + (\beta - \beta) \frac{\partial E_z}{\partial t} + \frac{z\beta}{r^2} \right] dz$$

$\beta - \beta = 0$  contains field so no contribution

$$\left( \beta - \frac{\beta}{\beta} \right) = \beta \frac{d\mathcal{R}}{dt} = -\frac{1}{\beta} \frac{d\mathcal{R}}{dt}$$

$$\Delta(\mathcal{R}\beta') = \frac{-q\Gamma}{2(\beta\beta)^2 mc^2} \int_{-1/2}^{1/2} \frac{\partial E_z}{\partial t} dz$$

Now use the harmonic accel field

$$E_z = E_0(z) \cos(\omega t + \phi) \Rightarrow \frac{\partial E_z}{\partial t} = -\omega E_0(z) \sin(\omega t + \phi)$$

For gap  $\omega t = \frac{2\pi}{\beta\lambda} z$

$$\frac{\partial E_z}{\partial t} = -\omega E_0(z) \sin\left(\frac{2\pi}{\beta\lambda} z + \phi\right)$$

Insert this field expression in impulse formula!

$$\begin{aligned} \Delta(\chi\beta\tau) &= -\frac{q\tau\omega}{Z(\chi\beta)^2 mc^2} \int_{-L/2}^{L/2} E_0(z) \sin\left(\frac{2\pi z}{\beta\lambda\tau} + \phi\right) dz \\ &= -\frac{q\tau\omega}{Z(\chi\beta)^2 mc^2} \int_{-L/2}^{L/2} E_0(z) \left\{ \begin{array}{l} \sin\left(\frac{2\pi z}{\beta\lambda\tau}\right) \cos\phi \\ \cos\left(\frac{2\pi z}{\beta\lambda\tau}\right) \sin\phi \end{array} \right\} dz \end{aligned}$$

if  $E_0(z)$  even function: usual for symmetric gap

$$\Delta(\chi\beta\tau) = -\frac{q\tau\omega}{Z(\chi\beta)^2 mc^2} \int_{-L/2}^{L/2} E_0(z) \cos\left(\frac{2\pi z}{\beta\lambda\tau}\right) \cos\phi dz$$

This can be further simplified using our formula for the transit time factor of a symmetric gap:

$$T = \int_{-L/2}^{L/2} E_0(z) \cos\left(\frac{2\pi z}{\beta\lambda\tau}\right) dz$$

Transit Time

$$E_0 L = \int_{-L/2}^{L/2} E_0(z) dz$$

Avg Field over Cell

(L large enough to contain  $E_0(z)$ , usually take to be cell length  $\Rightarrow E_0$  is cell avg field.)

$$\frac{\omega}{c} = \frac{2\pi}{\lambda\tau} = \frac{2\pi \nu}{\lambda\tau c}$$

Then we have

Radial Impulse from RF Gap

$$\Delta(\delta p_r) = \frac{\pi (g E_0 L T) \sin(-\phi)_x r}{\sqrt{1 - \beta^2} mc^2 (\delta \beta)^2}$$

Comments:

- \* Linear optic: Impulse  $\propto r$
- \* For  $\phi < 0$  (RF stability) is defocusing
- \*  $\sim 1/(\delta \beta)^2 \Rightarrow$  quickly becomes weak for relativistic particles
- \*  $\Rightarrow$  will be stronger for NR heavy ions (FRIB).
- \* More detailed analysis by Gluckstern (see Wangler of 7.9) shows that impulse can become focusing or significantly weakened when  $\beta$  varies strongly in gap (low energy ions). In this context the Einzel lens electrostatic focus impulse part compensates or offsets the effect of the rising RF field during transit.

Quasistatic Modeling of RF Gap Field

Wangler § 5.14

In the previous treatment, we took  $E_z$  to be independent of  $r$  to calculate the approximate cavity detuning impedance. If one needs a better approx:

- 1) Import cavity fields from a cavity design code into a particle simulation.
- 2) Carry out more advanced analysis to better approx. fields and acceleration effects within gap.

Within the context of  $z$ , the so-called quasistatic approx. can be useful.

Cavity fields satisfy the wave eqn:

$$\left( \nabla^2 - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \right) \vec{E} = 0$$

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$$

For harmonically varying fields:  $\sim \cos(\omega t + \phi)$

$$\left( \nabla^2 + \omega^2 \epsilon_0 \right) \vec{E} = 0$$

But

$$\frac{\omega}{c} = \frac{2\pi}{\lambda_{RF}} = \frac{2\pi}{\lambda_{RF}}$$

If the gap has characteristic length scales  $l_{gap} \ll \lambda_{RF}$ , expect

$$\nabla^2 \sim \frac{1}{l_{gap}^2} >> \left( \frac{2\pi}{\lambda_{RF}} \right)^2 \Rightarrow \boxed{\nabla^2 \vec{E} \approx 0}$$

But  $\vec{E}$  satisfies (vector calculus, any field):

$$\nabla \times (\nabla \times \vec{E}) = \nabla \cdot (\nabla \cdot \vec{E}) - \nabla^2 \vec{E}$$

$\nabla \cdot \vec{E} = 0$  in cavity  
 $\nabla^2 \vec{E} = 0$

Gauss

$$\nabla \times (\nabla \times \vec{E}) = 0 \Rightarrow \nabla \times \vec{E} = 0 \text{ solution.}$$

Satisfied if we take

$$\vec{E} = -\nabla \phi_e$$

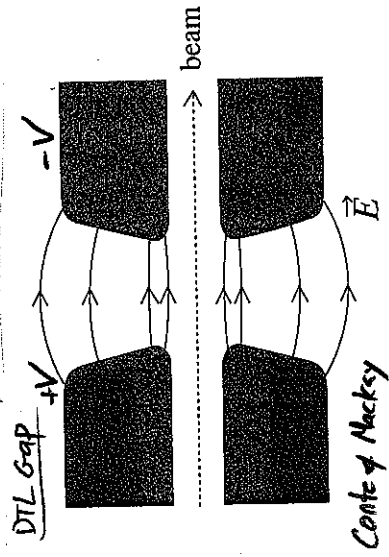
since  $\nabla \times \nabla \phi_e = 0$  for any  $\phi_e$ .

The Potential also must satisfy:

$$\nabla \cdot \vec{E} = -\nabla^2 \phi_e = 0 \Rightarrow \nabla^2 \phi_e = 0$$

$\phi_e$  satisfies Electrostatic Laplace eqn.

- \* Can only apply locally (say near short gap) with  $\lambda \ll \lambda_{rf}$
- \* Approx decouples electric and magnetic fields since  $-\frac{\partial \vec{B}}{\partial t}$  has been neglected in Faradays Law.



\* Used to model gap field regions,

\* Also applied in RFQ analysis (poles ripples small relative to RF wavelength) and analysis of induction accelerator gaps.