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## Injectors and longitudinal physics -- II

1. Acceleration - introduction
2. Space charge of short bunches (rf)
3. Space charge of long bunches
4. Longitudinal space charge waves
5. Longitudinal rarefaction waves and bunch ends

# Summary of fluid equations

Let  $n(\underline{x}, t) = \int d^3p f(\underline{x}, \underline{p}, t)$  PARTICLE DENSITY

$\underline{v}(\underline{x}, t) \equiv \frac{1}{n(\underline{x}, t)} \int d^3p \frac{\underline{p}}{\gamma m} f(\underline{x}, \underline{p}, t)$  FLUID VELOCITY

$\underline{P}(\underline{x}, t) \equiv \frac{1}{n(\underline{x}, t)} \int d^3p \underline{p} f(\underline{x}, \underline{p}, t)$  FLUID MOMENTUM

$\underline{\underline{P}}(\underline{x}, t) \equiv \int d^3p (\underline{p} - \underline{P})(\frac{\underline{p}}{\gamma m} - \underline{v}) f(\underline{x}, \underline{p}, t)$  PRESSURE TENSOR

$\frac{d\underline{x}}{dt} = \frac{\underline{p}}{\gamma m}$   $\frac{d\underline{p}}{dt} = q(\underline{E}(\underline{x}, t) + \frac{\underline{p}}{\gamma m} \times \underline{B}(\underline{x}, t))$   $\gamma^2 = \frac{\underline{p} \cdot \underline{p}}{(mc)^2} + 1$

CONTINUITY EQUATION:  $\frac{\partial n(\underline{x}, t)}{\partial t} + \frac{\partial}{\partial \underline{x}} \cdot n(\underline{x}, t) \underline{v}(\underline{x}, t) = 0$

MOMENTUM EQUATION:  $\frac{\partial \underline{P}}{\partial t} + \underline{v} \cdot \frac{\partial \underline{P}}{\partial \underline{x}} = q(\underline{E} + \underline{v} \times \underline{B}) - \frac{1}{n(\underline{x}, t)} \frac{\partial}{\partial \underline{x}} \cdot \underline{\underline{P}}$

THE ABOVE EQUATIONS ARE RELATIVISTICALLY CORRECT. IN THE NON-RELATIVISTIC LIMIT THE CONTINUITY EQUATION REMAINS UNCHANGED & THE MOMENTUM EQUATION MAY BE WRITTEN:

NON RELATIVISTIC  $\rightarrow \frac{\partial \underline{v}}{\partial t} + \underline{v} \cdot \frac{\partial \underline{v}}{\partial \underline{x}} = \frac{q}{m} (\underline{E} + \underline{v} \times \underline{B}) - \frac{1}{m n} \frac{\partial}{\partial \underline{x}} \cdot \underline{\underline{P}}$

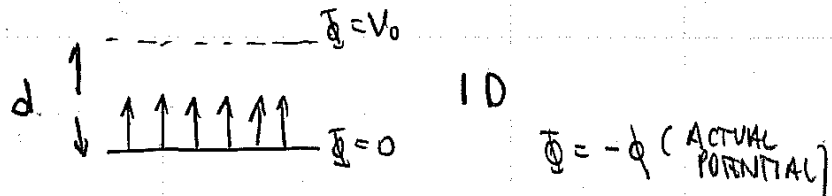
THESE EQUATIONS ARE SUPPLEMENTED WITH MAXWELL'S EQUATIONS: for  $\underline{E}(\underline{x}, t)$  &  $\underline{B}(\underline{x}, t)$

$\frac{\partial}{\partial \underline{x}} \cdot \underline{E} = \frac{q n(\underline{x}, t)}{\epsilon_0}$   $\frac{\partial}{\partial \underline{x}} \times \underline{E} = -\frac{\partial \underline{B}}{\partial t}$

$\frac{\partial}{\partial \underline{x}} \cdot \underline{B} = 0$   $\frac{\partial}{\partial \underline{x}} \times \underline{B} = \mu_0 \underline{J} + \frac{1}{c^2} \frac{\partial \underline{E}}{\partial t}$   $\underline{J}(\underline{x}, t) = q n(\underline{x}, t) \underline{v}(\underline{x}, t)$

NEED ADDITIONAL EQUATIONS SUCH AS  $\underline{\underline{P}} = 0$  OR ENERGY EQUATION TO TERMINATE SET OF EQUATIONS.

## Summary of Child Langmuir Law



CURRENT DENSITY:  $J = \frac{4}{9} \epsilon_0 \left( \frac{2q}{m} \right)^{1/2} \frac{V_0^{3/2}}{d^2}$

$\Phi(z) = V_0 \left( \frac{z}{d} \right)^{4/3}$  — ELECTROSTATIC POTENTIAL

$E(z) = \frac{4}{3} \frac{V_0}{d} \left( \frac{z}{d} \right)^{1/3}$  ELECTRIC FIELD

$v(z) = \left( \frac{2qV_0}{m} \right)^{1/2} \left( \frac{z}{d} \right)^{2/3}$  LONGITUDINAL VELOCITY

$\rho(z) = \frac{J}{v(z)} = \left( \frac{J^2 m}{2qV_0} \right)^{1/2} \left( \frac{z}{d} \right)^{-2/3}$

IF WE MULTIPLY BY  $\pi V_b^2$  (TO ACCOUNT FOR FINITE RADIUS) BEAM:

$I = \frac{4}{9} \epsilon_0 \left( \frac{2q}{m} \right)^{1/2} \left( \frac{V_b}{d} \right)^2 V_0^{3/2}$

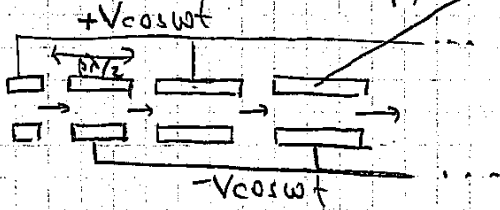
$K \equiv \text{GUN PERVEANCE} \equiv \frac{I}{V_0^{3/2}}$  DIMENSIONS:  $\frac{\text{CURRENT}}{\text{VOLTAGE}^{3/2}}$

GENERALIZED  
(EXCEPT: (DIMENSIONLESS))  
 $Q(z) = \frac{\lambda}{4\pi\epsilon_0 \Phi(z)} = \frac{\pi V_b^2 \rho(z)}{4\pi\epsilon_0 \Phi(z)} = \frac{1}{9} \left( \frac{V_b^2}{z^2} \right)$

(NOTE THAT CHILD-LANGMUIR LAW ONLY VALID FOR  $z \gg \lambda_D$ , WHERE  $\frac{1}{2} m v(z)^2 \gg kT$  &  $\lambda_D = \frac{v_{th}}{\omega_p} = \frac{\sqrt{kT/m}}{\left( \frac{qN(z)^{1/2}}{\epsilon_0 m} \right)}$ )

# ACCELERATION

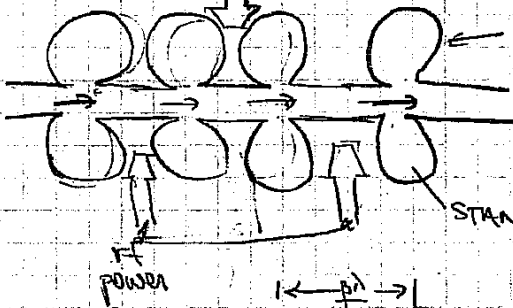
rf (radio-frequency)



TUBE SHIELDS BEAM

(Wideroe lineal)

LOW FREQUENCIES (< 100 MHz)



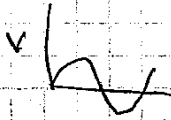
RESONANT CAVITY

(COUPLED CAVITY LINEAL)

$0.1 < \beta < 1.0$

STANDING EM wave

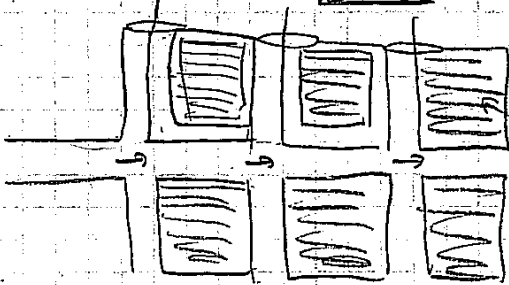
FREQUENCIES ~ 100's MHz - ~ GHz



IN EACH GAP  $E = E_{peak} \cos \omega t$

## Induction acceleration

PULSED POWER



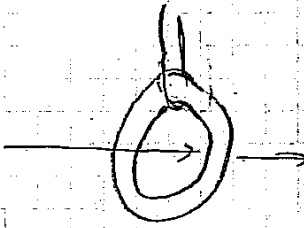
(INDUCTION LINEAL)

TOROIDAL Ferromagnetic CORE

$\nabla \times E = -\partial B / \partial t$

IN EACH GAP  $E = \text{CONSTANT}$

(OR SOME PRESCRIBED FUNCTION)



TRANSFORMER

# I STRATEGY FOR CALCULATING LONGITUDINAL EQUATIONS OF MOTION

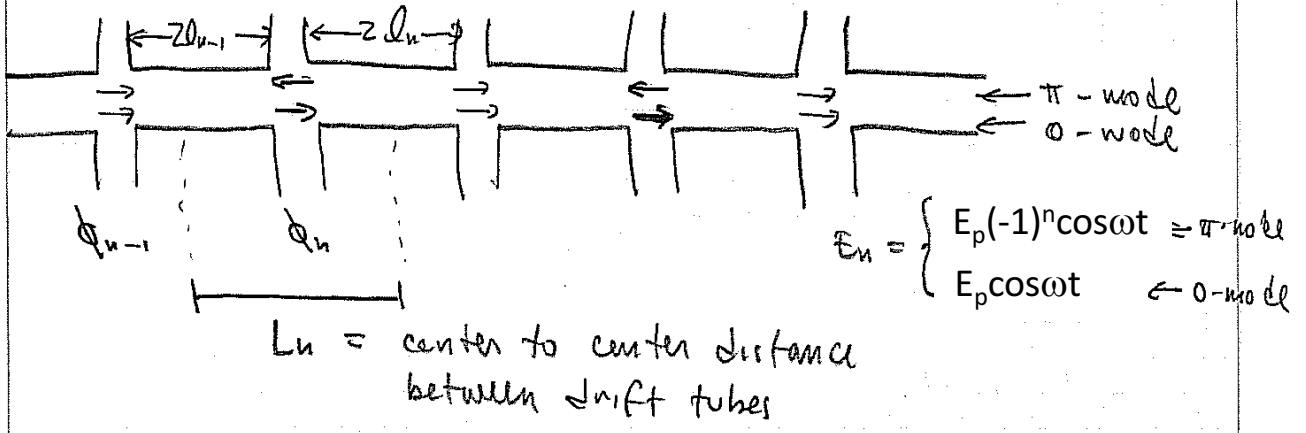
## 1. rf / short bunches

- EXTERNAL FIELD: ACCELERATES AND FOCUSES
  - CALCULATE CHANGE IN PHASE AND ENERGY AS PARTICLE MOVES FROM ACCELERATING GAP TO ACCELERATING GAP
  - APPROXIMATE MOTION AS CONTINUOUS
- SPACE CHARGE FIELD: UNIFORM DENSITY ELLIPSOID

## 2. INDUCTION / LONG BUNCHES

- EXTERNAL FIELD: ACCELERATION, FOCUSING, AND COMPRESSION ACCOMPLISHED BY PRESCRIBING VOLTAGE WAVE FORM
- FOCUSING (CONFINEMENT) IS DONE AT BEAM ENDS
- SPACE CHARGE FIELD:  $E_z \propto \frac{\partial \gamma}{\partial z}$

RF longitudinal equation of motion



$E_z = E_p \cos(\phi_s)$  ← synchronous particle enters each gap at same phase

RESONANCE CONDITION ON SYNCHRONOUS PARTICLE:

$$L_{n-1} = \frac{\beta_s \lambda}{2} \begin{cases} \frac{1}{2} \\ 1 \end{cases} \begin{cases} \pi\text{-mode} \\ 0\text{-mode} \end{cases}$$

$\lambda = \frac{2\pi}{\omega} c =$  light travel distance in one cycle = extra n of oscillation

(IT TAKES  $\frac{1}{\beta_s}$  OSCILLATION PERIOD TO TRAVEL BETWEEN GAPS),  
 $\beta_s = \frac{v_s}{c} =$  velocity of synchronous particle

PARTICLE PHASE RELATIVE TO  $\omega t$  at the  $n^{\text{th}}$  gap:

$$\phi_n = \phi_{n-1} + \omega \frac{2L_{n-1}}{\beta_{n-1} c} + \begin{cases} \pi & \pi\text{-mode} \\ 0 & 0\text{-mode} \end{cases}$$

$$\Delta(\phi - \phi_s)_n = 2\pi \beta_{s,n-1} \left( \frac{1}{\beta_{n-1}} - \frac{1}{\beta_{s,n-1}} \right) \begin{cases} \frac{1}{2} \\ 1 \end{cases} \begin{cases} \pi\text{-mode} \\ 0\text{-mode} \end{cases}$$

$$\approx -2\pi \frac{\delta\beta}{\beta_{s,n-1}} \begin{cases} \frac{1}{2} \\ 1 \end{cases}$$

A VELOCITY DIFFERENCE LEADS TO A PHASE DIFFERENCE

$$\Delta(\phi - \phi_s)_n \approx -2\pi \frac{W_{n-1} - W_{s,n-1}}{m c^2 \gamma_{s,n-1}^3 \beta_{s,n-1}^2} \begin{cases} \frac{1}{2} \\ 1 \end{cases}$$

$$W = (\gamma - 1) m c^2$$

$$\frac{1}{\beta} - \frac{1}{\beta_s} \approx \frac{-\delta\beta}{\beta_s^2}$$

$$\delta W = \gamma_s^3 \beta_s m c^2 \delta\beta$$

SIMILARLY, A PHASE DIFFERENCE PRODUCES

AN ENERGY CHANGE (RELATIVE TO SYNCHRONOUS PARTICLES)

$$\Delta(W - W_s)_n = q E_0 L_n (\cos \psi_n - \cos \psi_{s,n})$$

$$L_n = \frac{(\beta_{s,n-1} + \beta_{s,n}) \lambda}{2} \left\{ \begin{matrix} 1/2 \\ 1 \end{matrix} \right\} =$$

CENTER-TO-CENTER  
DISTANCE  
BETWEEN  
DRIFT SECTIONS

$$(\Delta W_s = q E_0 L_n \cos \psi_s)$$

ENERGY (VELOCITY) DIFFERENCE  $\Rightarrow$

ARRIVAL TIME DIFFERENCE  
(PHASE DIFFERENCE)

PHASE DIFFERENCE IN RF  
FIELD  $\Rightarrow$  DIFFERENCE  
IN ENERGY GAIN

Note that  $E_0$  = the electric field averaged over the distance between accelerating gaps times the "transit time factor".

The transit time factor accounts for the change of the field during the transit of the beam through the gap of width  $d$ .

$E_0 \cong E_p (d/L_n) T$  where  $E_p$  is the peak field and

$$\begin{aligned} \text{where } T &\cong \int_{-d/2}^{d/2} E_{peak} \cos(2\pi z/\beta\lambda) dz / \int_{-d/2}^{d/2} E_{peak} dz \\ &= \sin(\pi d/\beta\lambda) / (\pi d/\beta\lambda) \quad \rightarrow 1 \text{ if } \pi d/\beta\lambda \ll 1 \end{aligned}$$

CONVERTING TO A CONTINUOUS VARIABLE:

$$\Delta(\phi - \phi_s) \rightarrow \frac{d\Delta\phi}{dn} \quad \Delta(W - W_s) \rightarrow \frac{d\Delta W}{dn}$$

$$\Rightarrow \left[ \gamma_s^3 \beta_s^3 \frac{d\Delta\phi}{ds} = -2\pi \frac{\Delta W}{mc^2 \lambda} \right] \quad \left. \frac{dn = ds}{\beta_s \lambda} \left\{ \begin{matrix} 2 \\ 1 \end{matrix} \right\} \right\} = \frac{ds}{2l_{n-1}}$$

$$\frac{d\Delta W}{ds} = qE_0 (\cos \phi - \cos \phi_s)$$

$$\frac{d}{ds} \left[ \gamma_s^3 \beta_s^3 \frac{d\Delta\phi}{ds} \right] = -2\pi \frac{qE_0}{mc^2 \lambda} [\cos \phi - \cos \phi_s] \quad (I)$$

NOW THE SPATIAL SEPARATION IS GIVEN BY:

$$\Delta z \equiv z - z_s = -\frac{\beta_s \lambda}{2\pi} \Delta\phi$$

$$\Rightarrow \text{ALSO, LET } \cos \phi - \cos \phi_s \approx -\sin \phi_s \Delta\phi \quad \left[ \text{fn } \frac{2\pi \Delta z}{\beta_s \lambda} = \Delta\phi \ll 1 \right]$$

$$\Rightarrow \frac{d}{ds} \left[ \gamma_s^3 \beta_s^3 \frac{d}{ds} \left( \frac{\Delta z}{\beta_s} \right) \right] \approx \frac{2\pi}{\lambda} \frac{qE_0}{mc^2} \sin \phi_s \frac{\Delta z}{\beta_s}$$

WHEN THE ACCELERATION RATE IS SMALL

$$\Rightarrow \frac{d^2}{ds^2} \Delta z \approx \frac{2\pi}{\lambda} \frac{qE_0 \sin \phi_s}{\gamma_s^3 \beta_s^3 mc^2} \Delta z$$

$$\equiv -k_{s0}^2 \Delta z \quad (\text{synchronization oscillations})$$



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RETURNING TO  $\Delta W - \phi$  NOTATION

Let  $w = \frac{\Delta W}{mc^2}$

$A = \frac{2\pi}{\beta_s^2 \gamma_s^2 \lambda}$

$B = \frac{q E_0}{mc^2}$

$$\Rightarrow w' = B(\cos \phi - \cos \phi_s)$$

$$\phi' = -Aw$$

$$\phi'' = -AB(\cos \phi - \cos \phi_s)$$

MULTIPLYING BY  $\phi'$  AND INTEGRATING:

$\frac{\phi'^2}{2} = -AB(\sin \phi - \phi \cos \phi_s) + \text{const}$

Using  $\phi' = -Aw$  & DIVIDING BY A

$\Rightarrow \frac{Aw^2}{2} + B(\sin \phi - \phi \cos \phi_s) = \text{CONST.}$

kinetic energy

potential energy

$\frac{dW_s}{ds} \sim qE_0 \cos \phi_s$

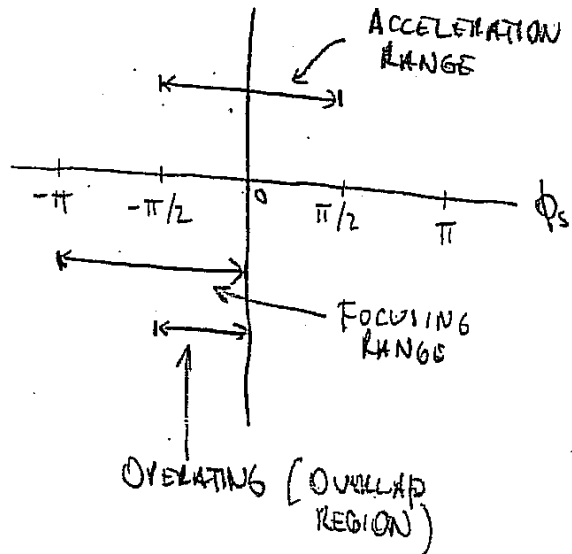
$V(\phi) = B(\sin \phi - \phi \cos \phi_s)$

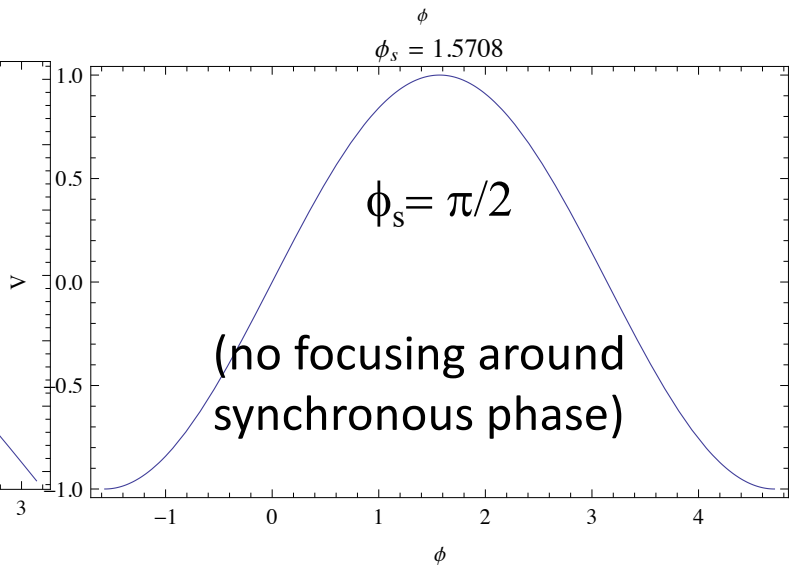
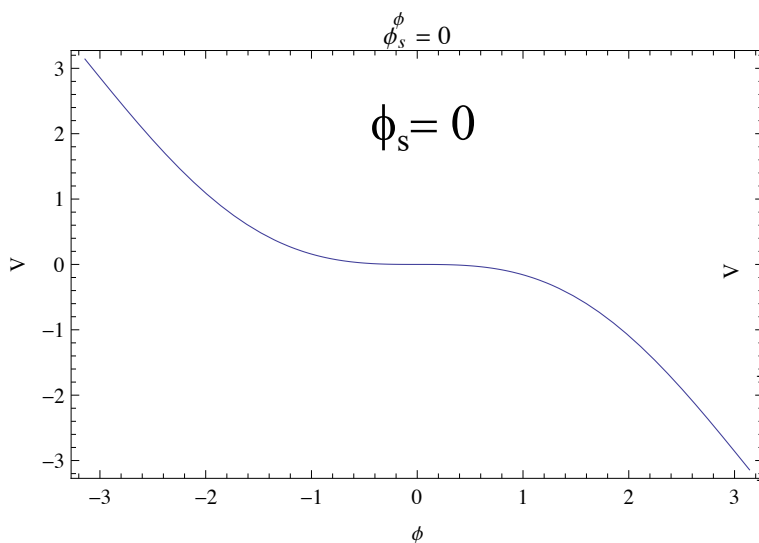
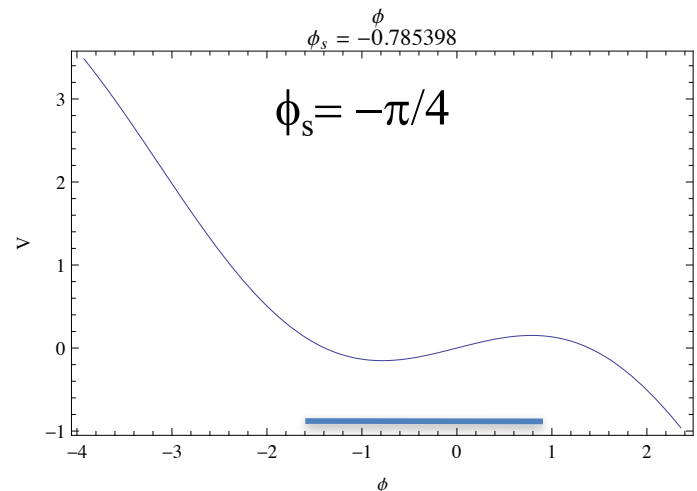
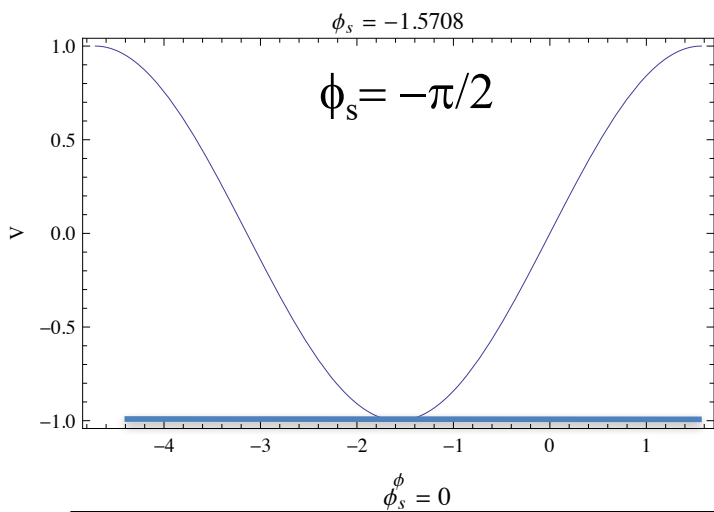
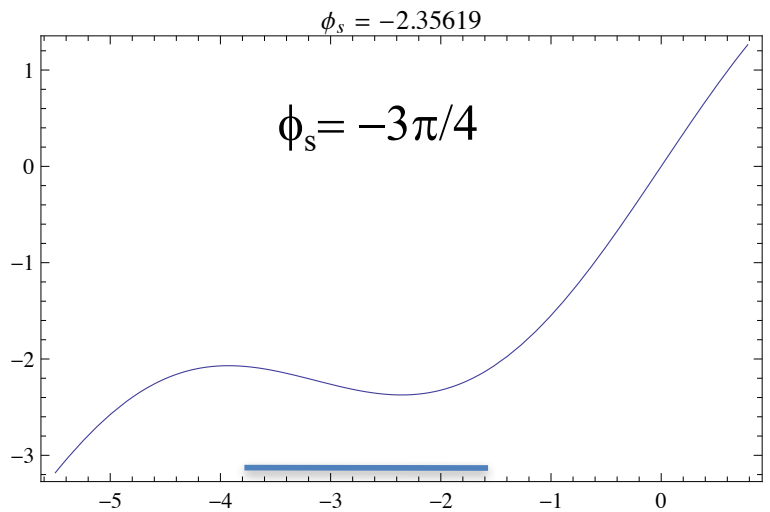
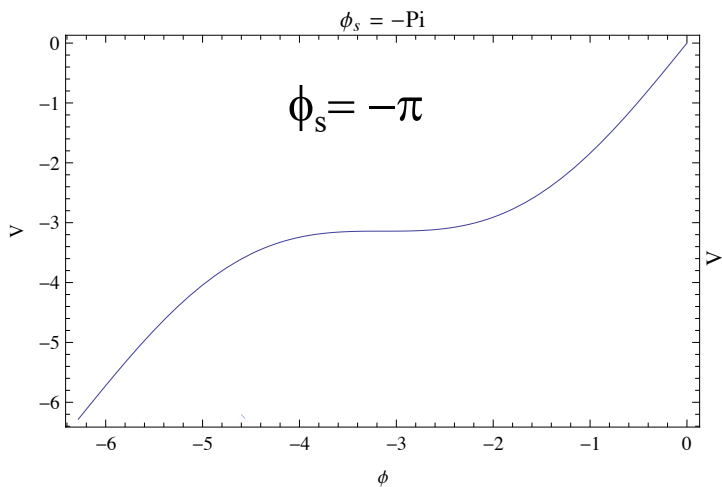
$\frac{dV}{d\phi} = B(\cos \phi - \cos \phi_s)$

$\frac{d^2V}{d\phi^2} = -B \sin \phi$

$> 0 \Rightarrow -\pi < \phi_s < 0$

FOR LONGITUDINAL FOCUSING



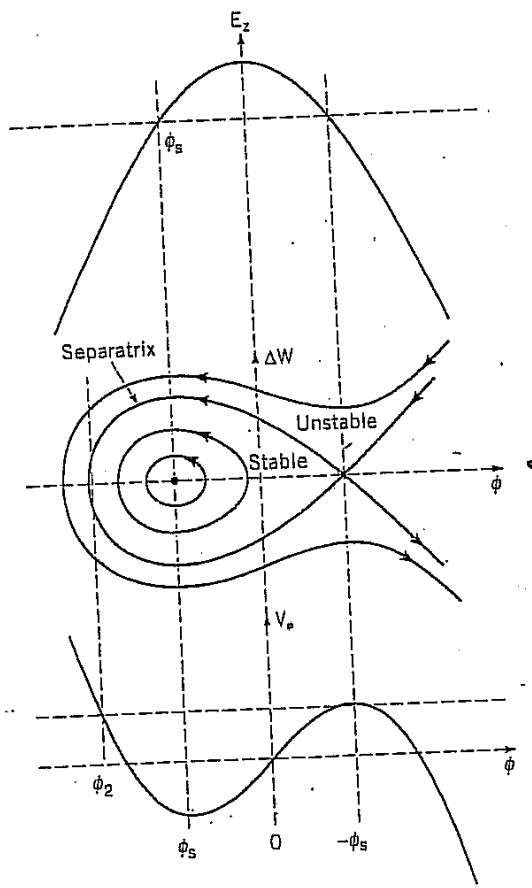


$$V(\phi) \sim B(\sin \phi - \phi \cos \phi_s)$$

For there to be a region of focusing around the synchronous phase,  $-\pi < \phi_s < 0$ .

simultaneous acceleration and a potential well when  $-\pi/2 \leq \phi_s \leq 0$ . The stable region for the phase motion extends from  $\phi_2 < \phi < -\phi_s$ , where the lower phase limit  $\phi_2$  can be obtained numerically by solving for  $\phi_2$  using  $H_\phi(\phi_2) = H_\phi(-\phi_s)$ . Figure 6.3 shows longitudinal phase space and the longitudinal potential well. At the potential maximum, where  $\phi = -\phi_s$ , we

12) are 13) 14) 15) 16) 17) gain, 18) the the 19) < 0. gains



from T. Wangle's "PRINCIPLES of RF LINEAR ACCELERATORS"

←  $\omega - \phi$  PHASE SPACE

Figure 6.3. At the top, the accelerating field is shown as a cosine function of the phase; the synchronous phase  $\phi_s$  is shown as a negative number, which lies earlier than the crest where the field is rising in time. The middle plot shows some longitudinal phase-space trajectories, including the separatrix, the limiting stable trajectory, which passes through the unstable fixed point at  $\Delta W = 0$ , and  $\phi = -\phi_s$ . The stable fixed point lies at  $\Delta W = 0$ , and  $\phi = \phi_s$ . The stable fixed point lies at  $\Delta W = 0$ , and  $\phi = \phi_s$ . The stable fixed point lies at  $\Delta W = 0$ , and  $\phi = \phi_s$ . The stable fixed point lies at  $\Delta W = 0$ , and  $\phi = \phi_s$ .

## Electrostatic potential of a uniform density

ellipsoid in free space

(cf Landau & Lifshitz, Classical Theory of Fields, p. 277)

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} = 1$$

It can be shown that:

$$\varphi = \frac{\rho}{4\epsilon_0} a b c \int_{s_{\min}}^{\infty} \left( 1 - \frac{x^2}{a^2+s} - \frac{y^2}{b^2+s} - \frac{z^2}{c^2+s} \right) \frac{ds}{R_s}$$

$$R_s = \sqrt{(a^2+s)(b^2+s)(c^2+s)}$$

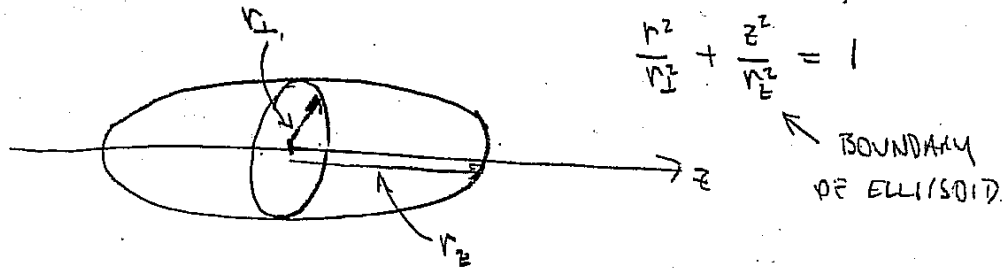
$$s_{\min} = \begin{cases} 0 & \text{if interior point } \left( \frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} < 1 \right) \\ \xi & \text{if exterior point } \left( \frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} > 1 \right) \end{cases}$$

Here  $\xi$  is the positive root of

$$\frac{x^2}{a^2+\xi} + \frac{y^2}{b^2+\xi} + \frac{z^2}{c^2+\xi} = 1$$

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AXISYMMETRIC  
SPACE-CHARGE FIELD OF A BUNCHED BEAM



INTERIOR  
THE POTENTIAL OF A UNIFORM DENSITY BUNCH IN FREE SPACE  
(A MACLAURIN SPHEROID) IS GIVEN BY:

(cf Landau & Lifshitz, Classical Theory of Fields, p 297)

$$\phi = \frac{-\rho}{4\epsilon_0} (\alpha_{\perp} r_{\perp}^2 + \alpha_{\parallel} z^2 - \delta)$$

where  $\alpha_{\perp} = r_{\perp}^2 r_z \int_0^{\infty} \frac{ds}{(r_{\perp}^2 + s) \Delta}$

$$\alpha_{\parallel} = r_{\perp}^2 r_z \int_0^{\infty} \frac{ds}{(r_z^2 + s) \Delta}$$

$$\delta = r_{\perp}^2 r_z \int_0^{\infty} \frac{ds}{\Delta}$$

where  $\Delta^2 = (r_{\perp}^2 + s)^2 (r_z^2 + s)$

FOR NON-RELATIVISTIC BEAM:

$$E_z = -\frac{\partial \phi}{\partial z} = f \frac{\rho}{\epsilon_0} z$$

$$E_r = -\frac{\partial \phi}{\partial r} = \frac{(1-f)}{2} \frac{\rho}{\epsilon_0} r$$

$$f = f(\alpha) = \begin{cases} \frac{\alpha^2}{1-\alpha^2} \left[ \frac{1}{\sqrt{1-\alpha^2}} \tanh^{-1} \sqrt{1-\alpha^2} - 1 \right] & \alpha < 1 \\ \frac{1}{3} & \alpha = 1 \\ \frac{\alpha^2}{\alpha^2-1} \left[ 1 - \frac{1}{\sqrt{\alpha^2-1}} \tanh^{-1} \sqrt{\alpha^2-1} \right] & \alpha > 1 \end{cases} \quad \alpha \equiv \frac{r_{\perp}}{r_z}$$

Check: for a spherical bunch

$$\nabla \cdot \underline{E} = \frac{\rho}{\varepsilon_0} \quad \Rightarrow \quad 4\pi r^2 E_r = \frac{4\pi r^3}{3} \frac{\rho}{\varepsilon_0}$$

$$\Rightarrow E_r = \frac{\rho}{3\varepsilon_0} r$$

THE FIELD FOR ALL RADII MAY BE WRITTEN:

$$E_r = \frac{\rho}{2\epsilon_0} \left[ \frac{\alpha^2}{(\alpha^2 + \chi)(1 + \chi)^{3/2}} - F(\chi, \alpha) \right] r$$

$$E_z = \frac{\rho}{\epsilon_0} [ F(\chi, \alpha) ] z$$

$$F(\chi, \alpha) = \begin{cases} \frac{\alpha^2}{1 - \alpha^2} \left[ \frac{1}{\sqrt{1 - \alpha^2}} \tanh^{-1} \frac{\sqrt{1 - \alpha^2}}{\sqrt{1 + \chi}} - \frac{1}{\sqrt{1 + \chi}} \right] & \alpha < 1 \\ \frac{1}{3(1 + \chi)^{3/2}} & \alpha = 1 \\ \frac{\alpha^2}{\alpha^2 - 1} \left[ \frac{1}{\sqrt{1 + \chi}} - \frac{1}{\sqrt{\alpha^2 - 1}} \tanh^{-1} \left( \frac{\sqrt{\alpha^2 - 1}}{\sqrt{1 + \chi}} \right) \right] & \alpha > 1 \end{cases}$$

$\chi$  satisfies:

$$\frac{\alpha^2 (r^2/r_L^2)}{\alpha^2 + \chi} + \frac{(z^2/r_E^2)}{1 + \chi} = 1 \quad \text{for exterior particle}$$

$$\chi = 0 \quad \text{for interior particle}$$

$$\alpha \equiv \frac{r_L}{r_E}$$

FOR AN EXTERIOR PARTICLE AT  $r \neq z \Rightarrow \chi$  CAN BE SOLVED FOR (QUADRATIC EQUATION FOR  $\chi$ ).

$\Rightarrow E_r$  &  $E_z$  ARE KNOWN ANALYTICALLY FOR ALL  $r, z$ .

$$\text{EXAMPLE: } r = 0 \Rightarrow \chi = \frac{z^2}{r_L^2} - 1$$

(and  $z > r_L$ )

RELATIVISTIC TRANSFORMATION FROM BEAM FRAME TO LAB FRAME:  
(see e.g. JACKSON, CLASSICAL ELECTRODYNAMICS)

$$\underline{E} = \gamma (\underline{E}' - \underline{c} \underline{\beta} \times \underline{B}') - \frac{\gamma^2}{\gamma+1} \underline{\beta} (\underline{\beta} \cdot \underline{E}')$$

$$\underline{B} = \gamma (\underline{B}' + \frac{\underline{\beta} \times \underline{E}'}{c}) - \frac{\gamma^2}{\gamma+1} \underline{\beta} (\underline{\beta} \cdot \underline{B}')$$

$$\underline{B}' = 0$$

$$\Rightarrow E_z = \gamma E'_z - \frac{\gamma^2}{\gamma+1} \beta^2 E'_z = E'_z$$

$$E_r = \gamma E'_r$$

$$B_\theta = \frac{\gamma \beta}{c} E'_r$$

$$F_z = q E_z = q E'_z$$

$$F_r = q (E_r - v_z B_\theta) = \frac{1}{\gamma} q E'_r$$



$$\Delta z = \frac{1}{\gamma} \Delta z'$$

$$\underline{x}_\perp = \underline{x}'_\perp$$

$$\rho = \gamma \rho'$$

$$\underline{F}_\perp = \frac{d\underline{p}_\perp}{dt} = \gamma_s m v_{zs}^2 \frac{d^2 \underline{x}_\perp}{ds^2} \quad (\text{NEGLECTING } \frac{d\gamma_s}{dt}, \frac{dv_{zs}}{dt})$$

$$\Delta \underline{F}_\perp = \frac{d\underline{p}_\perp}{dt} - \frac{d\underline{p}'_\perp}{dt} = \gamma_s^3 m v_{zs}^2 \frac{d^2 (z - z_s)}{ds^2}$$

$$(\text{USING } \frac{d}{ds} \gamma \rho = \gamma^3 \frac{d\rho}{ds})$$



FOR RELATIVISTIC BEAM

(cf. BARNARD & LUND 1997  
LUND & BARNARD 1997)  
PAC 97 CONF. PROCEEDINGS

$$\frac{d^2 X_L}{ds^2} = \frac{F_L}{\gamma_s^3 \beta_s^2 mc^2}$$

$$\underline{F}_{\perp s} = \frac{q\rho}{2\gamma_s^2 \epsilon_0} [1 - f(\alpha)] X_L$$

$$\frac{d^2 \Delta z}{ds^2} = \frac{F_z}{\gamma_s^3 \beta_s^2 mc^2}$$

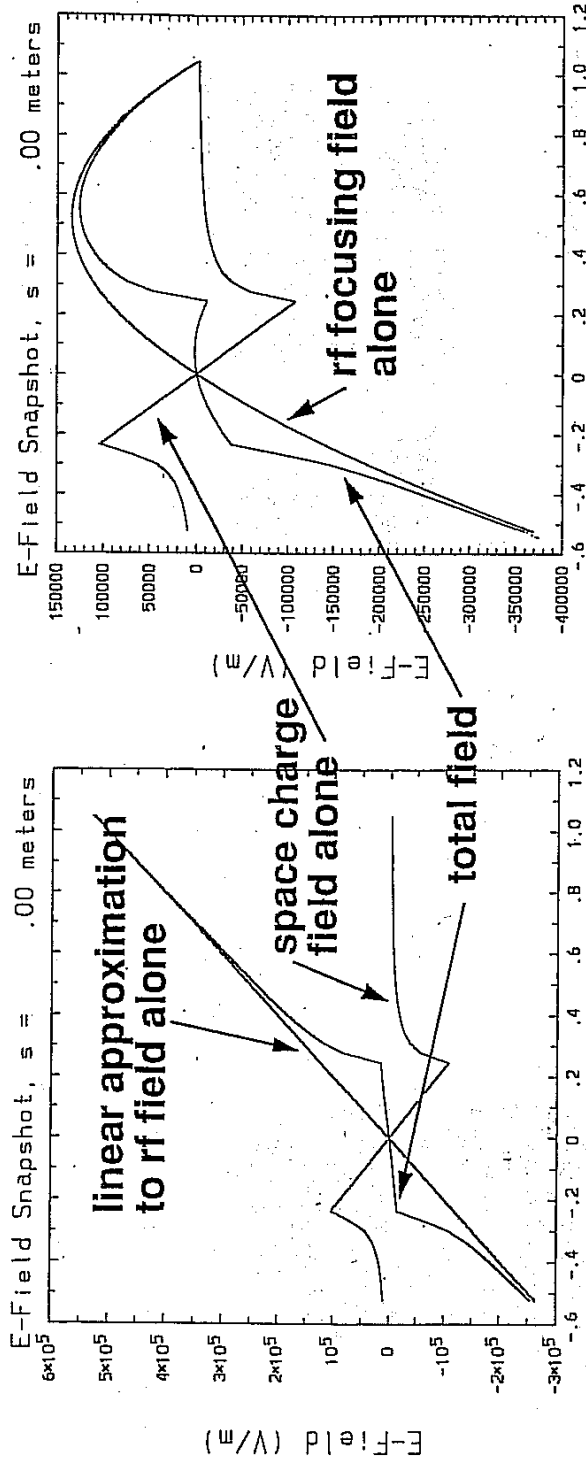
$$\underline{F}_{zs} = \frac{q\rho}{\epsilon_0} f(\alpha) \Delta z$$

$$\alpha = \frac{r_L}{\gamma v_z} \quad \left[ \alpha = \frac{r_L}{(v_z \text{ in comoving frame})} \right]$$

COMBINING FOCUSING + SELF FIELDS

$$\frac{d^2 \Delta z}{ds^2} = -k_{s0} \Delta z + \frac{q\rho f(\alpha)}{\gamma_s^3 \beta_s^2 mc^2 \epsilon_0} \Delta z \quad (\text{LINEAR rf})$$

# Total field seen by particle is sum of rf and spacecharge

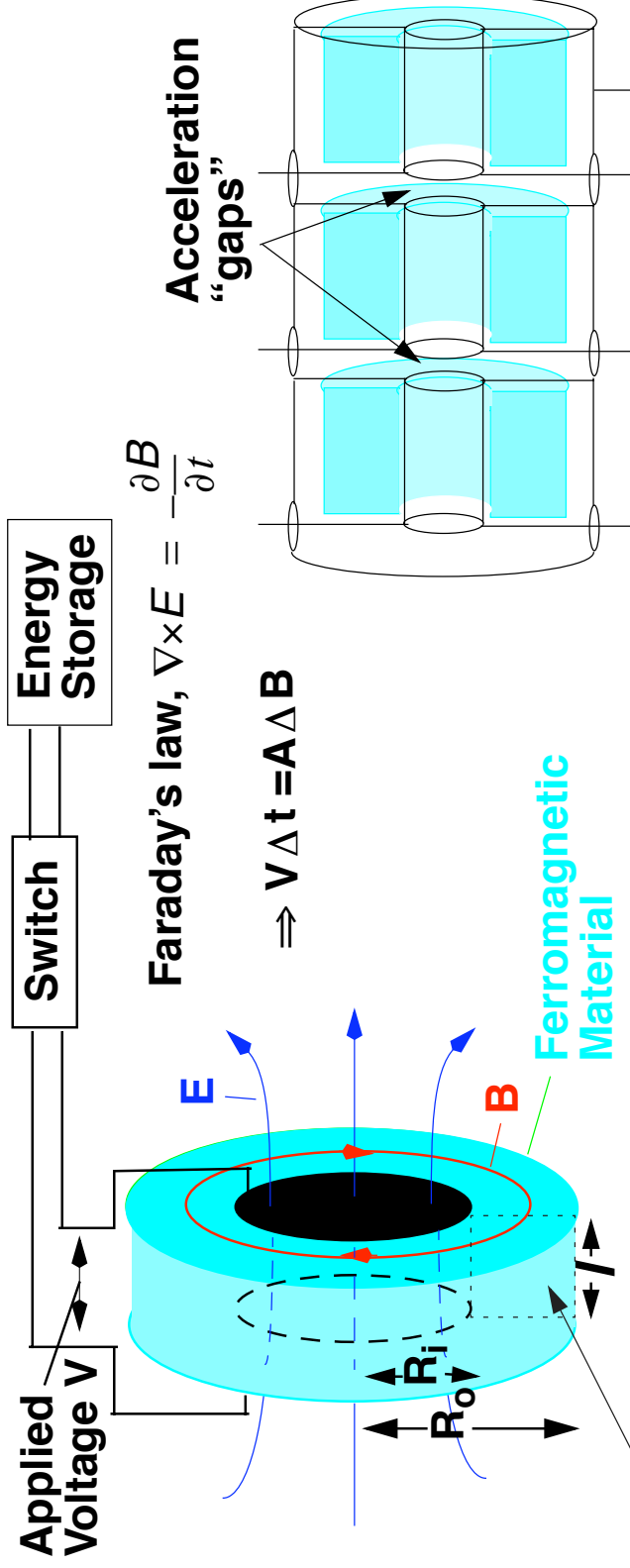


$\phi - \phi_s$  (rad)

$\phi - \phi_s$  (rad)

here  $\phi - \phi_s = - (2 \pi / \beta_s \lambda) \Delta z$ , where  $\beta_s c$  is the longitudinal velocity of the synchronous particle and  $\lambda = c/v$  is the rf vacuum wavelength

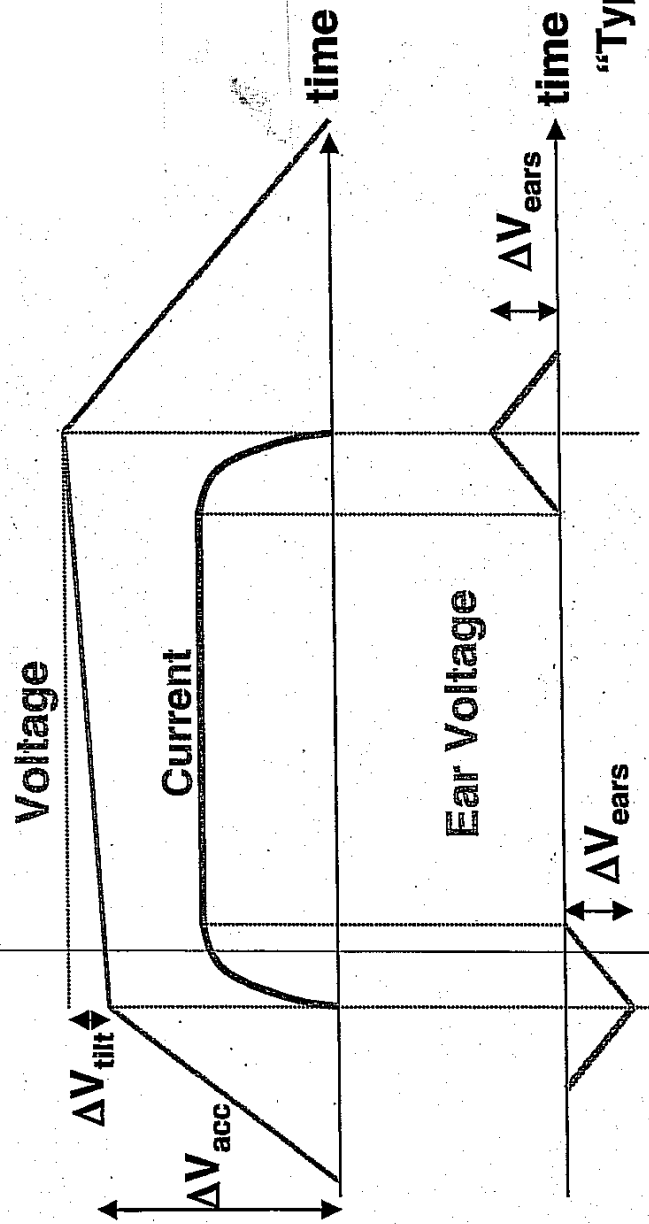
# Induction acceleration: Volt-second limits



Volt-seconds per m:  $(dV/dz) \Delta t = (R_o - R_i) \Delta B$   $f_{\text{radial}}$   $f_{\text{longit.}}$   
 $\sim 1 \text{ m}$   $\sim 2.5 \text{ T}$   $\sim 0.8$   $\sim 0.8$

$(dV/dz) \Delta t < \sim 1.6 \text{ V-s/m}$

Several types of waveform are needed to accelerate, compress, and confine the beam



"Typical" numbers:

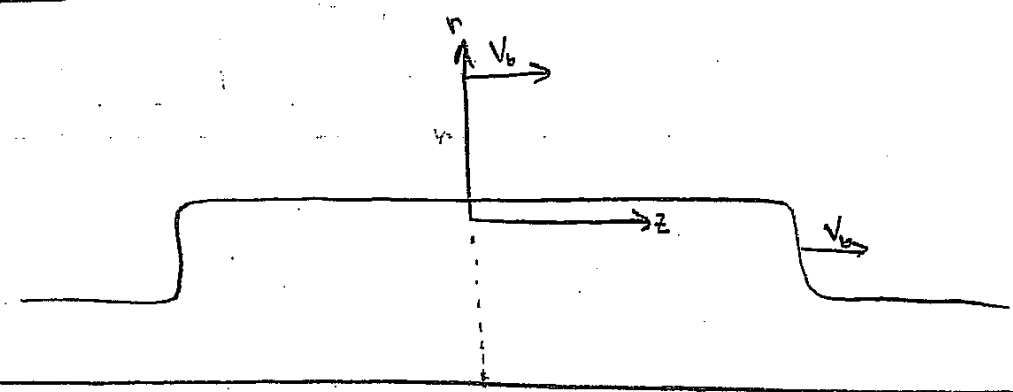
- $\Delta V_{tilt} \sim 1 \text{ kV}$
- $\Delta V_{ears} \sim 14 \text{ kV}$
- $\Delta V_{acc} \sim 100 \text{ kV}$



The Heavy Ion Fusion Virtual National Laboratory



# COORDINATE SYSTEM



42-182 100 SHEETS  
National Brand  
Made in U.S.A.

$s=0$

$s = \beta_0 c t$  for drifting beam  
= position of beam center in lab frame

$s \leftrightarrow t$  are related by  $\beta_0 c$  for drifting beam

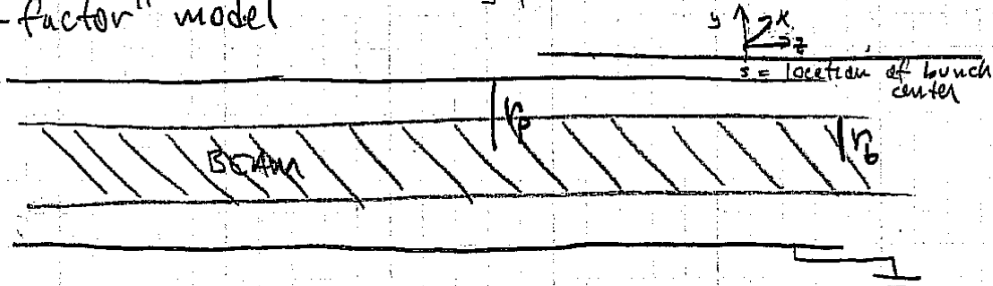
$z$  = longitudinal coordinate in beam frame ( $z=0$  = beam center)

$r$  = radial coordinate in beam frame (or lab frame).

(This class will assume non-relativistic dynamics)  
These are ions with  $\beta < 0.2$ ).

# LONGITUDINAL PHYSICS OF LONG PULSES (BUNCH LENGTH $\gg r_{\text{pipe}}$ )

"g-factor" model



If  $\frac{\partial^2 \phi}{\partial z^2} \ll \frac{1}{r} \left( \frac{\partial}{\partial r} r \frac{\partial \phi}{\partial r} \right) \Rightarrow \frac{\partial \phi}{\partial r} = - \frac{\lambda(r)}{2\pi\epsilon_0 r}$

Let  $\rho = \begin{cases} \rho_0 & 0 < r < r_b \\ 0 & r_b < r < r_p \end{cases} \Rightarrow \lambda = \lambda_0 \left( \frac{r}{r_b} \right)^2$

$\phi = \int_r^{r_p} \frac{\partial \phi}{\partial r} dr = \begin{cases} \frac{\lambda}{2\pi\epsilon_0} \left[ \frac{1}{2} \left( 1 - \frac{r^2}{r_b^2} \right) + \ln \frac{r_p}{r_b} \right] & 0 < r < r_b \\ \frac{\lambda}{2\pi\epsilon_0} \ln \left( \frac{r_p}{r} \right) & r_b < r < r_p \end{cases}$

$\frac{\partial \phi}{\partial z} = \frac{1}{2\pi\epsilon_0} \left[ \frac{1}{2} \left( 1 - \frac{r^2}{r_b^2} \right) + \ln \frac{r_p}{r_b} \right] \frac{\partial \lambda}{\partial z} - \frac{1}{2\pi\epsilon_0} \left[ 1 - \frac{r^2}{r_b^2} \right] \frac{\lambda}{r_b} \frac{\partial r_b}{\partial z}$

If  $\rho = \text{const} \Rightarrow \frac{\lambda}{r_b^2} = \text{const} \Rightarrow \frac{\partial \lambda}{\partial z} = - \frac{2\lambda}{r_b} \frac{\partial r_b}{\partial z}$

$\Rightarrow \frac{\partial \phi}{\partial z} = \frac{1}{2\pi\epsilon_0} \ln \left( \frac{r_p}{r_b} \right) \frac{\partial \lambda}{\partial z}$

$E_z = - \frac{g}{4\pi\epsilon_0} \frac{\partial \lambda}{\partial z}$

where  $g = 2 \ln \left( \frac{r_p}{r_b} \right)$

For space charge dom. beam:

$k_{\beta 0}^2 r_b = Q/r_b$

$k_{\beta 0}^2 \sim \lambda/r_b^2 \sim \rho \sim \text{const}$

[ SPACE-CHARGE DOMINATED BEAM ]

500 SHEETS, FULLER'S SQUARE  
 450 SHEETS, FULLER'S SQUARE  
 400 SHEETS, FULLER'S SQUARE  
 350 SHEETS, FULLER'S SQUARE  
 300 SHEETS, FULLER'S SQUARE  
 250 SHEETS, FULLER'S SQUARE  
 200 SHEETS, FULLER'S SQUARE  
 150 SHEETS, FULLER'S SQUARE  
 100 SHEETS, FULLER'S SQUARE  
 50 SHEETS, FULLER'S SQUARE  
 25 SHEETS, FULLER'S SQUARE  
 10 SHEETS, FULLER'S SQUARE  
 5 SHEETS, FULLER'S SQUARE  
 1 SHEET, FULLER'S SQUARE  
 MADE IN U.S.A.



$$\frac{\partial d}{\partial z} = \frac{1}{2\pi\epsilon_0} \left[ \frac{1}{2} \left( 1 - \frac{v^2}{v_b^2} \right) + \ln \frac{r_p}{r_b} \right] \frac{\partial \lambda}{\partial z} - \frac{1}{2\pi\epsilon_0} \left[ 1 - \frac{v^2}{v_b^2} \right] \frac{\lambda}{r_b} \frac{\partial r_b}{\partial z}$$

FOR EMITTANCE DOMINATED BEAMS:

(with constant emittance and radius)

RADIUS NOT DETERMINED BY  $\lambda$

$$\text{so } \frac{\partial r_b}{\partial z} \approx 0$$

$$\left\langle \frac{\partial d}{\partial z} \right\rangle = \frac{1}{2\pi\epsilon_0} \left[ \frac{1}{2} \left( 1 - \left\langle \frac{v^2}{v_b^2} \right\rangle \right) + \ln \frac{r_p}{r_b} \right] \frac{\partial \lambda}{\partial z}$$

$$\Rightarrow g = 2 \ln \left( \frac{r_p}{r_b} \right) + \frac{1}{2} \quad (\text{EMITTANCE DOMINATED BEAMS})$$

(SEE REISER, SECTION 6.3 FOR DISCUSSION ON g-FACTOR).

Vlasov - equation for a drifting beam:

$$\frac{\partial f}{\partial s} + x' \frac{\partial f}{\partial x} + x'' \frac{\partial f}{\partial x'} + y' \frac{\partial f}{\partial y} + y'' \frac{\partial f}{\partial y'} + z' \frac{\partial f}{\partial z} + z'' \frac{\partial f}{\partial z'} = 0$$

Let  $\tilde{f}(z, z', s) \equiv \iiint f dx dx' dy dy'$

INTEGRATING VLASOV EQUATION:

If  $z'' \neq f(x, x', y, y')$ :

$$\Rightarrow \frac{\partial \tilde{f}}{\partial s} + \iiint x' \frac{\partial f}{\partial x} dx dx' dy dy' + \dots + z' \frac{\partial \tilde{f}}{\partial z} + z'' \frac{\partial \tilde{f}}{\partial z'} = 0$$

$\int_{-\infty}^{\infty} x' f dx = \frac{d}{ds} \int_{-\infty}^{\infty} x f dx$

$$\Rightarrow \boxed{\frac{\partial \tilde{f}}{\partial s} + z' \frac{\partial \tilde{f}}{\partial z} + z'' \frac{\partial \tilde{f}}{\partial z'} = 0} \quad \text{1D Vlasov}$$

Now let  $\lambda \equiv q \int \tilde{f} dz'$ ;  $\lambda \bar{z}' = \int \tilde{f} z' dz'$ ;  $\lambda \bar{z}'^2 \equiv \int \tilde{f} z'^2 dz'$

Also, let  $\Delta z'^2 \equiv \bar{z}'^2 - (\bar{z}')^2$

FLUID EQUATIONS

INTEGRATING 1D VLASOV OVER  $z'$ :

$$\boxed{\frac{\partial \lambda}{\partial s} + \frac{\partial (\lambda \bar{z}')}{\partial z} = 0} \quad \text{(CONTINUITY EQUATION)}$$

MULTIPLYING BY  $z'$  & INTEGRATING VLASOV OVER  $z'$ :

$$\frac{\partial}{\partial s} \lambda \bar{z}' + \frac{\partial}{\partial z} \lambda \bar{z}'^2 - \lambda \bar{z}'' = 0$$

DIVIDING BY  $\lambda$ , USING CONTINUITY EQUATION & DEFINITION OF  $\Delta z'^2$ :

$$\boxed{\underbrace{\frac{\partial \bar{z}'}{\partial s} + \bar{z}' \frac{\partial}{\partial z} \bar{z}'}_{\text{INERTIAL}} + \underbrace{\frac{1}{\lambda} \frac{\partial (\lambda \Delta z'^2)}{\partial z}}_{\text{PRESSURE TERM}} = \underbrace{\bar{z}''}_{\text{FORCE}}} \quad \text{(MOMENTUM EQUATION)}$$

$$= \frac{1}{v_0^2} \frac{q E_z}{m}$$

100% RECYCLED PAPER  
 50% RECYCLED FIBER  
 100% RECYCLED INK  
 100% RECYCLED GLUE  
 100% RECYCLED WHITE  
 100% RECYCLED  
 MADE IN U.S.A.



## COMBINING g-factor model with fluid equations

$$\frac{\partial \lambda}{\partial s} + \frac{\partial}{\partial z} (\lambda \bar{z}') = 0$$

$$\frac{\partial \bar{z}'}{\partial s} + \bar{z}' \frac{\partial \bar{z}'}{\partial z} + \underbrace{\frac{1}{\lambda} \frac{\partial}{\partial z} (\lambda \Delta \bar{z}'^2)}_{\text{PRESSURE TERM}} = \underbrace{\frac{-gg}{4\pi \epsilon_0 m v_0^2} \frac{\partial \lambda}{\partial z}}_{\text{SPACE CHARGE TERM}}$$

WHEN PRESSURE TERM  $\ll$  SPACE CHARGE TERM,

$$\left( \text{LET } c_s^2 \equiv \frac{gg \lambda_0}{4\pi \epsilon_0 m} \right) = \text{"(SPACE CHARGE WAVE SPEED)}^2"$$

$$\Rightarrow \left\{ \begin{aligned} \frac{\partial \lambda}{\partial s} + \lambda \frac{\partial \bar{z}'}{\partial z} + \bar{z}' \frac{\partial \lambda}{\partial z} &= 0 \\ \frac{\partial \bar{z}'}{\partial s} + \bar{z}' \frac{\partial \bar{z}'}{\partial z} + \frac{c_s^2}{\lambda v_0^2} \frac{\partial \lambda}{\partial z} &= 0 \end{aligned} \right. \quad (g1)$$

### LINEARIZING g1

$$\text{Let } \lambda = \lambda_0 + \lambda_1 \quad \bar{z}' = \bar{z}'_0 + \bar{z}'_1$$

$$\text{EQUILIBRIUM } \lambda_0 = \text{CONSTANT}$$

$$\bar{z}'_0 = 0$$

### LINEARIZING

$$\frac{\partial \lambda_1}{\partial s} + \lambda_0 \frac{\partial \bar{z}'_1}{\partial z} = 0 \quad (g2a)$$

$$\frac{\partial \bar{z}'_1}{\partial s} + \frac{c_s^2}{\lambda_0 v_0^2} \frac{\partial \lambda_1}{\partial z} = 0 \quad (g2b)$$

TAKING  $\frac{\partial}{\partial s}$  of (g2a) &  $\frac{\partial}{\partial z}$  of g2b and combining:

$$\Rightarrow \left[ \frac{\partial^2 \lambda_1}{\partial s^2} - \frac{c_s^2}{v_0^2} \frac{\partial^2 \lambda_1}{\partial z^2} \right] = 0 \quad \Rightarrow \text{WAVE EQUATION}$$

SOLVING WAVE EQUATION

$$\frac{\partial^2 \lambda_1}{\partial s^2} - \frac{c_s^2}{v_0^2} \frac{\partial^2 \lambda_1}{\partial z^2} = 0$$

Let  $\lambda_1 = \tilde{\lambda}_1 \exp\left[\frac{i\omega}{v_0} s \pm ikz\right]$

$$-\frac{\omega^2}{v_0^2} + \frac{k^2 c_s^2}{v_0^2} = 0 \Rightarrow \omega = c_s k$$

→ PHASE & GROUP VELOCITY OF WAVES =  $c_s$   
(in beam frame)

GENERAL SOLUTION

$$\lambda_1 = \lambda_0 f_+[u_+] + \lambda_0 f_-[u_-]$$

where  $u_+ = z + \frac{c_s s}{v_0} + C_0$  &  $u_- = z - \frac{c_s s}{v_0} + C_0$

&  $f_+[u]$  &  $f_-[u]$  are any functions of the argument &  $C_0$  is an arbitrary constant.

$$\tilde{z}_1 = \frac{c_s}{v_0} [-f_+[u_+] + f_-[u_-]]$$

s=0:

$\lambda_1(z)$

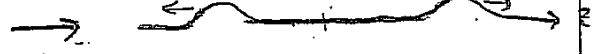


s=s\_0:

$\lambda_1(z)$

BACKWARD WAVE

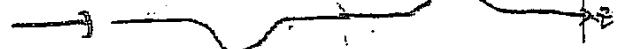
FORWARD WAVE



$\tilde{z}_1(z)$



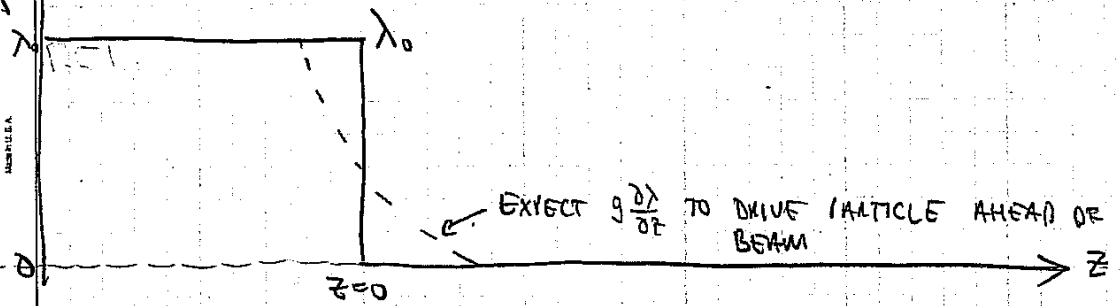
$\tilde{z}_1(z)$



# BEAM ENDS & RAREFACTION WAVES

(FALTINGS & LEE,  
J. App. Phys. 61, 5219)  
(Also Landau & Lifshitz #5,  
Fluid Mechanics)

SUPPOSE YOU START WITH A PULSE THAT ENDS WITH A STEP FUNCTION IN  $\lambda$ . WHAT HAPPENS TO THE END?



TO ANALYZE: RETURN TO NON-LINEAR FLUID EQUATIONS (SINCE  $\delta\lambda \sim \lambda_0$ ) (g1):

$$\frac{\partial \lambda}{\partial t} + \lambda \frac{\partial \lambda}{\partial z} + \frac{c^2}{\lambda} \frac{\partial \lambda}{\partial z} = 0 \quad (\text{CONTINUITY})$$

$$\frac{\partial^2 \lambda}{\partial t^2} + \frac{\partial^2 \lambda}{\partial z^2} + \frac{c^2}{\lambda_0 v_0^2} \lambda \frac{\partial \lambda}{\partial z} = 0 \quad (\text{MOMENTUM})$$

1st IT IS CONVENIENT TO DEFINE:  $\Lambda \equiv \lambda / \lambda_0$

$$V \equiv \frac{v_0}{c} \frac{z}{\lambda_0}$$

$$z \equiv \frac{v_0}{c} z$$

$$(c^2 \equiv \frac{g \rho \lambda_0}{m 4\pi \epsilon_0})$$

$$\Rightarrow \frac{\partial \Lambda}{\partial t} + \Lambda \frac{\partial \Lambda}{\partial z} + \Lambda \frac{\partial \Lambda}{\partial z} = 0 \quad (\text{CONTINUITY})$$

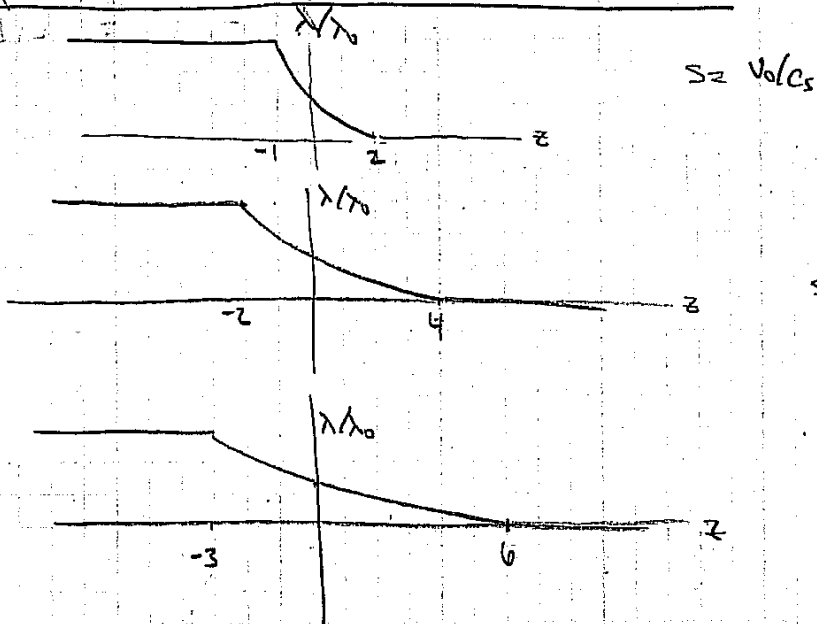
$$\frac{\partial \Lambda}{\partial t} + \Lambda \frac{\partial \Lambda}{\partial z} + \frac{\partial \Lambda}{\partial z} = 0 \quad (\text{r1})$$

(momentum)





### SPATIAL PROFILES OF $V/\lambda_0$ VS $z$ AT VARIOUS $s$



$s = v_0/c_s$

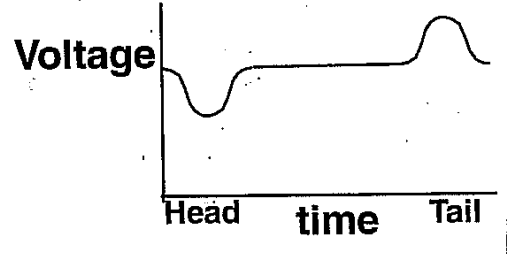
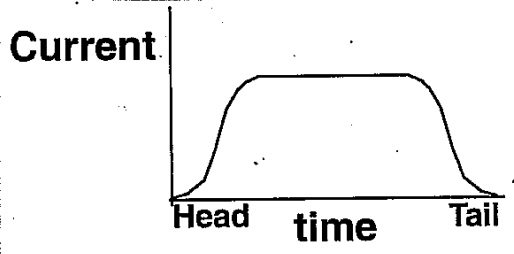
$s = 2v_0/c_s$

$s = 3v_0/c_s$

### HOW DOES ONE PREVENT "END EROSION"?

APPLY EAR PULSES AT END OF BEAM:

$$V \sim E_z = \frac{+q \cdot \partial \lambda}{4\pi \epsilon_0 \partial z}$$



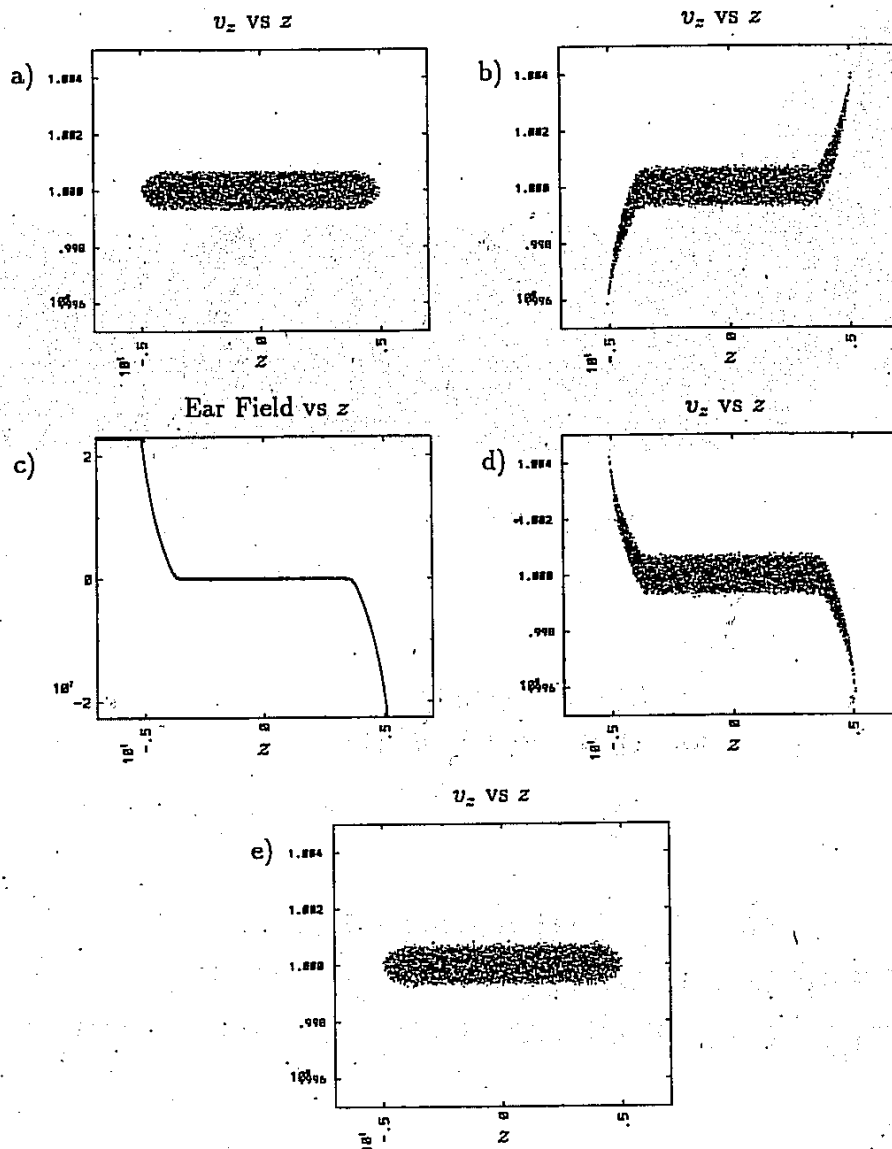


Figure 6.4: One cycle of intermittently-applied ears. (a) Initial phase space (b) Beam expands (c) Ear Field is applied (d) Beam is compressed (e) Beam expands back to its initial state

from D. Callahan Miller  
 PhD thesis, U.C. Davis, 1994.