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## Injectors and longitudinal physics -- I

1. Fluid equations
2. Child-Langmuir Law  
(Reiser 2.5.2, Appendix 1)
3. Pierce electrodes
4. Transients in injectors
5. Injector choices

## I) FLUID EQUATIONS

START WITH VLASOV EQUATION FOR  $f(\underline{x}, \underline{p}, t)$ 

$$\frac{\partial f(\underline{x}, \underline{p}, t)}{\partial t} + \underline{\dot{x}} \cdot \frac{\partial f(\underline{x}, \underline{p}, t)}{\partial \underline{x}} + \underline{\dot{p}} \cdot \frac{\partial f(\underline{x}, \underline{p}, t)}{\partial \underline{p}} = 0$$

$$\text{HERE } \underline{\dot{x}} = \frac{d\underline{x}}{dt} = \frac{\underline{p}}{\gamma m}$$

$$\underline{\dot{p}} = \frac{d\underline{p}}{dt} = q(\underline{E}(\underline{x}, t) + \frac{\underline{p}}{\gamma m} \times \underline{B}(\underline{x}, t))$$

$$\gamma^2 = (p/mc)^2 + 1$$

INTEGRATE OVER MOMENTUM AND MULTIPLY BY VOLUME OF  $\underline{p}$ 

## a) CONTINUITY EQUATION

$$\int \int \int \underline{p} \left\{ \frac{\partial f}{\partial t} + \underline{\dot{x}} \cdot \frac{\partial f}{\partial \underline{x}} + (q \underline{E}(\underline{x}, t) + \frac{q \underline{p}}{\gamma m} \times \underline{B}(\underline{x}, t)) \cdot \frac{\partial f}{\partial \underline{p}} \right\} = 0$$

$$\text{DEFINE } n(\underline{x}, t) = \int f(\underline{x}, \underline{p}, t) \int \int \underline{p}$$

$$n(\underline{x}, t) \underline{v}(\underline{x}, t) = \int \frac{\underline{p}}{\gamma m} f(\underline{x}, \underline{p}, t) \int \int \underline{p}$$

## ① FIRST INTEGRAL

$$\int \int \int \underline{p} \frac{\partial f}{\partial t} = \frac{\partial}{\partial t} \int f \int \int \underline{p} = \frac{\partial n(\underline{x}, t)}{\partial t}$$

## ② SECOND INTEGRAL

$$\begin{aligned} \int \int \int \underline{p} \cdot \underline{\dot{x}} \cdot \frac{\partial f}{\partial \underline{x}} &= \int \int \int \frac{\underline{p}}{\gamma m} \cdot \frac{\partial f}{\partial \underline{x}} = \frac{\partial}{\partial \underline{x}} \cdot \int \int \underline{p} \frac{\underline{p}}{\gamma m} f \\ &= \frac{\partial}{\partial \underline{x}} \cdot n \underline{v} \end{aligned}$$

③ THIRD INTEGRAL

$$\int d^3p \left( q \underline{E} + \frac{q}{\gamma m} \underline{p} \times \underline{B} \right) \cdot \frac{\partial f}{\partial \underline{p}}$$

$\swarrow$   $\searrow$   
 $\int_{p=-\infty}^{p=\infty} q \underline{E} f$   $\int \frac{q}{\gamma m} (p_y B_z - p_z B_y) \frac{\partial f}{\partial p_x} dp_x dp_y dp_z + \dots$   
 $= 0$

$$\int_{-\infty}^{\infty} u v' dp_x = u v \Big|_{-\infty}^{\infty} - \int_{-\infty}^{\infty} u' v dp_x$$

$$u = \frac{q}{\gamma m} (p_y B_z - p_z B_y)$$

$$u' = \frac{\partial}{\partial p_x} \left( \frac{q}{\gamma m} (p_y B_z - p_z B_y) \right) \frac{\partial \gamma}{\partial p_x}$$

$$v = f$$

$$v' = \frac{\partial f}{\partial p_x}$$

$$\gamma^2 = \frac{p_x^2 + p_y^2 + p_z^2}{m^2 c^2} + 1$$

$$\Rightarrow 2\gamma \frac{\partial \gamma}{\partial p_x} = \frac{2 p_x}{m^2 c^2}$$

$$\int \frac{q}{\gamma^3 m^3 c^2} (p_y B_z - p_z B_y) p_x$$

$$+ \frac{q}{\gamma^3 m^3 c^2} (p_z B_x - p_x B_z) p_y$$

$$+ \frac{q}{\gamma^3 m^3 c^2} (p_x B_y - p_y B_x) p_z \cdot f d^3p$$

$= 0$  !

So  $\int d^3p \left\{ \frac{\partial f}{\partial t} + \underline{x} \cdot \frac{\partial f}{\partial \underline{x}} + \underline{p} \cdot \frac{\partial f}{\partial \underline{p}} \right\} = 0$

$$\Rightarrow \left[ \frac{\partial n(\underline{x}, t)}{\partial t} + \underline{\nabla} \cdot n(\underline{x}, t) \underline{v}(\underline{x}, t) = 0 \right]$$

CONTINUITY EQUATION  $\uparrow$   $\left\{ q n(\underline{x}, t) \underline{v}(\underline{x}, t) = \underline{J}(\underline{x}, t) \right.$

CURRENT DENSITY  $\uparrow$

ALTERNATIVELY  $\frac{\partial \rho}{\partial t} + \underline{\nabla} \cdot \underline{J} = 0$

BALANCED  
& LUND

## b) MOMENTUM EQUATION

(FOR SIMPLICITY : ASSUME NON-RELATIVISTIC)

$$\dot{\underline{x}} = \frac{\underline{p}}{m} \quad \dot{\underline{p}} = q(\underline{E}(x,t) + \frac{\underline{p}}{m} \times \underline{B}(x,t))$$

MULTIPLY BY  $\dot{\underline{x}}$  & INTEGRATE OVER MOMENTUM ( $\int^3 p$ )

$$\int \int^3 p \left\{ \dot{\underline{x}} \frac{\partial f}{\partial t} + \dot{\underline{x}} \cdot \underline{\dot{x}} \cdot \frac{\partial f}{\partial \underline{x}} + \dot{\underline{x}} \left( q\underline{E} + \frac{\underline{p}}{m} \times \underline{B} \right) \cdot \frac{\partial f}{\partial \underline{p}} \right\} = 0$$

DEFINE  $\underline{P} \equiv m \int \int^3 p (\underline{x} - \underline{v})(\underline{x} - \underline{v}) f(x, p, t)$

( $\underline{P}$  = pressure tensor)

$$\begin{aligned} &= m \int \int^3 p \dot{\underline{x}} \dot{\underline{x}} f - 2m \underline{v} \int \int^3 p \dot{\underline{x}} f + m \underline{v} \underline{v} \int \int^3 p f \\ &= m \int \int^3 p \dot{\underline{x}} \dot{\underline{x}} f - mn \underline{v} \underline{v} \end{aligned}$$

① FIRST INTEGRAL:

$$\int \int^3 p \dot{\underline{x}} \frac{\partial f}{\partial t} = \frac{\partial}{\partial t} \int \int^3 p \dot{\underline{x}} f = \frac{\partial}{\partial t} n \underline{v}$$

② SECOND INTEGRAL:

$$\begin{aligned} \int \int^3 p \underline{\dot{x}} \cdot \underline{\dot{x}} \cdot \frac{\partial f}{\partial \underline{x}} &= \frac{\partial}{\partial \underline{x}} \cdot \int \int^3 p \underline{\dot{x}} \dot{\underline{x}} f \\ &= \frac{1}{m} \frac{\partial}{\partial \underline{x}} \cdot \underline{P} + \frac{\partial}{\partial \underline{x}} \cdot n \underline{v} \underline{v} \\ &= \frac{1}{m} \frac{\partial}{\partial \underline{x}} \cdot \underline{P} + \left( \frac{\partial}{\partial \underline{x}} \cdot n \underline{v} \right) \underline{v} + n \underline{v} \cdot \frac{\partial \underline{v}}{\partial \underline{x}} \end{aligned}$$

③ THIRD INTEGRAL:

$$\begin{aligned} &\int \int^3 p \frac{\underline{p}}{m} (q\underline{E} + q \frac{\underline{p}}{m} \times \underline{B}) \cdot \frac{\partial f}{\partial \underline{p}} \\ &= \underbrace{f \frac{\underline{p}}{m} (q\underline{E} + q \frac{\underline{p}}{m} \times \underline{B})}_{=0} \Big|_{-\infty}^{\infty} - \int \int^3 p \frac{q\underline{p}}{m} (q\underline{E} + q \frac{\underline{p}}{m} \times \underline{B}) f \\ &= -\frac{nc}{m} (q\underline{E} + q \underline{v} \times \underline{B}) \end{aligned}$$

$$\begin{aligned} u &\frac{p_x}{m} (q\underline{E} + \frac{p}{m} \times \underline{B}) \\ u' &\frac{1}{m} (q\underline{E} + \frac{p}{m} \times \underline{B}) \\ v &\frac{\partial f}{\partial p_x} \\ v' &\frac{\partial f}{\partial p_x} \end{aligned}$$

BALANCED  
& LUND

## b) MOMENTUM EQUATION

(FOR SIMPLICITY : ASSUME NON-RELATIVISTIC)

$$\dot{\underline{x}} = \frac{\underline{p}}{m} \quad \dot{\underline{p}} = q(\underline{E}(x,t) + \frac{\underline{p}}{m} \times \underline{B}(x,t))$$

MULTIPLY BY  $\dot{\underline{x}}$  & INTEGRATE OVER MOMENTUM ( $\int^3 p$ )

$$\int \int^3 p \left\{ \dot{\underline{x}} \frac{\partial f}{\partial t} + \dot{\underline{x}} \cdot \underline{\dot{x}} \cdot \frac{\partial f}{\partial \underline{x}} + \dot{\underline{x}} \left( q\underline{E} + \frac{\underline{p}}{m} \times \underline{B} \right) \cdot \frac{\partial f}{\partial \underline{p}} \right\} = 0$$

DEFINE  $\underline{P} \equiv m \int \int^3 p (\underline{x} - \underline{v})(\underline{x} - \underline{v}) f(x, p, t)$

( $\underline{P}$  = pressure tensor)

$$\begin{aligned} &= m \int \int^3 p \underline{\dot{x}} \underline{\dot{x}} f - 2m \underline{v} \int \int^3 p \underline{\dot{x}} f + m \underline{v} \underline{v} \int \int^3 p f \\ &= m \int \int^3 p \underline{\dot{x}} \underline{\dot{x}} f - mn \underline{v} \underline{v} \end{aligned}$$

① FIRST INTEGRAL:

$$\int \int^3 p \underline{\dot{x}} \frac{\partial f}{\partial t} = \frac{\partial}{\partial t} \int \int^3 p \underline{\dot{x}} f = \frac{\partial}{\partial t} n \underline{v}$$

② SECOND INTEGRAL:

$$\begin{aligned} \int \int^3 p \underline{\dot{x}} \cdot \underline{\dot{x}} \cdot \frac{\partial f}{\partial \underline{x}} &= \frac{\partial}{\partial \underline{x}} \cdot \int \int^3 p \underline{\dot{x}} \underline{\dot{x}} f \\ &= \frac{1}{m} \frac{\partial}{\partial \underline{x}} \cdot \underline{P} + \frac{\partial}{\partial \underline{x}} \cdot n \underline{v} \underline{v} \\ &= \frac{1}{m} \frac{\partial}{\partial \underline{x}} \cdot \underline{P} + \left( \frac{\partial}{\partial \underline{x}} \cdot n \underline{v} \right) \underline{v} + n \underline{v} \cdot \frac{\partial \underline{v}}{\partial \underline{x}} \end{aligned}$$

③ THIRD INTEGRAL:

$$\begin{aligned} &\int \int^3 p \frac{\underline{p}}{m} (q\underline{E} + q\frac{\underline{p}}{m} \times \underline{B}) \cdot \frac{\partial f}{\partial \underline{p}} \\ &= \underbrace{f \frac{\underline{p}}{m} (q\underline{E} + q\frac{\underline{p}}{m} \times \underline{B})}_{=0} \Big|_{-\infty}^{\infty} - \int \int^3 p \frac{q\underline{p}}{m} (q\underline{E} + q\frac{\underline{p}}{m} \times \underline{B}) f \\ &= -\frac{nc}{m} (q\underline{E} + q\underline{v} \times \underline{B}) \end{aligned}$$

$$\begin{aligned} u &\frac{p_x}{m} (q\underline{E} + \frac{p}{m} \times \underline{B}) \\ u' &\frac{1}{m} (q\underline{E} + \frac{p}{m} \times \underline{B}) \\ v &\frac{\partial f}{\partial p_x} \\ v' &\frac{\partial f}{\partial p_x} \end{aligned}$$

ADDING THE INTEGRALS TOGETHER:

$$\frac{\partial}{\partial t} n \underline{\underline{v}} + \left( \frac{\partial}{\partial x} \cdot n \underline{\underline{v}} \right) \underline{\underline{v}} + n \underline{\underline{v}} \cdot \frac{\partial \underline{\underline{v}}}{\partial x} = n \frac{q}{m} (\underline{\underline{E}} + \underline{\underline{v}} \times \underline{\underline{B}}) - \frac{1}{m} \frac{\partial}{\partial x} \cdot \underline{\underline{P}}$$

$$\underbrace{n \frac{\partial \underline{\underline{v}}}{\partial t} + \frac{\partial n}{\partial t} \underline{\underline{v}} + \left( \frac{\partial}{\partial x} \cdot n \underline{\underline{v}} \right) \underline{\underline{v}}}_{= 0 \text{ BY CONTINUITY EQUATION}} + n \underline{\underline{v}} \cdot \frac{\partial \underline{\underline{v}}}{\partial x} = \quad \quad \quad \text{" "}$$

DIVIDING BY  $n$ :

$$\rho(x,t) = m n(x,t)$$

$$\frac{\partial \underline{\underline{v}}}{\partial t} + \underline{\underline{v}} \cdot \frac{\partial \underline{\underline{v}}}{\partial x} = \frac{q}{m} (\underline{\underline{E}} + \underline{\underline{v}} \times \underline{\underline{B}}) - \frac{1}{\rho} \frac{\partial}{\partial x} \cdot \underline{\underline{P}}$$

↑ MOMENTUM EQUATION ↑

NON-RELATIVISTIC

NOTE THAT  $\frac{\partial \underline{\underline{v}}}{\partial t} + \underline{\underline{v}} \cdot \frac{\partial \underline{\underline{v}}}{\partial x} = \frac{d}{dt} \underline{\underline{v}}$  ALONG A TRAJECTORY

$$\Rightarrow \frac{d \underline{\underline{v}}}{dt} = \frac{q}{m} (\underline{\underline{E}} + \underline{\underline{v}} \times \underline{\underline{B}}) - \frac{1}{\rho} \frac{\partial}{\partial x} \cdot \underline{\underline{P}}$$

NON-RELATIVISTIC

## Summary of fluid equations

$$\text{Let } n(\underline{x}, t) = \int d^3p f(\underline{x}, \underline{p}, t) \quad \text{PARTICLE DENSITY}$$

$$\underline{v}(\underline{x}, t) \equiv \frac{1}{n(\underline{x}, t)} \int d^3p \frac{\underline{p}}{\gamma m} f(\underline{x}, \underline{p}, t) \quad \text{FLUID VELOCITY}$$

$$\underline{P}(\underline{x}, t) \equiv \frac{1}{n(\underline{x}, t)} \int d^3p \underline{p} f(\underline{x}, \underline{p}, t) \quad \text{FLUID MOMENTUM}$$

$$\underline{P}(\underline{x}, t) \equiv \int d^3p (p - \underline{P}) \left( \frac{\underline{p}}{\gamma m} - \underline{v} \right) f(\underline{x}, \underline{p}, t) \quad \text{PRESSURE TENSOR}$$

$$\frac{d\underline{x}}{dt} = \frac{\underline{p}}{\gamma m} \quad \frac{d\underline{p}}{dt} = q(\underline{E}(\underline{x}, t) + \frac{\underline{p}}{\gamma m} \times \underline{B}(\underline{x}, t)) \quad \gamma^2 = \frac{\underline{p} \cdot \underline{p}}{(mc)^2} + 1$$

CONTINUITY EQUATION:  $\frac{\partial n(\underline{x}, t)}{\partial t} + \frac{\partial}{\partial \underline{x}} \cdot n(\underline{x}, t) \underline{v}(\underline{x}, t) = 0$

MOMENTUM EQUATION:  $\frac{\partial \underline{P}}{\partial t} + \underline{v} \cdot \frac{\partial \underline{P}}{\partial \underline{x}} = q(\underline{E} + \underline{v} \times \underline{B}) - \frac{1}{n(\underline{x}, t)} \frac{\partial}{\partial \underline{x}} \cdot \underline{P} = 0$

THE ABOVE EQUATIONS ARE RELATIVISTICALLY CORRECT,  
IN THE NON-RELATIVISTIC LIMIT THE CONTINUITY EQUATION  
REMAINS UNCHANGED & THE MOMENTUM EQUATION MAY BE WRITTEN:

NON RELATIVISTIC  $\rightarrow \frac{\partial \underline{v}}{\partial t} + \underline{v} \cdot \frac{\partial \underline{v}}{\partial \underline{x}} = \frac{q}{m} (\underline{E} + \underline{v} \times \underline{B}) - \frac{1}{m n} \frac{\partial}{\partial \underline{x}} \cdot \underline{P}$

THESE EQUATIONS ARE SUPPLEMENTED WITH MAXWELL'S EQUATIONS:  
for  $\underline{E}(\underline{x}, t)$  &  $\underline{B}(\underline{x}, t)$

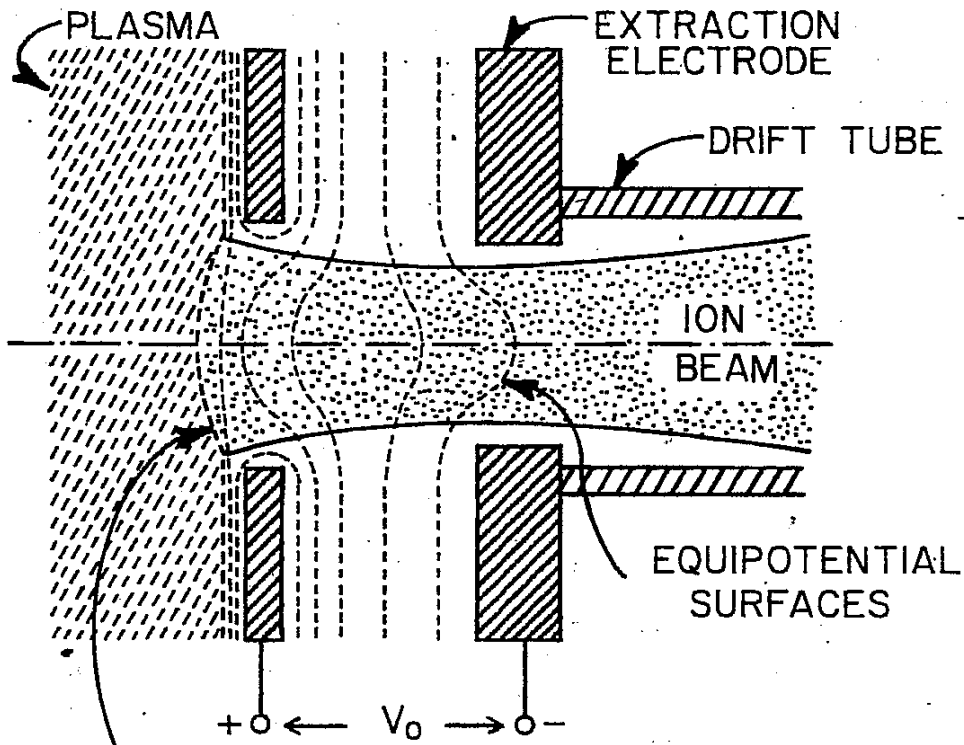
$$\frac{\partial}{\partial \underline{x}} \cdot \underline{E} = \frac{q n(\underline{x}, t)}{\epsilon_0} \quad \frac{\partial}{\partial \underline{x}} \times \underline{E} = -\frac{\partial \underline{B}}{\partial t}$$

$$\frac{\partial}{\partial \underline{x}} \cdot \underline{B} = 0 \quad \frac{\partial}{\partial \underline{x}} \times \underline{B} = \mu_0 \underline{J} + \frac{1}{c^2} \frac{\partial \underline{E}}{\partial t} \quad \underline{J}(\underline{x}, t) = q n(\underline{x}, t) \underline{v}$$

NEED ADDITIONAL EQUATIONS SUCH AS  $\underline{P} = 0$  OR ENERGY EQUATION  
TO TERMINATE SET OF EQUATIONS.

# INJECTORS

(5)



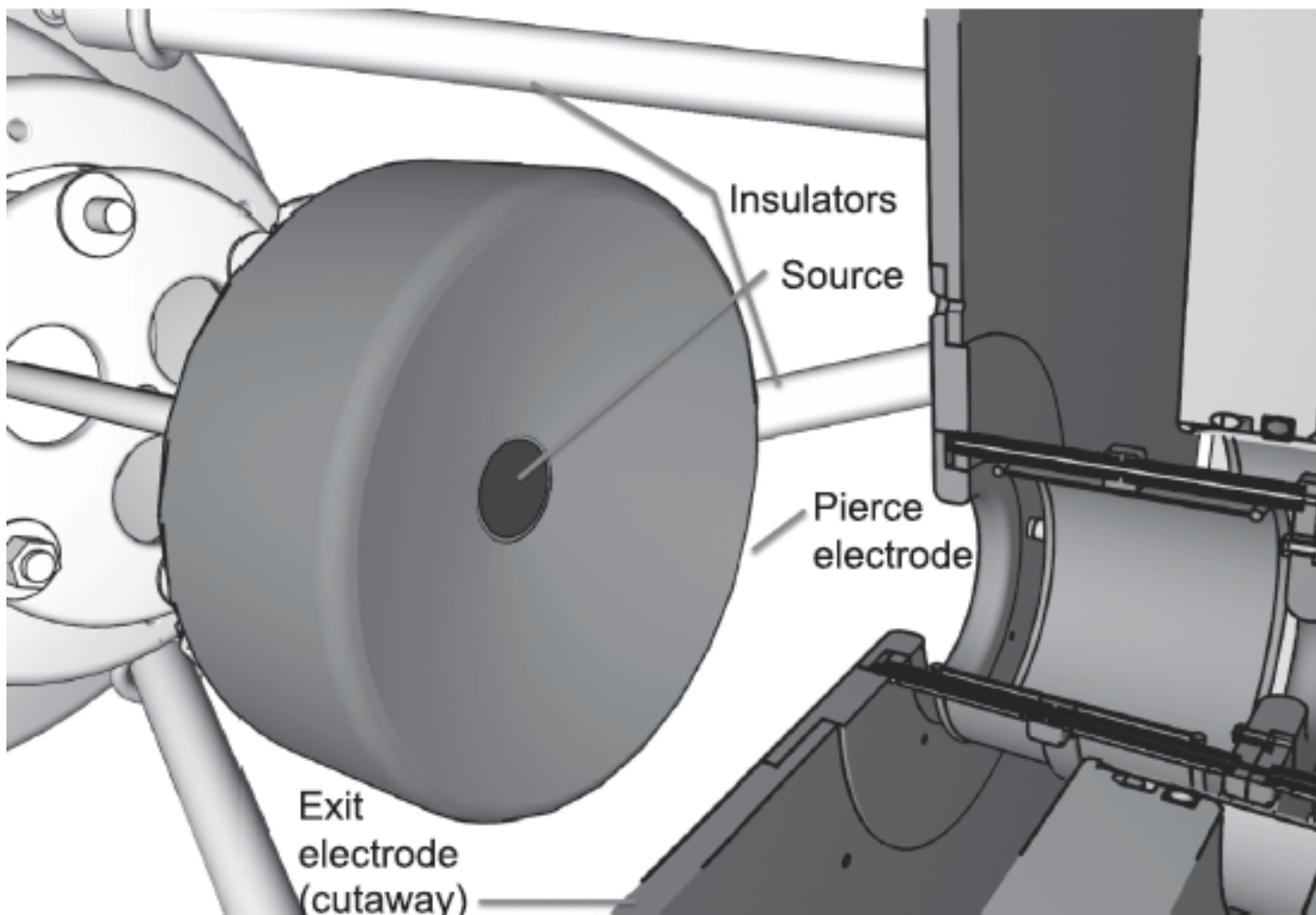
EMITTING SURFACE  
(PLASMA "SHEATH" OR "MENISCUS")

OR "HOT PLATE"

REISER, FIGURE 1.2

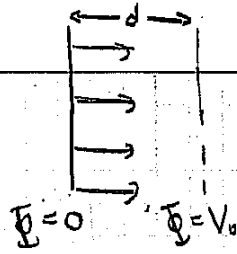
- DOPED TUNGSTEN
- ALUMINO-SILICATE





A mechanical drawing of a hot-plate diode used on the NDCX-1 experiment at LBNL. One quarter of the exit electrode is cut away for viewing the source geometry

# I CHILD-LANGMUIR EMISSION



ASSUME EMISSION IS PLANAR 1-D:

$$J = \rho v_z \quad (1)$$

$$\frac{\partial v_z}{\partial t} + v_z \frac{\partial v_z}{\partial z} = q \frac{\partial \Phi}{\partial z} \Rightarrow \frac{1}{2} m v_z^2 = q \Phi(z) \quad |z| \Rightarrow v_z = \left( \frac{2q\Phi}{m} \right)^{1/2}$$

$$\frac{J^2 \Phi}{\epsilon_0^2} = \frac{\rho^2}{\epsilon_0^2}$$

$$(3) \quad \text{(NOTE } \Phi = -\phi \text{ ACTUAL E.I. POTENTIAL)}$$

CONTINUITY EQUATION (1-D)  $\frac{\partial \rho}{\partial t} + \frac{\partial \rho v_z}{\partial z} = 0 \quad (4)$

for time steady emission  $\rho v_z = \text{constant} = J$

$$\Rightarrow \frac{J^2 \Phi}{\epsilon_0^2} = \frac{J}{\epsilon_0 v_z} = \frac{J}{\epsilon_0 \left( \frac{2q\Phi}{m} \right)^{1/2}}$$

MULTIPLYING BY  $\frac{d\Phi}{dz}$  AND INTEGRATING:

$$\frac{\Phi^{3/2}}{2} = \frac{J m^{1/2}}{\epsilon_0 (2q)^{1/2}} z \Phi^{1/2} + \text{const}$$

Assume  $\Phi' = 0$  at  $z=0$  (Space-charge limited emission)

$$\Phi = 0 \text{ at } z=0 \Rightarrow \text{const} = 0$$

$$\frac{d\Phi}{dz} = \left( \frac{4J}{\epsilon_0} \right)^{1/2} \left( \frac{m\Phi}{2q} \right)^{1/4}$$

$$\Rightarrow \frac{4}{3} \Phi^{3/4} = \left( \frac{4J}{\epsilon_0} \right)^{1/2} \left( \frac{m}{2q} \right)^{1/4} z \Rightarrow$$

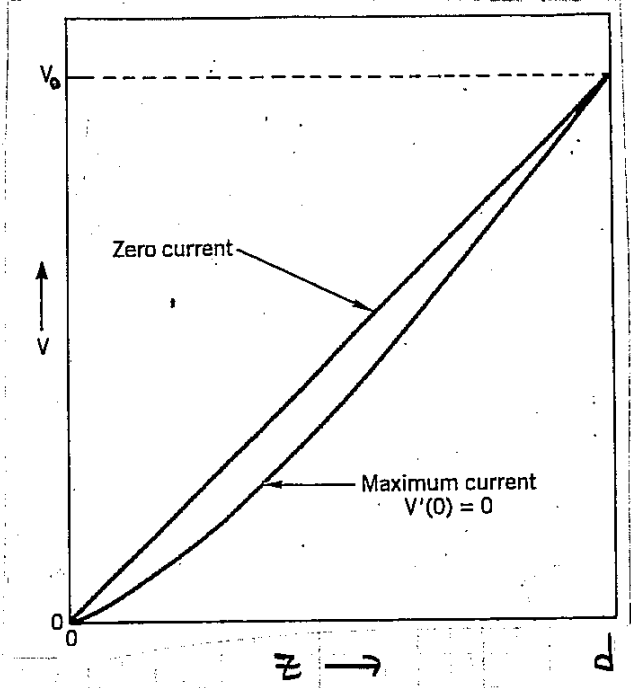
$$\Phi(z) = \left( \frac{3}{4} \right)^{4/3} \left( \frac{4J}{\epsilon_0} \right)^{2/3} \left( \frac{m}{2q} \right)^{1/3} z^{4/3}$$

(7)

If  $\Phi = V_0$  at  $z = d \Rightarrow \Phi = V_0 \left(\frac{z}{d}\right)^{4/3}$

$\Rightarrow V_0 = \left(\frac{3}{4}\right)^{4/3} \left(\frac{4J}{\epsilon_0}\right)^{2/3} \left(\frac{m}{2q}\right)^{1/3} d^{4/3}$

9  $J = \frac{4}{9} \epsilon_0 \left(\frac{2q}{m}\right)^{3/2} \frac{V_0^{3/2}}{d^2}$



NOTE THAT IF WE MULTIPLY J BY THE BEAM AREA  $\pi V_b^2$ , AND DIVIDE BY  $v = \left(\frac{2qV_0}{m}\right)^{1/2}$

$\Rightarrow \lambda = \frac{4\pi \epsilon_0 V}{9} \left(\frac{V_b^2}{J^2}\right)$

RECALL:  $Q \equiv \frac{\lambda}{4\pi \epsilon_0 V}$  (NON-LOCAL.)

$\Rightarrow Q = \frac{1}{9} \left(\frac{V_b^2}{d^2}\right)$  or as a function of z:  $Q(z) = \frac{1}{9} \left(\frac{V_b^2}{z^2}\right)$

REFERENCE

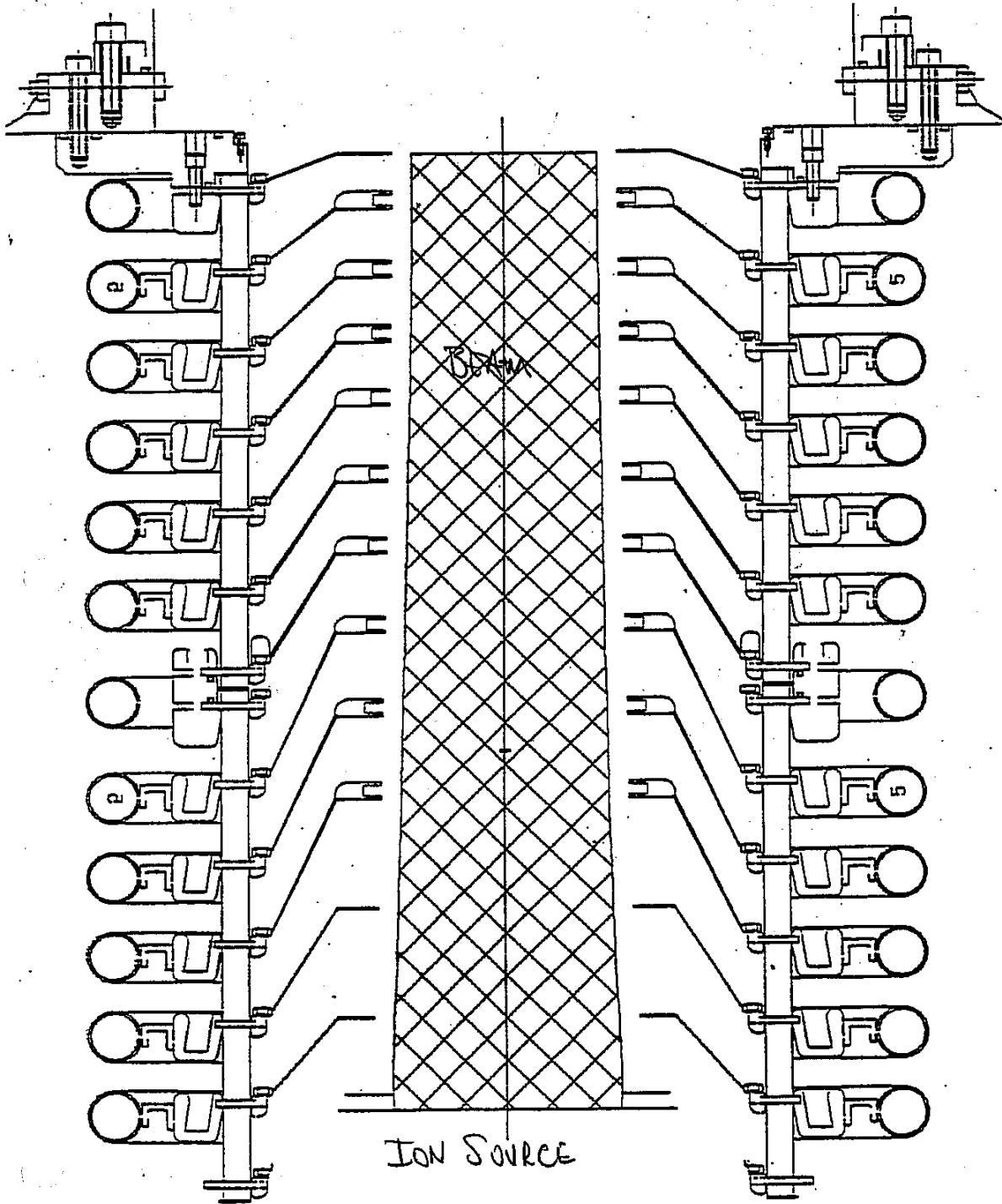
FOR EVERY COLOR SQUARE  
49 SHEETS OF 8 1/2 X 11 SQUARE  
49 SHEETS OF 11 X 17 SQUARE  
100 SHEETS OF 8 1/2 X 11 SQUARE  
100 SHEETS OF 11 X 17 SQUARE  
100 SHEETS OF 14 X 17 SQUARE  
100 RECYCLED WHITE SQUARE  
100 RECYCLED WHITE SQUARE  
MADE IN U.S.A.



# PIERCE COLUMN

$$V \sim z^{4/3}$$

$$E \sim z^{1/3}$$



DEVELOP  
~~WE~~ WE USE THE PARAXIAL RAY EQUATION FOR PARTICLES IN  
 AXISYMMETRIC SYSTEMS:

$$r'' + \underbrace{\frac{\gamma'}{\beta^2 \gamma}}_{\text{INERTIAL}} r' + \underbrace{\frac{\gamma''}{2\beta^2 \gamma}}_{E_r} r + \underbrace{\left(\frac{\omega_L}{2\gamma\beta c}\right)^2}_{V_0 B_z - \text{CENTRIFUGAL}} r - \underbrace{\left(\frac{p_0}{\gamma\beta m c}\right)^2 \frac{1}{r^3}}_{\text{CENTRIFUGAL}} - \underbrace{\frac{q}{\gamma^3 m v_z^2} \frac{\lambda(r)}{2\beta^2 \gamma}}_{\text{SELF-FIELD}} = 0$$

$$\theta' = \frac{p_0}{\gamma m r^2 \beta c} - \frac{\omega_c}{2\gamma\beta c} \quad \leftarrow \text{CONSTANCY \& DEFINITION OF CANONICAL MOMENTUM}$$

ENVELOPE EQUATION FOR AXISYMMETRIC BETA

$$n_b'' + \frac{\gamma' n_b'}{\beta^2 \gamma} + \frac{\gamma''}{2\beta^2 \gamma} n_b + \left(\frac{\omega_c}{2\gamma\beta c}\right)^2 n_b - \frac{4\langle p_0 \rangle^2}{(\gamma m \beta c)^2 r_b^3} - \frac{E_r^2}{V_b^3} - \frac{Q}{n_b} = 0$$

$$E_r^2 \equiv 4(\langle n^2 \rangle \langle v_{te} \rangle - \langle n v \rangle^2) + \langle n^2 \rangle \langle n^2 \theta'^2 \rangle - \langle n^2 \theta' \rangle^2$$

### RETURNING TO PARAXIAL ENVELOPE EQUATION:

$$(for \beta \ll 1) \quad v_b'' + \frac{\beta'}{\beta} v_b' + \left[ \frac{1}{2} \frac{\beta'^2}{\beta^2} + \frac{1}{2} \frac{\beta''}{\beta} \right] v_b - \frac{Q}{v_b} = 0$$

$$for \quad v_b'' = \frac{\beta'}{\beta} v_b' = 0$$

$$if \quad \Phi = v_b \left( \frac{z}{d} \right)^{1/3}$$

$$v = C z^{2/3}$$

$$v' = \frac{2}{3} C z^{-1/3}$$

$$v'' = -\frac{2}{9} C z^{-4/3}$$

$$\Rightarrow \left[ \frac{1}{2} \frac{\beta'^2}{\beta^2} + \frac{1}{2} \frac{\beta''}{\beta} \right] v_b^2 = Q$$

$$\left[ \frac{z}{9} \frac{1}{z^2} \quad -\frac{1}{9} \frac{1}{z^2} \right]$$

$$\Rightarrow Q(z) = \frac{1}{9} \frac{v_b^2}{z^2}$$

So Child-Langmuir flow satisfies the

PARAXIAL ENVELOPE EQUATION FOR

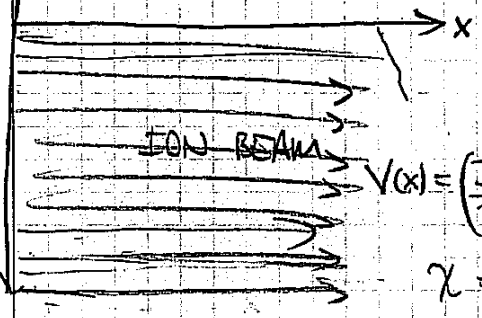
A CONSTANT BEAM RADIUS (AS IT SHOULD!)

# PIERCE'S ELECTRODES: GOING BEYOND 1D

CONSIDER THE CASE A BEAM WHICH FILLS THE LOWER HALF-SPACE.

CHARGE FREE REGION  $\nabla^2 \phi = 0$

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = 0$$



$$V(x) = \left(\frac{J}{\chi}\right)^{2/3} x^{4/3}$$

$$\chi = \left(\frac{4\epsilon_0}{9}\right) \sqrt{\frac{2q}{m}}$$

FIND SOLUTION

SUCH THAT

$$\frac{\partial \phi(x, y=0)}{\partial y} = 0$$

$$\phi(x, y=0) = V(x)$$

PIERCE'S SOLUTION: LET THE POTENTIAL BE THE REAL PART

OF 
$$\phi + iW = V(x+iy) \equiv V(z) \quad z = x+iy$$

NOTE THAT FOR ANY  $V(z)$  WITH DERIVATIVES THAT EXIST INDEPENDENT OF DIRECTION (ANALYTIC) THE REAL PART OF  $V(z)$

SATISFIES LAPLACE'S EQUATION: 
$$\frac{\partial^2 \text{Re}[V]}{\partial x^2} + \frac{\partial^2 \text{Re}[V]}{\partial y^2} = 0$$

$$\frac{\partial \phi}{\partial x} = \text{Re} \left[ \frac{dV}{dz} \right]$$

$$\frac{\partial \phi}{\partial y} = \text{Re} \left[ i \frac{dV}{dz} \right]$$

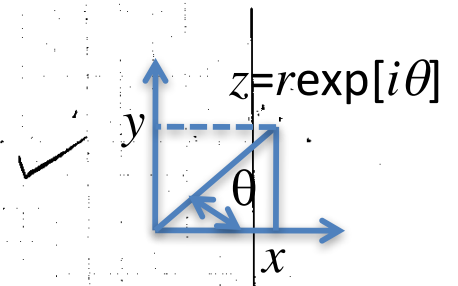
$$\frac{\partial^2 \phi}{\partial x^2} = \text{Re} \left[ \frac{d^2 V}{dz^2} \right]$$

$$\frac{\partial^2 \phi}{\partial y^2} = -\text{Re} \left[ \frac{d^2 V}{dz^2} \right]$$

$$\Rightarrow \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = \text{Re} \left[ \frac{d^2 V(z)}{dz^2} \right] - \text{Re} \left[ \frac{d^2 V(z)}{dz^2} \right] = 0$$

CHOOSE  $V(z) = \left(\frac{J}{\lambda}\right)^{2/3} (x+iy)^{4/3}$

By construction  $\phi(x, y=0) = V(x)$



$$\phi = \text{Re} \left[ \left(\frac{J}{\lambda}\right)^{2/3} (x+iy)^{4/3} \right]$$

$$= \left(\frac{J}{\lambda}\right)^{2/3} (x^2+y^2)^{2/3} \text{Re} \left[ \exp \left[ i \frac{4}{3} \tan^{-1} \left( \frac{y}{x} \right) \right] \right]$$

Let  $x+iy = r \exp[i\theta]$   
 $(x+iy)^{4/3} = r^{4/3} \exp \left[ i \frac{4\theta}{3} \right]$

$$\phi(x, y) = \left(\frac{J}{\lambda}\right)^{2/3} (x^2+y^2)^{2/3} \cos \left[ \frac{4}{3} \tan^{-1} \left( \frac{y}{x} \right) \right]$$

Note that  $\phi(x, y) = \phi(x, -y) \Rightarrow \frac{\partial \phi}{\partial y}(x, y=0) = 0$

$\phi = 0$  EQUIPOTENTIAL:  
 $\Rightarrow 0 = \cos \left[ \frac{4}{3} \tan^{-1} \left( \frac{y}{x} \right) \right]$   
 $\Rightarrow \tan^{-1} \left( \frac{y}{x} \right) = \frac{3}{4} \left( \frac{\pi}{2} \right) = 67.5^\circ$

So line  $\theta = 67.5^\circ$  is a  $\phi=0$  equipotential.

FOR A GENERAL EQUIPOTENTIAL PASSING THROUGH  $x_0$ :

$$x_0^{4/3} = (x^2+y^2)^{2/3} \cos \left[ \frac{4}{3} \tan^{-1} \left( \frac{y}{x} \right) \right]$$

Equipotential that passes through point  $(x_0, 0)$

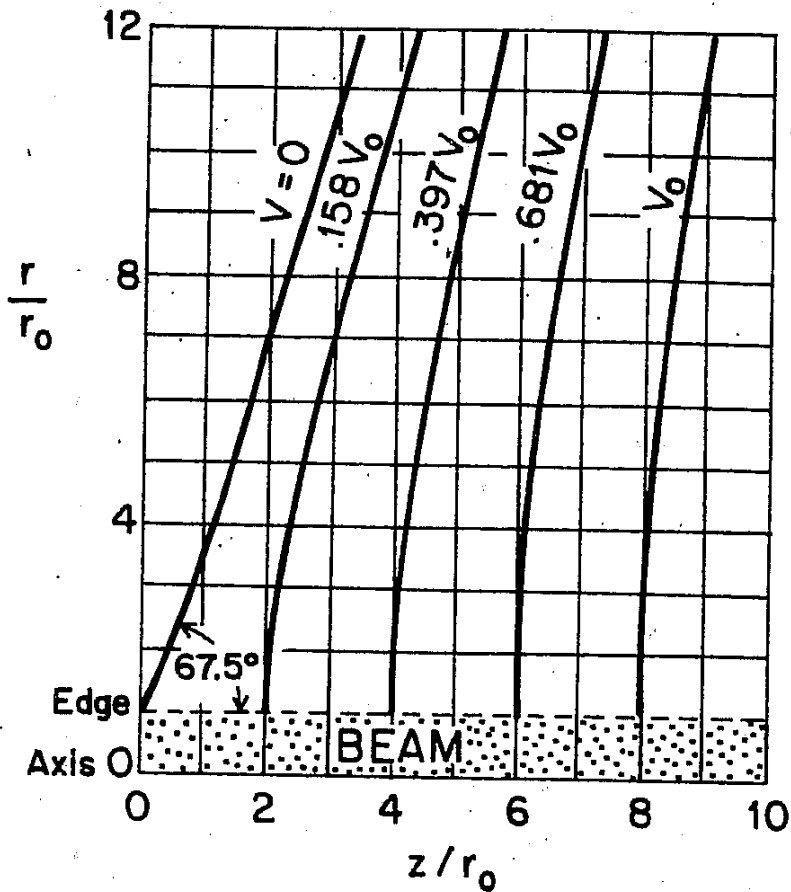
$$\phi(x_0) = \left(\frac{J}{\lambda}\right)^{2/3} x_0^{4/3}$$

13706 100% RECYCLED PAPER 50% RECYCLED FIBER 2 SQUARE FEET PER SHEET 100 SHEETS PER PACK 2 SQUARE FEET PER SHEET 100 SHEETS PER PACK 4 SQUARE FEET PER SHEET 25 SHEETS PER PACK 5 SQUARE FEET PER SHEET 10 SHEETS PER PACK 100% RECYCLED PAPER 50% RECYCLED FIBER 2 SQUARE FEET PER SHEET 100 SHEETS PER PACK 2 SQUARE FEET PER SHEET 100 SHEETS PER PACK 4 SQUARE FEET PER SHEET 25 SHEETS PER PACK 5 SQUARE FEET PER SHEET 10 SHEETS PER PACK  
 Made in U.S.A.  
 National Brand





# PIERCE ELECTRODES FOR CIRCULAR BEAMS



- SOLUTION is similar, but must be done numerically
- $\phi = 0$  is same as planar case

FIGURES FROM A.T. FORRESTER,  
"LARGE ION BEAMS",  
WILEY, 1988

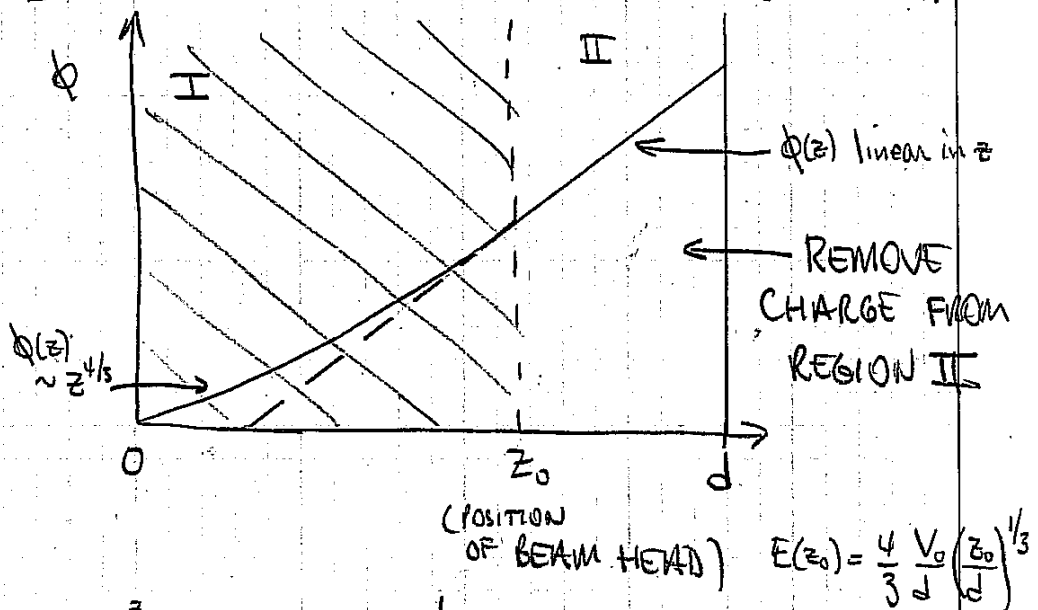
100% RECYCLED PAPER, 50% SOY INK  
 42-200 42-201 42-202 42-203 42-204 42-205 42-206 42-207 42-208 42-209 42-210  
 100% RECYCLED PAPER, 50% SOY INK  
 42-200 42-201 42-202 42-203 42-204 42-205 42-206 42-207 42-208 42-209 42-210  
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# TRANSIENTS IN $\pi$ INJECTORS (LAMPEL & TIEFENBACH, Appl. Phys. Lett., 43, 57, 1983)

DURING TURN-ON THERE IS NO SPACE CHARGE IN FRONT OF BEAM, SO FIELDS MAY NOT BE GIVEN BY CHILD-LANGMUIR LAW.  $\Rightarrow$  CURRENT SPIKES POSSIBLE  $\Rightarrow$  ADVERSE TRANSDUCER COUPLING.

SOLUTION: ADJUST VOLTAGE ON DIODE SUCH THAT C-L FIELD OCCURS EVERYWHERE THERE IS BEAM.



$$\begin{aligned}
 \Phi(d) &= - \int_0^{z_0} E(z) dz + \int_{z_0}^d E(z) dz \\
 &= V_0 \left( \frac{z_0}{d} \right)^{4/3} + \frac{4}{3} \frac{V_0}{d} \left( \frac{z_0}{d} \right)^{1/3} (d - z_0) \\
 &= V_0 \left[ \frac{4}{3} \left( \frac{z_0}{d} \right)^{1/3} - \frac{1}{3} \left( \frac{z_0}{d} \right)^{4/3} \right]
 \end{aligned}$$

(NOTE  $V_0$  IS THE DESIRED STEADY STATE VOLTAGE ACROSS DIODE)

So if we know  $z_0(t)$  we can determine  $\Phi(t)$ .

$$\frac{1}{2} m \dot{z}_0^2 = qV_0 \left(\frac{z_0}{d}\right)^{4/3}$$

(since by construction, HEAD OF BEAM TRAVELS AT CHILD-LANGMUIR VELOCITY LIKE ALL PARTICLES),

$$\dot{z}_0 = \left(\frac{2qV_0}{m}\right)^{1/2} \left(\frac{z_0}{d}\right)^{2/3}$$

$$\frac{dz_0}{z_0^{2/3}} = \left(\frac{2qV_0}{m}\right)^{1/2} \frac{dt}{d^{2/3}}$$

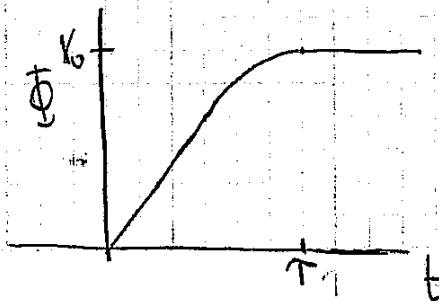
$$\Rightarrow 3z_0^{1/3} = \left(\frac{2qV_0}{m}\right)^{1/2} \frac{t}{d^{2/3}} \Rightarrow t = \frac{3(z_0 d^2)^{1/3}}{\left(\frac{2qV_0}{m}\right)^{1/2}}$$

Let  $\uparrow = \frac{3d}{\left(\frac{2qV_0}{m}\right)^{1/2}} =$  transit time across diode

$$\Rightarrow \frac{t}{\uparrow} = \left(\frac{z_0}{d}\right)^{1/3}$$

$$\Phi(d, z_0) = V_0 \left[ \frac{4}{3} \left(\frac{z_0}{d}\right)^{1/3} - \frac{1}{3} \left(\frac{z_0}{d}\right)^{4/3} \right]$$

$$\Rightarrow \Phi(d, t) = \begin{cases} V_0 \left[ \frac{4}{3} \left(\frac{t}{\uparrow}\right) - \frac{1}{3} \left(\frac{t}{\uparrow}\right)^4 \right] & \text{for } 0 < t < \uparrow \\ V_0 & \text{for } t > \uparrow \end{cases}$$



INJECTOR CHOICES (cf. Kwan et al, NIMRA 464, 379 (2001))

$$\text{CHILD-LANGMUIR} \Rightarrow J = \chi \frac{V^{3/2}}{d^2}$$

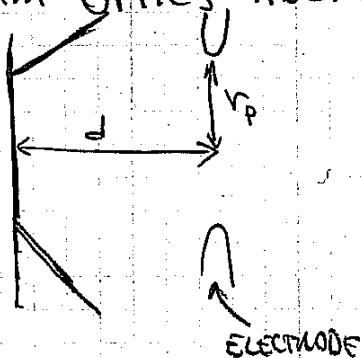
$$\text{where } \chi = \frac{4}{9} \epsilon_0 \left(\frac{2q}{m}\right)^{1/2}$$

SOME CONSTRAINTS:

(1) VOLTAGE BREAKDOWN

EMPIRICALLY  $V \leq \sim 100 \text{ kV} \begin{cases} \left(\frac{d}{1 \text{ cm}}\right) & \text{for } d \leq 1 \text{ cm} \\ \left(\frac{d}{1 \text{ cm}}\right)^{1/2} & \text{for } d \geq 1 \text{ cm} \end{cases}$

(2) BEAM OPTICS ABERRATIONS:  $d \gtrsim \frac{3}{4} r_p$  (TYPICALLY)



NOTE THAT

$$J \sim \frac{V^{3/2}}{d^2} \sim \begin{cases} V^{-1/2} \sim d^{-1/2} & d < 1 \text{ cm} \\ V^{-5/2} \sim d^{-5/4} & d > 1 \text{ cm} \end{cases} \quad I \sim \pi r_p^2 J \sim \begin{cases} V^{3/2} \\ \end{cases}$$

Thus current density decreases with size and voltage, but  $I$  increases.

100% RECYCLED PAPER 5 EQUARE  
 100% RECYCLED PAPER 4 EQUARE  
 100% RECYCLED PAPER 3 EQUARE  
 100% RECYCLED WHITE 5 EQUARE  
 100% RECYCLED WHITE 4 EQUARE  
 100% RECYCLED WHITE 3 EQUARE  
 100% RECYCLED WHITE 2 EQUARE  
 100% RECYCLED WHITE 1 EQUARE  
 Made in U.S.A.



$A_{IV}$   
 $V = 24.54 \sqrt{S}$

from A. Faltens:

V, kV

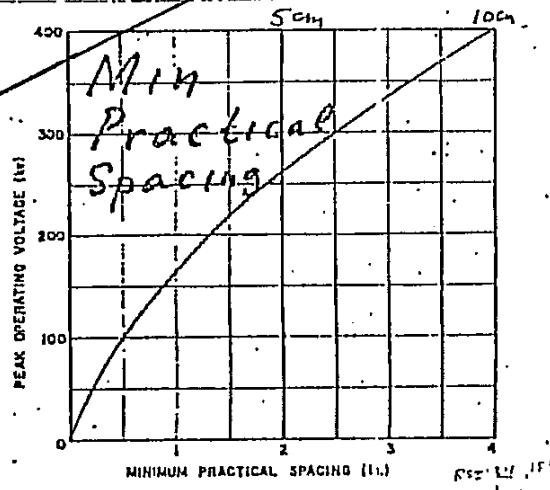
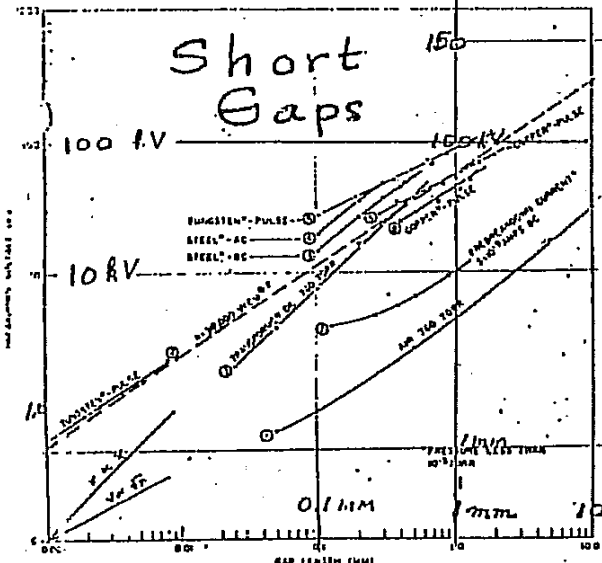
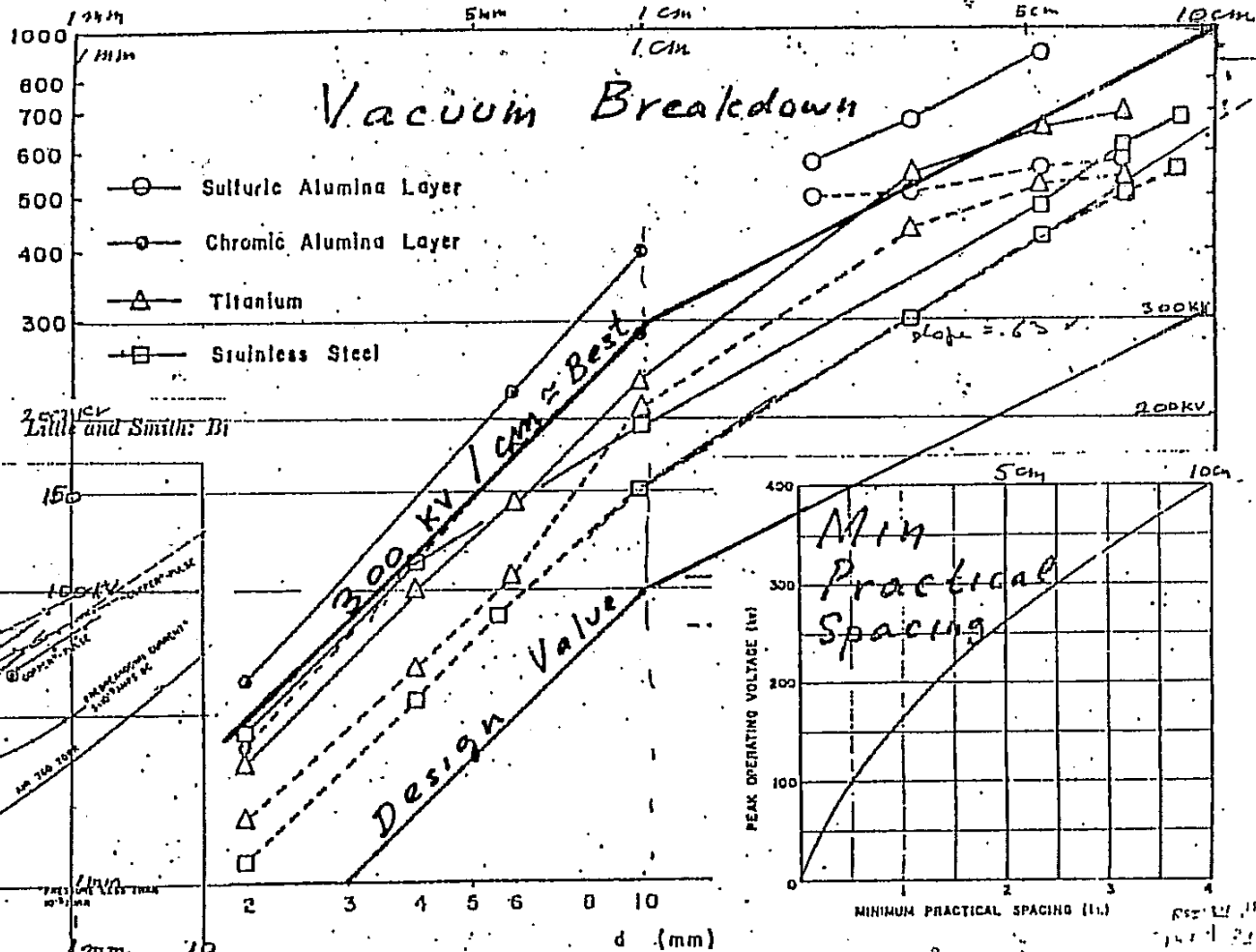
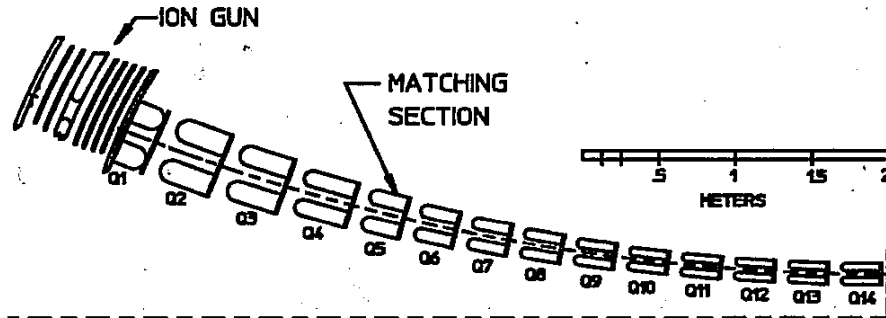


Figure 7.13 log U - log d plot.

Fig. 1. Breakdown voltage-vs-gap length for uniform-field and non-uniform-field geometry. Numbers on curves indicate the

MULTIPLE BEAMLET INJECTORS CAN HAVE HIGHER CURRENT DENSITY  
 DECREASING SIZE OF INJECTOR

traditional design using single large diameter source



advanced design using multiple beamlets

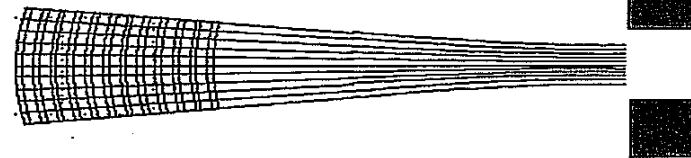


Each beamlet carries higher current density; But merging beamlets increases thermal spread.

Child-Langmuir  $J_{CL} \propto \frac{V^{3/2}}{d^2}$

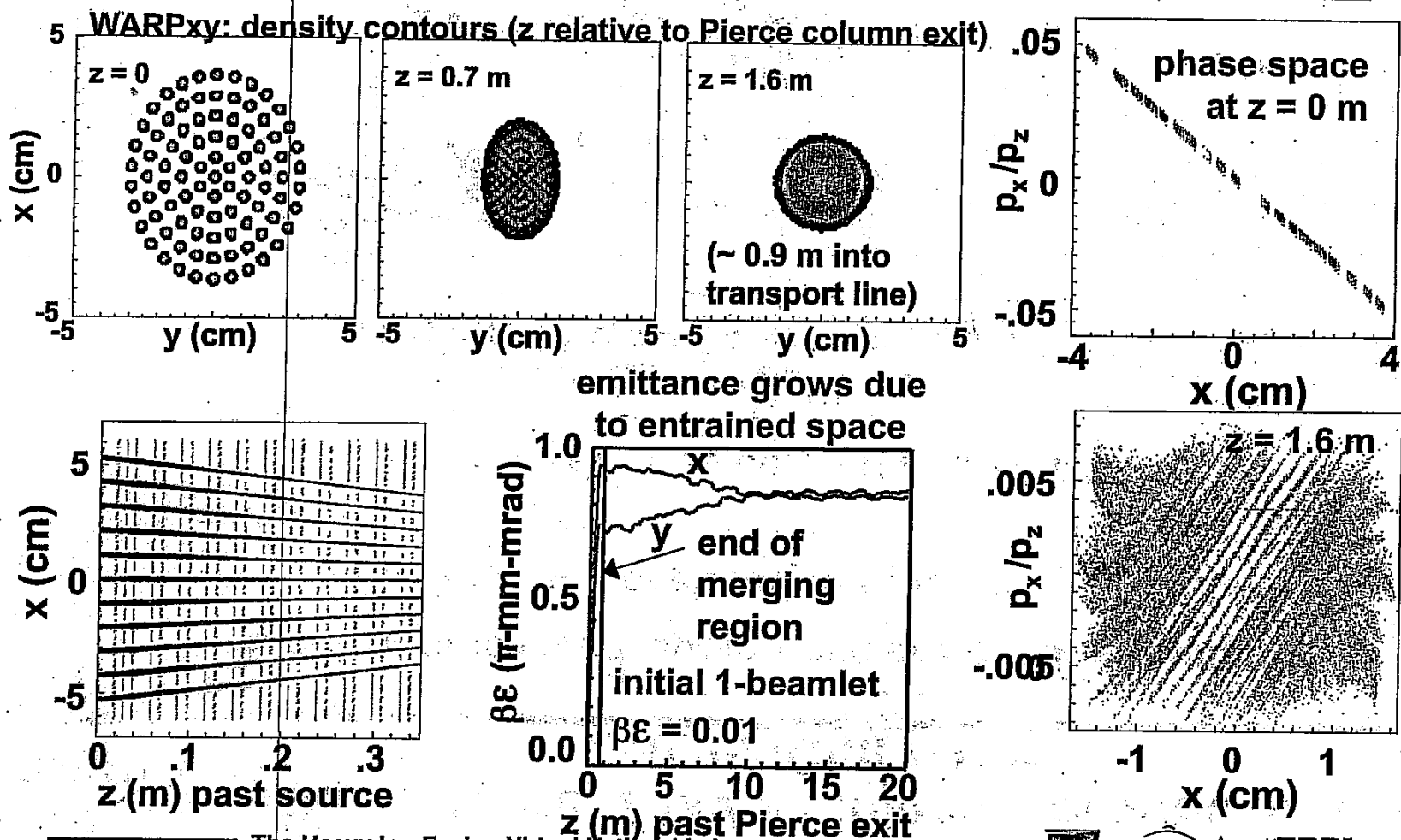
Breakdown limit  $V \propto d^{1.0 \text{ to } 0.5}$

$J \propto V^{-1/2 \text{ to } -5/2} \propto d^{-1/2 \text{ to } -5/4}$



Merge and match beamlets into an ESQ channel

# Simulations of merging-beamlet injector



The Heavy Ion Fusion Virtual National Laboratory.



from D.I. GROTE, E. HENSTLOZA, J.W. KWAN, "DESIGN & SIMULATION OF THE MULTIBEAMLET INJECTOR FOR A HIGH CURRENT ACCELERATOR" SUBMITTED TO PACSTAR (2002)

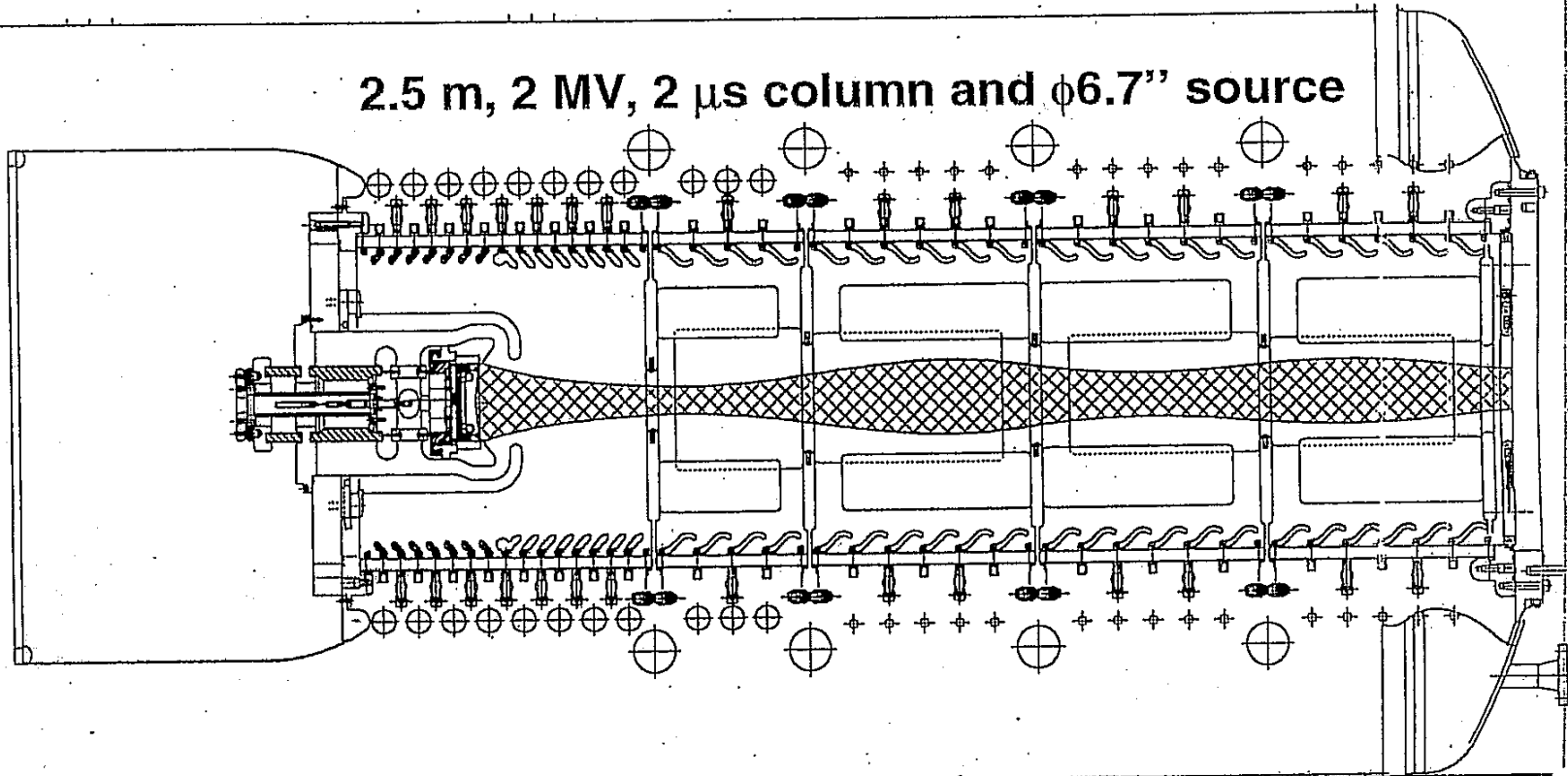




# 0.8 Ampere, 2 MV $K^+$ Injector produced a $\lambda=0.25\mu C/m$ beam

Electrostatic Quadrupole Accelerator for simultaneous focusing and acceleration of ion beams to 2 MV.

2.5 m, 2 MV,  $2\mu s$  column and  $\phi 6.7''$  source



LAWRENCE BERKELEY NATIONAL LABORATORY

Figure no for each of reference

## SCALING OF BRIGHTNESS IN INJECTORS

$$E_N = 4 \rho \langle x^2 \rangle^{1/2} \langle x'^2 \rangle^{1/2} = \frac{4}{c} \left( \frac{v_b}{2} \right) \langle v_x^2 \rangle^{1/2}$$

$$c.v. = 2 r_b \sqrt{\frac{kT}{mc^2}}$$

$$\frac{1}{2} m v_x^2 = \frac{1}{2} kT$$

$$\Rightarrow B = \frac{I}{E_N^2} = \frac{\pi J}{4(kT/mc^2)} \sim \frac{J}{T}$$

$\Rightarrow$  FOR HIGH BRIGHTNESS & HIGH CURRENT  
 MAY WISH TO ACCELERATE MANY BEAMLETS  
 AND THEN MERGE TO FORM SINGLE BEAM.

MANY ISSUES NOT DISCUSSED HERE!

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- SOURCES
- ELECTRON TRAPPING
- CONVERGING BEAMS
- MATCHING TO AN ESQ (e.g.)
- rf
- ...